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X. Contributions to Terrestrial Magnetism.—No. V. By Lieut.-Colonel Edward Sabine, R.A., F.R.S.

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- § 8. Observations within the Antarctic Circle, made on Board Her Majesty's Ships Erebus and Terror, in the Summer of 1840, 1841, in the Expedition under the command of Captain James Clark Ross, R.N.
- § 9. Observations between Kerguelen Island and Van Diemen Island, made on Board Her Majesty's Ship Erebus, July and August 1840.
 - § 8. Observations within the Antarctic Circle in the Summer of 1840, 1841.

IN the present number of these Contributions, I have the pleasure of laying before the Royal Society the magnetic observations made by Captain James Clark Ross, and the Expedition under his command, in the first of the three voyages in which these researches have been prosecuted within the Antarctic Circle; and I gladly avail myself of the opportunity which the occasion affords, of congratulating the Society on the successful completion of the labours and on the approaching return, of an Expedition, in which the Fellows individually, and as a body, have taken so strong an interest. A large portion of the observations contained in this number were made in southern latitudes never before reached by man; and nearly the whole in a part of the globe extremely difficult of access, but containing within itself a field for researches peculiarly needed for completing and perfecting, in the words of Halley, "the abstruse theory of terrestrial magnetism."

In presenting to the Royal Society this portion of the results of an arduous enterprise, undertaken at their recommendation, it appears no improper departure from the usual tone of these communications, to allude very briefly to the causes which, under Providence, have conduced to its safe and successful issue;—to the admirable preparation and equipment of the vessels on the part of the Government,—to the high qualities of its Commander, manifested in conducting to its close, almost without an accident, and to the fullest accomplishment of its objects, a service of such duration and peculiar hazard,—and to the excellent spirit in which the Commander has been seconded by Captain Crozier, and supported by the officers and seamen who have been their worthy associates.

Viewed merely as an expedition of discovery, its voyages must ever rank high in the annals of those maritime achievements of which our country is proud; but as a scientific expedition, which is its more proper character, as well as that in which the Royal Society must regard it with the greatest satisfaction, its best praise will undoubtedly be found in the record of its performances; and I hasten therefore to enter on that portion of them which I am now enabled to present to the Society.

The peculiar feature in the magnetic survey of the portion of the southern hemisphere now under notice is, that it was conducted almost exclusively on board ship, the observations being subject to the disturbance occasioned by the ship's iron, in a part of the globe where the effect of this influence becomes excessive. The first consideration, therefore, must be to investigate the corrections which it is necessary to employ in compensation. The analysis of the effects produced by the iron of a vessel, and the theory of their corrections, have been given by the late M. Poisson, in a memoir read in 1838, and published in the Transactions of the Académie des Sciences, entitled "Mémoire sur les déviations de la Boussole produites par le fer des Vaisseaux." In cases in which the disturbance is due, partly to the magnetism induced by the earth's influence in the soft iron of the vessel, and partly to permanent magnetism acquired and retained by harder portions of her iron, the complexity of the source from whence the disturbance originates renders its correction very difficult. But in wood-built ships, when proper precautions are taken in regard to the place in the ship in which the instrument is used in observation, the disturbing influence is generally found to be that of induced magnetism alone: and in this case the correction may be obtained with tolerable facility*. The disturbance produced by the iron of the Erebus and Terror appearing to be of the latter class, I requested my friend Mr. ARCHIBALD SMITH, Fellow of Trinity College, Cambridge, who in his academic course obtained the highest distinction conferred by the University, to draw out from M. Poisson's fundamental equations, applicable to induced magnetism, the most convenient and practical formulæ for computing the corrections of the three magnetic

* Since this communication was read to the Royal Society, Mr. Airy has favoured me with the following note:—"M. Poisson's deductions are founded on the assumption, that the phenomena of magnetism depend on the action of two fluids which attract each other, but which each repel other portions of fluid of the same kind: and that induction is caused by an alteration in the arrangement of these fluids among the particles of iron, produced by the attraction and repulsion of the earth's magnetic fluids. His fundamental equations in common language may be stated as follows:—

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\begin{aligned} & \text{Horizontal force towards the} \\ & \text{ship's head, as disturbed,} \end{aligned} = A' \times \left\{ \begin{matrix} \text{Undisturbed horizontal} \\ & \text{force to ship's head} \end{matrix} \right\} + C \times \text{undisturbed vertical force.} \end{aligned} \begin{aligned} & \text{Horizontal force towards the} \\ & \text{ship's head, as disturbed,} \end{aligned} \end{aligned} = E' \times \left\{ \begin{matrix} \text{Undisturbed horizontal} \\ & \text{force to ship's side} \end{matrix} \right\} \end{aligned} \begin{aligned} & \text{Vertical force, as disturbed } \ldots = G \times \left\{ \begin{matrix} \text{Undisturbed horizontal} \\ & \text{force to ship's head} \end{matrix} \right\} + K' \times \text{undisturbed vertical force,} \end{aligned}
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"These equations are the same as those obtained by Mr. Airy in the Philosophical Transactions, 1839, the first and second being the same as the two equations in page 184, and the third being the same as the last of the group of three equations in page 181. Mr. Airy's expressions however imply that G is equal to C. The calculations in the sequel of this paper seem to show that in the Erebus G is greater than C. Mr. Airy's deductions are founded on the assumption that each particle of iron is converted, by the earth's magnetic action, into a magnet with its length parallel to the direction of terrestrial magnetism."

elements, for the use of nautical men, and of others who might be engaged in reducing magnetic observations made at sea. He has obligingly furnished me with the following memorandum:—

"At a given geographical position let φ represent the total magnetic intensity of the earth; θ the dip, which is considered positive when the north end of the needle dips below the horizontal plane, negative when it inclines above it; ζ the azimuth of the ship's head, or the angle between the principal section of the ship and the magnetic meridian, which is considered positive when the ship's head is to the west of the magnetic north, negative when to the east. Let $\varphi', \theta', \zeta'$, be the values of the same elements shown by a needle whose centre is at a given place in the ship, when affected by the magnetism induced in the soft iron of the ship by the magnetism of the earth. M. Poisson has shown that if the dimensions of the needle are very small compared to its distance from the iron by which it is affected, the following equations are true;

$$\varphi' \cos \theta \cos \zeta' = \varphi \left[A' \cos \theta \cos \zeta + B \cos \theta \sin \zeta + C \sin \theta \right],$$

$$\varphi' \cos \theta' \sin \zeta' = \varphi \left[D \cos \theta \cos \zeta + E' \cos \theta \sin \zeta + F \sin \theta \right],$$

$$\varphi' \sin \theta' = \varphi \left[G \cos \theta \cos \zeta + H \cos \theta \sin \zeta + K' \sin \theta \right].$$

"In these equations, A', B, C, D, E', F, G, H, K' are constants which depend only on the distribution of the iron in the ship relatively to the position of the needle and the plane of the horizon, and which continue the same for every geographical position of the ship, while the distribution of the iron within the ship, and the inclination of the ship to the horizon, remain the same.

"If the centre of the needle is placed in the principal section of the ship, and the iron is symmetrically distributed on each side of that section, it will easily be seen that for values of ζ equal in magnitude and opposite in sign, the corresponding values of ζ' are equal in magnitude and opposite in sign, and the corresponding values of φ' and θ' are respectively equal in magnitude and the same in sign. These results necessarily imply that B, D, F and H are equal to zero. The equations in this case become

$$\varphi' \cos \theta' \cos \zeta' = \varphi \left[A' \cos \theta \cos \zeta + C \sin \theta \right],$$

$$\varphi' \cos \theta' \sin \zeta' = \varphi \cdot E' \cos \theta \sin \zeta,$$

$$\varphi' \sin \theta' = \varphi \left[G \cos \theta \cos \zeta + K' \sin \theta \right].$$

"If we divide each term by φ A' and put $\frac{C}{A'}=a$, $\frac{E'}{A'}=b$, $\frac{G}{A'}=c$, $\frac{K'}{A'}=d$,

$$\frac{\varphi'}{\Lambda'\overline{\varphi}}\sin\theta' = c\cos\theta\cos\zeta + d\sin\theta. \qquad (3.)$$

"From these equations are derived the following:-

$$\frac{\varphi'}{\Lambda'\varphi'}\cos\theta' = (\cos\zeta\cos\zeta' + b\sin\zeta\sin\zeta')\cos\theta + a\cos\zeta'\sin\theta, . . . (4.)$$

and representing $\zeta - \zeta'$, or the deviation by δ ,

$$= \frac{2a}{1+b} \tan \theta \sin \zeta' + \frac{1-b}{1+b} \sin (\zeta + \zeta') \quad . \quad . \quad . \quad . \quad (7.)$$

$$c\cos\zeta + d\tan\theta = b\sin\zeta\csc\zeta'\tan\theta' (9.)$$

$$\tan \theta' = \frac{c}{b} \cdot \left(\cos \zeta + \frac{d}{c} \tan \theta\right) \sin \zeta' \csc \zeta \quad . \quad . \quad . \quad (12.)$$

$$= c \cdot \frac{\cos \zeta + \frac{d}{c} \tan \theta}{\sqrt{(\cos \zeta + a \tan \theta)^2 + b^2 \sin^2 \zeta}}. \qquad (14.)$$

"From these equations, and observations made at one geographical position with the ship's head on different azimuths, the constants a, b, c, d, A' may be determined, and the corrections of the affected elements at any other geographical position may be calculated.

"a and b may be determined from observed deviations of the compass needle by means of equation (5.). A table of the deviations on each affected or compass course, and of the true magnetic course for each affected or compass course, may then be calculated by equations (6.) or (7.). In these equations ζ , which is an unknown quantity, occurs in the second term on the right-hand side; but the term is so small that an approximate value of ζ may be used, and the error caused thereby neglected. This error is least in equation (7.), which is also the most convenient for calculation except on east and west courses.

"To find the compass course for each true magnetic course, it will generally be sufficient to apply the deviations corresponding to the nearest true magnetic courses contained in the Table last described; but if the deviations are large, it will be better to construct a separate table by means of equation (8.).

"c and d may be determined from the true dip and the affected dips observed on different courses by means of equation (11.), or more easily by means of (9.) and (10.); observing that the values of ζ employed should be not observed values, but tabular

values calculated in the manner described above. A table of the affected dip, and of the dip corrections on each course, may then be calculated from (14.), or more easily from (12.) and (13.); observing that (12.) must not be used when the ship's course is nearly north or south, and that (13.) must not be used when the ship's course is nearly east or west, and that the values of ζ should be tabular, not observed.

"The constants may also be determined from observations of the total intensity, by means of the first four equations, and tables for the correction of the observed intensities may be constructed by means of these equations. For this purpose, equation (3.) should be used when the dip is large, and the others when the dip is small.

"The values of a and b may be determined very readily, and probably with great accuracy, from observations of the horizontal intensity with the ship's head on the four principal compass courses. For if H_n , H_w , H_s , H_e represent the values so observed, then

"If observations are made at equal intervals of time with the ship's head successively on the N., W., S., E., and N. points, the values of a and b thus determined will be independent of any regular increase or diminution of the intensity. If n, w, s, e represent the number of vibrations in equal times, on the four principal courses, of the same horizontal needle, beginning to vibrate in the same arc, and corrected for temperature alone,

$$b = \frac{w^2 + e^2}{2 n s}. \qquad (18.)$$

"The true declination may be found independently of the dip and of the constant a, by means of observations of the true azimuth of the ship's head on two courses. Let ψ represent the declination, which is considered positive when the north end of the needle is to the west of the true north, ω the true azimuth of the ship's head, which is positive when the ship's head is to the west of the true north; so that $\zeta = \omega - \psi$. And let ω_1, ζ'_1 and ω_2, ζ'_2 represent the observed values of ω and ζ' on the two courses,

$$\tan\left(\psi - \frac{\omega_1 + \omega_2}{2}\right) = \frac{b\sin\left(\zeta'_1 + \zeta'_2\right)}{2\sin\zeta'_1\sin\zeta'_2 - b\sin\left(\zeta'_1 - \zeta'_2\right)\cot\frac{\omega_1 - \omega_2}{2}}.$$

"If the observations are made with the ship's head on exactly opposite courses, $\omega_1 - \omega_2 = 180^{\circ}$; and we have

$$\tan (\omega_1 - \psi) = \frac{2 \sin \zeta'_1 \sin \zeta'_2}{b \sin (\zeta'_1 + \zeta'_2)};$$

if at equal azimuths on each side of the magnetic north,

$$\psi = \frac{\omega_1 + \omega_2}{2}.$$

"The formula fails if $\zeta'_1 + \zeta'_2 = 180^\circ$, the denominator becoming zero; the true value of $\tan \left(\psi - \frac{\omega_1 + \omega_2}{2} \right)$ in that case is

$$\frac{b}{\sin 2 \zeta_1' + b \cos 2 \zeta_1' \cot \frac{\omega_1 - \omega_2}{2}}.$$

Corrections for the Erebus.—We will seek in the first instance the values of the constants a and b, because they are those which can be obtained with the greatest degree of exactness, being derived from observations with the compass needle, which are made with greater precision than those with the inclination or intensity needles. Before the Expedition quitted England, a suitable position in the midship line was chosen for magnetic observations on board ship, and the effect of the ship's attraction on a standard compass placed in that spot, was ascertained by observations with the ship's head turned successively on each of the thirty-two principal points. This was done in September 1839 at Gillingham near Chatham, where θ , or the Inclination, was at that epoch 69° 05'*.

The observations in the Erebus gave results as follows:—

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N. by w. N.N.W. N.W. by N. N.W. N.W. by W. W.N.W. W. by N.	$ \begin{vmatrix} +\mathring{0} & 0\acute{6} \\ +1 & 12 \\ +2 & 01 \\ +2 & 10 \\ +3 & 03 \\ +3 & 28 \\ +3 & 51 \\ +4 & 09 \end{vmatrix} $	w. w. by s. w.s.w. s.w. by w. s.w. s.w. s.w. s.s.w. s.s.w. s.s.w.	+4 19 +4 40 +4 03 +3 24 +2 45 +2 08 +1 34 +0 52	s. by E. s.s.e. by s. s.e. s.e. by e. e. s.e. by e. e. e.s.e. e. by s.	+ 0 28 -0 19 -0 48 -1 23 -1 53 -2 21 -2 50 -3 17	E. by N. E.N.E. N.E. by E. N.E. by N. N.N.E. N. by N.	-3 42 -4 53 -3 46 -3 18 -2 59 -2 16 -1 39 -0 49

We perceive by this Table that, allowance being made for slight irregularities in the observations, the masses of iron which acted on the compass needle of the Erebus in its standard position were distributed symmetrically, or very nearly so, on either side of the vertical plane, passing through the longitudinal midship section. We may therefore safely employ, in computing the corrections, the more simple formulæ which are applicable under this condition.

To obtain the constants a and b of these formulæ we may arrange equations on the several points, from the observations in the Table, of the form

$$\cos \zeta \sin \zeta' - b \sin \zeta \cos \zeta' = -a \tan \theta \sin \zeta'.$$

^{*} Reports of the British Association, 1838.

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N. by W.
                             1905 - 2115 b = - 0.510 a
                N.N.W.
                             3482 - 3834 b = - 1001 a
               N.W. by N.
                            4481 - 4916b = -1454a
                 N.W.
                            4727 - 5258 b = -1850 a
              N.W. by W.
                           4193 - 4798 b = -2.175 a
                N.N.W.
                            2954 - 3626 b = -2417 a
               W. by N.
                           1212 - 1936 b = -2.566 a
                         +2.2954 - 2.6483 b = -11.973 a.
                                                           . . . (1.)
                W. by S. -.2689 + .1876 b = -.2566 a
                W.S.W. - \cdot 4130 + \cdot 3423 b = - \cdot 2\cdot 417 a
              S.W. by W. - .5021 + .4427 b = - .2.175 a
                        -5233 + 4754 b = -1850 a
               S.W. by S. - .4729 + .4359 b = - 1.454 a
                S.S.W. - .3574 + .3301 b = - 1.001 a
                S. by W. - .1919 + .1768 b = - .0.510 a
                         -2.7295 + 2.3908 b = -11.973 a.
                                                                     (2.)
                S. by E.
                            1915 - 1860 b = 0.510 a
                 S.S.E.
                            3563 - 3366 b = 1.001 a
               S.E. by S.
                            4693 - 4451 b = 1.454 a
                  S.E.
                            .5161 - .4832 b = 1.850 a
               S.E. by E.
                            4900 - 4489 b = 2.175 a
                 E.S.E.
                            3953 - 3459 b = 2.417 a
                            2462 - 1888 b = 2566 a
                E. by S.
                         + 2.6647 - 2.4345 b = 11.973 a.
                                                         . . . . (3.)
                E. by N. - .1088 + .1939 b = 2.566 a
                E.N.E. - .2967 + .3625 b = 2.417 a
               N.E. by E. -.4214 + .4789 b = 2.175 a
                 N.E.
                        - .4732 + .5252 b = 1.850 a
               N.E. by N. - \cdot 4494 + \cdot 4888 b = 1.454 a
                N.N.E.
                       -3492 + 3780 b = 1.001 a
                N. by E. -1908 + 2050 b = 0.510 a
                         -2.2895 + 2.6323 b = 11.973 a.
                                                        \ldots \qquad \ldots \qquad (4.)
From (1.) and (4.), changing the signs of (1.) and summing, we have
                -4.5849 + 5.2806 b = +23.946 a. . . . .
                                                                     (5.)
From (2.) and (3.), changing the signs of (3.) and summing, we have
                -5.3942 + 4.8253 b = -23.946 a; \dots \dots \dots
                                                                     (6.)
                   whence 10.1059 b = +9.9791; and b = +.9875;
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From (5.) and (6.), changing the signs of (6.) and summing, we have

$$47.892 a = .4553 b + .8093;$$
 $a = + .0263.$

We have also the equations at east and west;

East
$$2.617 a = +.0645$$

West . . . $-2.617 a = -.0753$;

whence

$$a = \frac{\cdot 1398}{5 \cdot 234} = + \cdot 0267$$
;

or including the observations at east and west in the general sum, we have a = +.0264.

After the arrival of the Expedition at Hobarton, and before it sailed to the Antarctic Circle, a similar series of observations was made in the Erebus, on the 29th October 1840, and again repeated on her return to Hobarton the following autumn, viz. on the 29th June 1841. The south end of the needle being now the one which dipped below the horizon (θ being -70° 40'), the deviation of the compass was found to take place in the contrary direction to that which had been observed at Gillingham, the disturbance being towards the west as the ship's head went round from north by east to south, and towards the east as her head passed from south through west to north.

The line of no deviation was not found to correspond accurately with the north and south points of the compass on either of the occasions at Hobarton, but in 1840 coincided more nearly with the north by west and south by east, and in 1841 with the north by east and south by west. We may perhaps ascribe with probability irregularities of this nature to slight modifications in the distribution of the iron at different periods, which we cannot but view as of not unlikely occurrence; for example, such as might be occasioned by the ship being secured at different times by the starboard or the larboard chain cable. In looking through the observations of the Erebus, it is evident that there was no systematic or constant deviation of the plane of the ship's attraction from that of her principal section; but that the points of no disturbance were sometimes a little on the one side, and sometimes a little on the other, of the north and south points. It appears, therefore, not improper to class these irregularities with those others of accidental occurrence which occasion small discordances in partial results, and are usually ranged under the general technical head of errors of observation.

If, further, we compare generally the deviations in 1840 with those of April 1841, the latter appear systematically rather the more considerable in amount. Viewed as a single fact, this circumstance might be regarded simply as indicating that some change had taken place in the interim in the arrangement and distribution of the ship's iron, and an easy and natural explanation might appear to be afforded. It is however one of several facts which have presented themselves in the course of a careful examination of the observations of the first two years of Captain Ross's expedition, which seem to point to the possibility of a somewhat different cause, viz. that when

a ship changes her magnetic latitude, the corresponding change in the magnetism of the ship, or more strictly in that portion of it which is derived from induction, follows, but does not always, or altogether, take place instantaneously. It would accord with this supposition, that the disturbance of the compass should be less in the Erebus on her first arrival at Hobarton in 1840, than on her return there in 1841, because in 1840 she had recently passed through the lowest magnetic latitudes, and in 1841 she came immediately from the highest. The observations in 1840 give a less value for a tan θ than those of 1841, and taking the dip at Hobarton as the value of θ , to which the induced magnetism of the ship on both occasions should strictly correspond, we should have a less value for a in 1840 than in 1841; whereas if with the same dip we take a mean between the disturbances of the compass on the first arrival and on the return, by which we may be conceived to neutralize in a great measure the temporary influences which have been supposed, we find the value of ato be almost identical with the result of the former experiments at Gillingham. From this accordance in the value of the constant in dips which differ so greatly as from $+69^{\circ}$ to -70° , we should infer the probability,—first, that the local attraction of the Erebus was due to induced magnetism alone, the influence of any portions of iron which, in the strict sense of the term, were permanently magnetic, being insensible; and secondly, that no material change affecting the standard compass had taken place in the distribution of her iron. These inferences are by no means inconsistent with the supposition above suggested, that some portions of her iron might be of a quality intermediate between that of perfectly soft iron which undergoes instantaneous change, and that of iron which acquires permanent magnetism, and that such portions should be liable, in regard to their magnetic condition, to be more or less in arrear of the ship's magnetic position. I abstain from entering further into this question at present, because a fitter opportunity of doing so will be afforded when the whole of the observations of the Expedition shall be collected, including those which have yet to be made at Rio de Janeiro on the return from the high latitudes of the south, and in England after passing through the low magnetic latitudes of the equatorial region. Should it prove that the induced magnetism of a ship due to any particular dip requires time for its full development, more or less according to the various quality of her iron, the corrections to be applied may possibly in some ships be considerably complicated thereby: fortunately in the Erebus the difference in the amount of the disturbance on the two occasions at Hobarton, which gave rise to this discussion, is not of any serious consequence; and we may employ without any material inconvenience for our present purpose the mean of the two series as applicable generally between their respective dates, for which interval we specially desire the corrections.

Ship's head	Disturba	Disturbance towards the west. Ship's head Disturbance towards th					the west.
by compass.	1840.	1841.	Mean.	by compass.	1840.	1841.	Mean.
N. by w. N.N.W. N.W. by N. N.W. by w. W.N.W. W. by N. W. by S. W. s.W. S.W. by S. S.S.W. S. by W.	+ 1 10 +0 24 -0 40 -1 54 -2 10 -2 58 -3 18 -3 39 -4 15 -4 13 -4 27 -4 39 -4 06 -3 36 -2 30 -1 39	-0 26 -1 14 -2 01 -2 34 -2 55 -3 13 -3 51 -4 32 -4 59 -4 56 -4 41 -2 50 -2 15 -0 19	+ 0 22 -0 25 -1 20 -2 14 -2 32 -3 05 -3 35 -4 06 -4 37 -4 35 -4 34 -4 29 -3 53 -3 13 -2 22 -0 59	s. by E. s.s.e. by s. s.e. by e. e.s.e. by s. e. by s. e. e. by n. e. n.e. by n. n.n.e. n.by e.	-0 49 -0 01 +0 38 +1 12 +1 35 +2 35 +3 17 +3 12 +3 38 +3 50 +3 21 +2 26 +2 19	+0 43 +2 32 +3 06 +3 51 +4 34 +5 01 +4 45 +5 21 +5 07 +4 46 +3 45 +3 08 +2 39 +1 30 +0 38	-0 03 +1 15 +1 52 +2 32 +3 04 +3 48 +4 01 +4 17 +4 22 +4 20 +3 48 +3 33 +3 10 +2 45 +1 58 +1 28

Employing the same formula as before, and forming equations from the observations on the twenty eight points, being all the points excepting the north, south, east and west, we obtain

$$10.1036 b = + 9.9673$$

 $b = + .9865$:

and from the sum of the thirty equations, including those at east and west, we have

$$+57.89 a = +1.0439 + .537 b,$$

$$a = \frac{1.0439 + .5297}{57.89} = +.0272.$$

On the passage from Hobarton to the Antarctic Circle, the Expedition stopped at Auckland Island for the purpose of observing on the term day of November 1840. The Erebus was not swung at this station, but with the value of θ observed on shore -73° 10', and the declination observed on board whilst at anchor, with the ship's head on the east and west points, and on the E.N.E. and W.N.W. points, we may obtain a satisfactory value for α . On the supposition of the symmetrical distribution of the iron on either side of the longitudinal midship section, the deviation occasioned by it should be the same in amount, but with opposite signs, at east and west, and also at E.N.E. and W.N.W.; the amount, however, being slightly different at east and west from that at E.N.E. and W.N.W.

From the observations at east and west we have

$$\psi' = -12^{\circ} 52'$$
 at east, and $\psi' = -22^{\circ} 55'$ at west;
 $\psi = \frac{\psi' + \psi'}{2} = -17^{\circ} 53' \cdot 5$, and
 $\delta = \pm 5^{\circ} 01' \cdot 5$; whence $a = +0265$.

From the observations at E.N.E. and W.N.W.,

$$\psi' = -13^{\circ} 36'$$
 at E.N.E., and $-22^{\circ} 06'$ at W.N.W.; $\psi = -17^{\circ} 51'$; $\zeta' = 67^{\circ} 30'$, and $\zeta = 63^{\circ} 15'$; whence $a = .0261$.

The mean of the two pairs of observations gives a = +.0263.

Whilst within the Antarctic Circle only a single opportunity occurred of observing the inclination otherwise than on board, and thus of obtaining a from a tan θ by having an assured value of θ . This was on the 8th of January 1841, in lat. $-68^{\circ}30'$, long. 176° 35′, where the inclination observed on the ice with a needle in which the observation was complete by the reversal of the poles, was found to be $-83^{\circ}.35'$. The declination was observed on board on the same afternoon and following morning, as nearly as could be in the same geographical position, with the ship's head on several points, from which we may select for a determination of a those nearest to the east and west points. We have then the following observations:—

1. At W.
$$\frac{3}{4}$$
 N. $\psi = -\stackrel{\circ}{46} \stackrel{\circ}{02}$ 4. At E. $\frac{3}{4}$ N. $\psi = -\stackrel{\circ}{20} \stackrel{\circ}{51}$
2. At W. by S. $\psi = -\stackrel{\circ}{46} \stackrel{\circ}{32}$ 5. At E. by S. $\frac{1}{2}$ S. $\psi = -\stackrel{\circ}{19} \stackrel{\circ}{58}$
3. At W. by S. $\frac{1}{2}$ S. $\psi = -\stackrel{\circ}{47} \stackrel{\circ}{17}$ 6. At E. by S. $\frac{3}{4}$ S. $\psi = -\stackrel{\circ}{20} \stackrel{\circ}{22}$

4. At E.
$$\frac{3}{4}$$
 N. $\psi = -20^{\circ}$ 5

2. At W. by S.
$$\psi = -46 32$$

5. At E. by S.
$$\frac{1}{3}$$
 S. $\psi = -19$ 58

3. At W. by S.
$$\frac{1}{2}$$
 S. $\psi' = -47$ 17

6. At E. by S.
$$\frac{2}{4}$$
 S. $\psi = -20$ 22

From 1. and 4. we have
$$\psi = \frac{\psi' + \psi'}{2} = -33 \ 27.5$$

From 3. and 5. we have $\psi = \frac{\psi' + \psi'}{2} = -33 \ 37.5$ Mean $-33 \ 32.5$.

Hence

$$\delta_1 = -\stackrel{\circ}{12} \stackrel{\circ}{29} \cdot 5$$
 $\delta_2 = -12 \cdot 59 \cdot 5$
 $\delta_3 = -13 \cdot 44 \cdot 5$
 $\delta_4 = +\stackrel{\circ}{12} \cdot 4\stackrel{\circ}{1} \cdot 5$
 $\delta_5 = +13 \cdot 34 \cdot 5$
 $\delta_6 = +13 \cdot 10 \cdot 5$;

and having thereby the values of ζ , as we have those of ζ' by observation, we obtain

$$a_1 = + .0249$$
 $a_4 = + .0259$ $a_5 = + .0274$ $a_5 = + .0266$ $a_6 = + .0266$

Means . . . $+ .0266$ $+ .0267$

The deviation of the compass observed on board the Erebus during the stay of the Expedition at Christmas Harbour, Kerguelen Island, in July 1840, when the ship's head was on the N.E., S.E., N.W., and S.W. points, and at the points on either side of those points, viz. N.E. by N., N.E. by E., S.E. by S., S.E. by E., &c., will furnish an additional determination of the value of b:

	δ.	ζ′.	ζ.
n.w. by n.	-2·12	33 45	31 33
n.w.	-2·07	45 00	42 53
n.w. by w.	-2·42	56 15	53 33
s.w. by w.	-3·52	123 45	119 53
s.w.	-3·28	135 00	131 32
s.w. by s.	-2·38	146 15	143 37
s.e. by s.	$ \begin{array}{r} +245 \\ +3.16 \\ +3.47 \end{array} $	213 45	216 30
s.e.		225 00	228 16
s.e. by e.		236 15	240 02
n.e. by e.	+2·08	303 45	305 53
n.e.	+2·05	315 00	317 05
n.e. by n.	+1·27	326 15	327 42

Employing these values of ζ' and ζ in the formula

$$\cos \zeta \sin \zeta' - b \cos \zeta' \sin \zeta + a \tan \theta \sin \zeta' = 0,$$

and eliminating $a \tan \theta \sin \zeta'$, we have

$$5.7471 \ b = 5.6233; \ b = .9785.$$

Collecting now in one view the values of a, we have as follows:—

- 1. From the observations at Gillingham near Chatham a = + .0264
- 2. From the observations at Hobarton a = +.0272
- 3. From the observations at Auckland Island . . . a = +.0263
- 4. From the observations in lat. $-68^{\circ}30'$, long. $176^{\circ}35'$ a = +.0267

From this near accordance in the values of a, obtained in dips varying from $+69^{\circ}05'$ to $-83^{\circ}35'$, we are warranted in regarding the local attraction in the Erebus as due to induced magnetism; and in employing the formulæ derived from M. Poisson's fundamental equations, which are based on the hypothesis of induced magnetism only, in computing corrections for the observations made on board that ship.

For the value of b we have

From the observations at Gillingham b = + .9874From the observations at Hobarton b = + .9865From the observations at Kerguelen Island . . . b = + .9785Mean . . . + .9841

With these values of a and b, a table of double entry was formed, having for arguments ζ' and θ ; ζ' being the compass direction of the ship's head when an azimuth was observed, and θ the inclination taken from the chart formed from the observations of that element on board ship, corrected in the manner that will be shown hereafter; the corrections for the ship's local attraction in the general Table of Declinations observed in the Erebus have been taken from the Table thus formed.

In geographical positions, where the inclication made a very near approximation to -90°, and when azimuths observed on the same day at places sufficiently near to each other included observations on the east and west points, or on points but little removed from them, on which the corrections for the deviation might have the same, or nearly the same, value, but with opposite signs, the inclination with which the corrections have been computed has been derived from the azimuths themselves in preference to being taken from the chart. In such cases, and when a and bhave been elsewhere satisfactorily determined for the ship, the amount of disturbance which her iron produces on the compass needle furnishes itself a measure of the inclination, exceeding in precision that of the dipping needle used on board. If the ship's magnetism should have already conformed to the terrestrial dip, the inclination corresponding to the disturbance of the compass is that belonging to the geographical position, and the ship herself, with merely her compass needle, would become in such rare situations an inclinometer of great delicacy. But if the change in the magnetism of the ship from that due to a former magnetic locality be not yet fully developed, the inclination thus furnished by the compass needle is on that account also preferable to that which might be taken from the chart, or to the dip observed with the dipping needle either on board or on shore, for the correction of other azimuths observed at the same time. Whenever the inclination used for the declination corrections has been thus derived, a notice is annexed in its proper place in the general table. It may be useful to give an example, and I select for that purpose the observations on the afternoon of the 16th February 1841, when, from the amount of the declination (-112° or -113°), the Expedition had without doubt penetrated to the south of the latitude of the magnetic pole; the particular observations are as follow:-

Latitude.	Longitude.	Ship's head.	Declination observed. ψ .
-76 35 -76 36 -76 36 -76 36 -76 36 -76 36 -76 36 -76 37 -76 37 -76 37 -76 37	166 17 166 16 166 16 166 16 166 16 166 17 166 17 166 16 166 16	E. by s. ½ s. N.N.W ½ W. N.W. by N. W. by s. ½ s. s.W. ¼ W. s.W. by N. s.W. ¼ s. E. by s. E. by s. E. by s. E. s.E. S.E. by E.	-158 51

From the observations at W., and E. by S., we have the approximate values of $\psi = \frac{\psi' + \psi'}{2} = -113^{\circ} \, 01'$; δ at W. = $-45^{\circ} \, 50'$; $\tan \theta = \frac{\sin \delta}{.0267}$; whence $\theta = -87^{\circ} \, 52'$.

With this approximate inclination we compute δ at E. by S. = $+45^{\circ}$ 04'; and with this correction, and the same observations as before, we have more precisely

$$\psi = -112^{\circ} 38'$$
; δ at W. = $-46^{\circ} 13'$; and $\theta = -87^{\circ} 53'$.

Substituting this value of θ in the formula

$$\sin \delta = \frac{2 a}{1+b} \tan \theta \sin \zeta' + \frac{1-b}{1+b} \sin (\zeta' + \zeta),$$

we have the corrections and the corrected declination as follows:-

```
E. by S. \frac{1}{9} S. Correction -4\hat{6} 0\hat{3}; \psi = -6\hat{4} 2\hat{3}; \psi = -10\hat{8} 2\hat{6}
N.N.W. \frac{1}{2} W. Correction + 19 46; \psi = -136 19; \psi = -116 33
              Correction + 41 38; \psi = -150 \ 04; \psi = -108 \ 26
  N.N.W.
N.W. by N. Correction + 23 31; \psi = -138 24; \psi = -114 53
              Correction + 46 13; \psi = -158 51; \psi = -112 38
    W.
W. by S. \frac{1}{2} S. Correction + 44 03; \psi = -156 58; \psi = -112 55
 S.W. \frac{1}{4} W. Correction + 33 04; \psi = -156 05; \psi = -123 01
S.W. by W. Correction +37\ 32; \psi = -154\ 06; \psi = -116\ 34
             Correction + 29 45; \psi = -14254; \psi = -11309
 S.W. \frac{1}{4} S.
  E.N.E.
             Correction -41\ 38; \psi = -67\ 01; \psi = -108\ 39
             Correction -45\ 19; \psi = -66\ 32; \psi = -111\ 51
  E. by S.
             Correction -45\ 19; \psi = -67\ 53; \psi = -113\ 12
  E. by S.
             Correction -42\ 18; \psi = -73\ 45; \psi = -116\ 03
   E.S.E.
 S.E. by E.
             Correction -37\ 32; \psi = -73\ 40; \psi = -111\ 12
                                                 Mean . . . - 113 23
```

On comparing the values of ψ thus obtained from the observations on the easterly points, with those on the westerly points, it is evident that the remaining differences in the individual results are not occasioned by faults in the corrections, but that they are actual differences in the observations of azimuth. In the extreme circumstances to which the Expedition had attained, when by reason of the great amount of dip, the terrestrial force acting on the compass needle, and directing it to one part of the horizon in preference to another, was reduced to $\frac{1}{27}$ th part of the whole amount of the terrestrial magnetic force in the same locality, the degree of accordance which was still preserved assuredly surpasses expectation*. The result at S.W. $\frac{1}{4}$ W. is the only one which presents an excessive discordance; and after a careful examination of the whole of the observations which the general table contains, it must be regarded

^{*} The compass used in the Erebus was the first of the new naval compasses made under the direction of a Committee appointed by the Admiralty "for the improvement of ships' compasses." The magnet was composed of several thin plates of clock-spring suitably arranged, giving very considerable magnetic force, with a suspension improved both in mode and materials. This compass appears to have answered remarkably well in the very trying circumstances in which it was employed. Captain Ross was himself the Chairman of the Committee, which gave its services gratuitously: the other members were Captain Beaufort, R.N., Mr. Christie, Major Jervis, Captain Edward Johnson, R.N., and Lieut.-Colonel Sabine.

as a case of very unusual observation error. Were we to omit this result, the mean would become -112° 39'. When the corrections for local attraction become so great, it is necessary to be very accurate in noting the direction of the ship's head at the same instant that the azimuth is observed, as at the points where the changes of δ for changes of ζ' are very great, an error of a degree in the direction of the ship's head will make nearly the same error in the correction; on such occasions therefore the result is liable to an additional source of observation error of serious magnitude.

We have seen that when the inclination is -87° 53', the sum of the deviations at east and west amounted to 92° 26'; with 10' increase in the dip, their joint amount would have become 126° 52'. The scale which the compass needle presents for the deduction of the inclination is consequently a very large one, when the inclination is so great as that which we are now considering; and it continues to increase in magnitude, until the compass ceases altogether to indicate the direction of the horizontal component of the terrestrial force, and points unchangingly, under every alteration of the ship's head, to the direction of the general resultant of the ship.

The terrestrial dip observed with a dipping-needle on board on the 16th of February, and corrected for the ship's attraction, was -88° 20'; that corresponding to the magnetism of the ship was, as we have seen, -87° 53', being a little in arrear, in a magnetic sense, of her then position.

For the constants c and d in the formula for the correction of the inclination, we have to take into account, in the first instance, a series of observations of the inclination with the ship's head successively on the sixteen principal points of the compass, made on board the Erebus at Hobarton in November 1840, before her departure for the Antarctic Circle, and a similar series made at the same place in June 1841 on her return from the south. The inclination observed on shore was -70° 40'.

Ship's head	Inclination observed. Ship's head Inclinat				clination obs	erved.	
by compass.	1840.	1841.	Mean.	by compass.	1840.	1841.	Mean.
N. N.N.W. N.W. W.N.W. W.S.W. S.W.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r rrrr} -72 & 00 \\ -71 & 45 \\ -71 & 24 \\ -70 & 55 \end{array} $		S. S.S.E. S.E. E.S.E. E. E.N.E. N.E.	$\begin{array}{ccccc} -69 & 49 \\ -70 & 00 \\ -70 & 22 \\ -70 & 45 \\ -70 & 58 \\ -71 & 33 \\ -71 & 35 \\ -71 & 42 \end{array}$	$ \begin{array}{r rrrr} -69 & 41 \\ -70 & 04 \\ -70 & 33 \end{array} $	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$

Employing for the observations between N.N.W. and S.S.W., and N.N.E. and S.S.E. the formula

$$c\cos\zeta + d\tan\theta = b\sin\zeta\csc\zeta'\tan\theta'$$
,

and for the other points

$$c\cos\zeta + d\tan\theta = (\cos\zeta + a\tan\theta)\sec\zeta'\tan\theta'$$
,

and using the values of ζ computed by means of the constants a and b already determined, we have the following equations:—

N.
$$+1.0000 c - 2.850 d = -2.830$$

N.N.W. $+ .9327 c - 2.850 d = -2.845$
N.W. $+ .7351 c - 2.850 d = -2.868$
N.S.W. $+ .4418 c - 2.850 d = -2.864$
W.S.W. $- .3139 c - 2.850 d = -2.864$
W.S.W. $- .3139 c - 2.850 d = -2.889$
S.W. $- .6617 c - 2.850 d = -2.889$
S.W. $- .6617 c - 2.850 d = -2.889$
S.W. $- .6617 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$
S.W. $- .9110 c - 2.850 d = -2.889$

Summing these equations, c is eliminated, and $d = \frac{45 \cdot 917}{45 \cdot 604} = 1 \cdot 0069$; and changing the signs in the equations from W. to E.S.E. inclusive and summing, we have $c = \frac{+ \cdot 361}{9 \cdot 9924} = + \cdot 0361$.

A similar series of observations made at Auckland Island on the passage from Hobarton to the Antarctic Circle, furnishes values of c and d differing but slightly from the preceding. The inclination observed on shore was -73° 10'.

Ship's head by compass.	Inclination observed.	Ship's head by compass.	Inclination observed.
N. N.N.W. N.N.E. N.W. N.E. W.N.W. E.N.E. W.	-74 24 -74 34 -74 09 -74 16 -74 13 -74 08 -73 43 -73 32	S. S.S.W. S.S.E. S.W. S.E. W.S.W. E.S.E.	-72 00 -72 17 -72 05 -72 36 -72 38 -73 09 -73 02 -73 26

Treating these observations in a similar manner to those at Van Diemen Island, we obtain

$$c = + .045$$
; $d = + 1.0039$.

Giving double weight to the observations at Hobarton, as representing a double series, we have c = +.039; and d = +1.006.

With these values of the constants in the formulæ

$$\tan \theta' = \frac{c}{b} \left(\frac{d}{c} \tan \theta + \cos \zeta \right) \sin \zeta' \csc \zeta$$
, from N.E to S.E., and from N.W. to S.W.

$$\tan \theta' = c \frac{\left(\frac{d}{c} \tan \theta + \cos \zeta\right) \cos \zeta'}{a \tan \theta + \cos \zeta} \text{ on other points,}$$

a table of double entry was formed for the corrections of the observations of in-

clination in the Erebus, having for arguments θ and ζ' ; the corrections in the general Table of the inclination observations were thus obtained.

We may compute the value of the remaining constant A' from the variations of the magnetic intensity observed on board the Erebus at Hobarton with Mr. Fox's intensity apparatus, with the ship's head on the sixteen principal points of the compass; two series of such observations were made, one in October 1840 with needle R. F. 4, the other in July 1841 with needle R. F. 5; expressing the value of the intensity on shore by $1.82 = \varphi$, the several values on board ship are shown in the following Table:—

Ship's head by		Intensit	у.
compass.	October 1840.	July 1841.	Means.
N.	1.792	1.806	$1.799 1.799 = \varphi'$
N.N.E.	1.787	1.803	1.795 $1.835 = \emptyset'$
N.N.W.	1.807	1.818	1.81%
N.E.	1·789 1·803	$\substack{1.813\\1.816}$	$\left \begin{array}{c} 1.801 \\ 1.809 \end{array}\right\} 1.805 = \varphi'$
N.W. E.N.E.	1.816	1.821	1.010
w.n.w.	1.830	1.832	$\left \begin{array}{c} 1.818 \\ 1.831 \end{array}\right\} 1.8245 = \varphi'$
E.	1.828	1.823	1.826 $1.828 = \varphi'$
w.	1.832	1.829	1.830)
E.S.E.	1.830	1.829	$\left\{\begin{array}{c} 1.830 \\ 1.849 \end{array}\right\} 1.836 = \varphi'$
W.S.W.	1.848	1·837 1·853	1.842 \ 1.848 \ 1.848 \ 1.050
S.E.	1.842 1.862	1.855	$\left \begin{array}{c} 1.858 \\ 1.858 \end{array}\right 1.853 = \varphi'$
S.W. S.S.E.	1.858	1.859	1.050
S.S.W.	1.863	1.857	$\begin{vmatrix} 1.859 \\ 1.860 \end{vmatrix}$ $1.8595 = \varphi'$
s.	1.864	1.864	$1.864 1.864 = \varphi'$

Employing the formula

$$\frac{\Phi'}{A'\Phi}\sin\theta' = c\cos\theta\cos\zeta + d\sin\theta$$

with the values of θ' and ζ computed by means of the constants a, b, c and d, already deduced, and with the observed values of φ , θ , and φ' , we have A' as follows:—

We obtain the same result if we employ the observed values of θ' instead of the

computed values; in this case the inclination and total intensity being both furnished at the several points by observation with Mr. Fox's apparatus, we have the ratios of the horizontal intensity $\frac{\phi'\cos\theta'}{\phi\cos\theta}$ on board as follows:—

From which by the formula

$$H = A'(\cos \zeta \cos \zeta' + b \sin \zeta \sin \zeta' + a \tan \theta \cos \zeta'),$$

we have

At N.N.E. and N.N.W.
$$A' = \frac{0.9262}{0.9239} = 1.003$$

At N.N.E. and N.N.W. $A' = \frac{0.9308}{0.9270} = 1.004$
At N.E. and N.W. $A' = \frac{0.9340}{0.9374} = 0.996$
At E.N.E. and W.N.W. $A' = \frac{0.9608}{0.9555} = 1.006$
At E. and W. $A' = \frac{0.9838}{0.9917} = 0.992$
At E.S.E. and W.S.W. $A' = \frac{1.0084}{1.0122} = 0.996$
At S.E. and S.W. $A' = \frac{1.0432}{1.0433} = 0.999$
At S.E. and S.S.W. $A' = \frac{1.0615}{1.0673} = 0.994$
At S. $A' = \frac{1.0800}{1.0761} = 1.004$
 $A' = 0.999$ Mean.

The correction for the ship's attraction in the general table of the intensities observed in the Erebus, have been computed with this value of A' used in the formula A' \bar{c} $\left(\frac{d}{c}\tan\theta + \cos\zeta\right)\cos\theta$ cosec θ' ; θ being taken from the chart formed from the observations of the inclination, and θ' and ζ from the tables with the arguments θ and ζ' .

Deduction of the Constants in Her Majesty's Ship Terror.—For these we have, in the first place, the observations at Gillingham, in September 1839, as follows: $\theta = 69^{\circ} 05'$.

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N. by w. N.N.W. N.W. by N. N.W. h.W. by w. w.N.W. w. by N.	+0·11 +1·35 +2·31 +3·9 +3·58 +4·39 +5·8 +5·35	w. w. by s. w.s.w. s.w. by w. s.w. s.w. s.s.w. s.s.w. s.s.w. s. by w.	$+\overset{\circ}{5}\cdot55 \\ +5\cdot17 \\ +4\cdot39 \\ +3\cdot50 \\ +3\cdot8 \\ +2\cdot24 \\ +1\cdot38 \\ +0\cdot55$	s. by E. s.s.e. s.e. by s. s.e. s.e. by E. e.s.e. by E. e.s.e. by s.	$\begin{array}{c} -\mathring{0}\cdot 8 \\ -0\cdot 51 \\ -1\cdot 42 \\ -2\cdot 30 \\ -3\cdot 9 \\ -3\cdot 40 \\ -4\cdot 34 \\ -4\cdot 57 \end{array}$	E. by N. E.N.E. N.E. by E. N.E. by N. N.E. by N. N.N.E. N. Dy E. N. Dy E.	- 5.22 - 5.50 - 5.22 - 4.27 - 3.37 - 2.37 - 1.40 - 0.33

We perceive by this Table that the masses of iron acting on the compass needle of the Terror were distributed, as in the Erebus, symmetrically, or very nearly so, on either side of the vertical plane passing through the longitudinal midship section. Using the formula

$$\cos \zeta \sin \zeta' - b \sin \zeta \cos \zeta' = a \tan \theta \sin \zeta'$$

and forming equations for the several points, we have from the sum of those from N. by W. to W. by N., and from N. by E. to E. by N.,

$$-4.4516 + 5.3295 b = +23.946 a$$
;

and for the sum of the equations on the points from S. by W. to W. by S., and from S. by E. to E. by S.,

$$-5.5092 + 4.7551 b = -23.946 a$$

whence we derive b = +.9877, and a = +.0339; or including the observations at east and west a = .0343.

We have next to consider a similar series of observations made in the River Derwent, near Hobarton, in Van Diemen Island, on October 20th, 1840, soon after the first arrival of the Expedition at that station; they were as follows:—

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N. by w. N.N.W. N.W. by N. N.W. h.W. by W. W.N.W. w. by N.	+0 42.4 -0 23.6 -1 20.6 -2 20.6 -3 25.6 -3 56.6 -4 01.6 -4 06.6	w. by s. w.s.w. s.w. by w. s.w. s.w. by s. s.s.w.	-4 36·6 -4 44·6 -4 52·6 -5 22·6 -4 23·6 -3 31·6 -2 03·6 -1 37·6	s. by E. s.s.e. s.e. by s. s.e. s.e. by E. e.s.e. by E. e.s.e. by s.	-0 11.6 +0 52.4 +1 56.4 +2 38.4 +3 29.4 +4 00.4 +4 43.4 +4 28.4	N.E. by E. N.E. by N. N.N.E.	+4 24·4 +4 11·4 +4 07·4 +3 27·4 +3 02·4 +2 37·4 +2 11·4 +1 26·4

In the Terror, as in the Erebus, the disturbance had changed its sign in passing from the northern to the southern hemisphere: the symmetrical distribution of the MDCCCXLIII.

iron on either side of the principal axis of the ship continued as at Gillingham, the observations showing only those very small differences in the exact points of no disturbance, which have been remarked in the Erebus, and which we may be content to view as accidental differences. From these observations, pursuing the usual course, we obtain b=+.9873, and a=+.0292. Here also, as in the case of the Erebus, the observations on the first arrival at Hobarton give a somewhat less value for a tan θ than those at Gillingham. It is possible that a similar series of experiments may have been repeated in the Terror on the return to the same station in 1841, but no record of it has been received in England, and the observations of 1840 are expressly referred to, in a note appended to them, as furnishing the corrections for the declinations observed between the months of October 1840 and April 1841. I think it not improbable that if the ship were swung in 1841, the resulting value of a tan θ will prove, as in the Erebus, to be somewhat greater than in 1840, and that the mean value of a at Hobarton will thereby come into a closer accord with its value at Gillingham.

The practical effect of so small a difference is however unimportant, and I have taken a in round numbers for the declinations under consideration = + .030, and b = + .9875, and have computed with these values the Tables from which the corrections for the Terror's declinations have been taken.

Part of the materials required for the correction of the observations of inclination and intensity, made in the Terror during the voyage under notice, not having yet reached England, the deduction of the constants c, d, and A' for that ship has been postponed.

Index Correction of Needle R. F. 4 for the Observations of the Inclination in the Erebus.—The observations of the inclination at sea on board the "Erebus," were made with Mr. Fox's apparatus for determining the magnetic inclination and intensity, and one needle, R. F. 4, was used throughout the observations which are now under consideration. The poles were not reversed; the circle was used with the face east only, and the needle with its marked side towards the observer. An index correction is therefore required for all the sea observations, and must be sought by comparing the inclination shown by the same circle and needle when observed with in the same manner on shore, at stations where the inclination was otherwise determined in an independent and complete manner, viz. by needles of which the poles were reversed, and the needle and circle used in the eight ordinary positions.

The determinations of this description made by the Expedition at the Magnetic Observatory at Van Diemen Island in 1840 and 1841, at Auckland Island in November and December 1840, at Campbell's Island in December 1840, and on the ice in lat. -68° 28', long. 176° 32', on the 8th of January 1841,—furnishing the required comparison,—were as follows:—

Observations of the Inclination, with Needles whose Poles were reversed, made at the Magnetic Observatory in Van Diemen Island in 1840, 1841.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1840. September 12.	h m 11 00 A.M.	R G 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\left.\begin{array}{cccccccccccccccccccccccccccccccccccc$	
14.	11 20 а.м.	R G 2	$\begin{array}{c} \beta & -70 & 35.6 \\ \beta & -70 & 40.9 \end{array}$	$\left.\right\} -70 \ 38.2$	
21.	11 30 а.м.	R 4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\left.\right\} -70 \ 37.6$	
21.	1 30 р.м.	R 10	$\begin{array}{c} \beta & 70 & 49.8 \\ \alpha & -70 & 53.7 \\ \beta & -70 & 53.7 \end{array}$	$\left.\right _{2}^{2}$ -70 51.7	
22.	11 20 а.м.	R 6	$\begin{vmatrix} a & -70 & 46.5 \\ \beta & -70 & 45.2 \end{vmatrix}$	$\left \begin{array}{c} 1 \\ -70 \\ 45.8 \end{array} \right $	Needles belonging to H.M.S. Erebus.
22.	2 00 р.м.	R 7	$\begin{vmatrix} \alpha - 70 & 46.4 \\ \beta - 70 & 45.2 \end{vmatrix}$	$\left \begin{array}{c} -70 & 45.8 \end{array} \right $	
October 5.	11 00 а.м.	R 6	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \begin{array}{c} -70 & 43.2 \end{array} \right $	
5.	2 00 р.м.	R 7	$\begin{vmatrix} \alpha - 70 & 43.3 \\ \beta - 70 & 40.4 \end{vmatrix}$	$\left \frac{1}{2} - 70 \ 42.0 \right $	
15.	1	D 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right = 70 \ 51.2$	Needles belonging to Sir John Frank-
	11 00 а.м.	D 2	$\begin{vmatrix} \alpha - 70 & 08.4 \\ \beta - 71 & 06.4 \end{vmatrix}$	$\left \frac{1}{2} \right = 70 \ 37.4$	LIN.
	10 20 а.м.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right = 70 \ 38.3$	Needles belonging to H.M.S. Terror.
	11 00 а.м.	C 2	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right = 70 \ 37.7$	Streeties belonging to 11.11.5. Terror.
1841. April 14	. 11 20 а.м.	R 4	$\alpha - 70 38.6$	} -70 38.7	
14	2 00 р.м.	R 10	$\beta - 70 \ 38.8$ $\alpha - 70 \ 46.5$	$\left.\right _{-70\ 42.9}$	
15	. 10 50 а.м.	R 6	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\right\}$ -70 39.0	
15	. 3 30 р.м.	R 7	$\begin{array}{ c c c c c c } \beta & -70 & 43.3 \\ \alpha & -70 & 40.6 \\ 6 & 70 & 33.0 \\ \end{array}$	$\left.\right _{2}^{2}$ -70 37.2	Needles belonging to H.M.S. Erebus.
16	. 1 30 г.м.	RG1	$ \begin{vmatrix} \beta - 70 & 33.9 \\ \alpha - 70 & 34.4 \\ \beta - 70 & 38.2 \end{vmatrix} $	$\left.\right _{0}^{1}$	
17	11 20 а.м.	R G 2	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left \frac{1}{2} \right = 70 \ 37.3$	
24	11 00 а.м.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} - 70 \ 38.0 \right $	<u></u>
24	Noon.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	
24	2 00 р.м.	C 2	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right = 70 \ 34.4$	Needles belonging to H.M.S. Terror.
30	Noon.	C 1	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} - 70 \ 36.4 \right $	
30	Noon.	C 2	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right = 70 \ 39.5$	
May 10	2 20 р.м.		$\begin{vmatrix} \alpha - 70 & 46.6 \\ \beta - 70 & 39.1 \end{vmatrix}$	$\left \frac{1}{2} \right = 70 \ 42.9$	h
10		R 10	$\begin{vmatrix} \alpha - 70 & 53.9 \\ \beta - 70 & 34.0 \end{vmatrix}$	$\left \begin{array}{c} \\ \\ \end{array} \right = 70 \ 43.9$	
I	. 10 30 а.м.		$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \frac{1}{2} \right -70 \ 42.4$	·
ľ	3. 10 45 а.м.	1	$\begin{vmatrix} \alpha - 70 & 45.4 \\ \beta - 70 & 36.3 \end{vmatrix}$	$\left \frac{1}{2} \right -70 \ 40.9$	Needles belonging to H.M.S. Erebus.
18			$\begin{vmatrix} \alpha - 70 & 47.1 \\ \beta - 70 & 33.1 \end{vmatrix}$	$\left \frac{1}{2} - 70 \ 40.5 \right $	
June 21		1	$\begin{vmatrix} \alpha - 70 & 45.8 \\ \beta - 70 & 35.1 \\ \pi - 70 & 45.1 \end{vmatrix}$	$\left \frac{1}{2} - 70 \ 40.4 \right $	
	. 10 45 A.M.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left \right\} -70 \ 40.8$	J
				-70 40.7	General Mean.

Observations of the Inclination with Needles whose poles were reversed, made at the Magnetic Observatory at Auckland Island.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1840. November 23. 23. 23. 25. 27. December 4.	1 00 p.m. 2 40 p.m. 3 30 p.m. 11 00 A.m. 1 00 p.m. 3 00 p.m. 4 00 p.m.	R G 2 C 1 C 2	$\begin{array}{c} \alpha - \mathring{7}3 & \mathring{1}7 \cdot 9 \\ \beta - 73 & 08 \cdot 2 \\ \alpha - 73 & 14 \cdot 4 \\ \beta - 73 & 12 \cdot 4 \\ \alpha - 73 & 15 \cdot 7 \\ \beta - 73 & 12 \cdot 9 \\ \alpha - 73 & 14 \cdot 7 \\ \beta - 73 & 11 \cdot 6 \\ \alpha - 73 & 06 \cdot 6 \\ \beta - 73 & 17 \cdot 0 \\ \alpha - 73 & 04 \cdot 0 \\ \beta - 73 & 11 \cdot 6 \\ \alpha - 73 & 08 \cdot 7 \\ \beta - 73 & 02 \cdot 9 \\ \alpha - 73 & 08 \cdot 2 \\ \beta - 72 & 55 \cdot 5 \\ \end{array}$	<u>J</u>	Needles belonging to H.M.S. Erebus. H. M. S. Terror. H. M. S. Erebus. General Mean.

Observations of the Inclination with Needles whose poles were reversed, at Campbell Island.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
15.	10 30 A.M. 10 30 A.M. 11 00 A.M. Noon.	C 1 C 2 R 4 R 10 R 6 R 7	$\begin{array}{c} \alpha = 73 & 55.7 \\ \beta = 73 & 48.4 \\ \alpha = 73 & 51.2 \\ \beta = 73 & 43.4 \\ \alpha = 73 & 56.5 \\ \beta = 73 & 50.7 \\ \alpha = 74 & 01.5 \\ \beta = 73 & 57.2 \\ \alpha = 73 & 45.8 \\ \beta = 73 & 49.5 \\ \alpha = 73 & 49.5 \\ \beta = 73 & 53.3 \\ \end{array}$	$ \begin{cases} -73 & 47.3 \\ -73 & 50.6 \end{cases} $ $ \begin{cases} -73 & 59.4 \\ -73 & 47.7 \end{cases} $ $ \begin{cases} -73 & 51.4 \end{cases} $	Needles belonging to H.M.S. Terror. Needles belonging to H.M.S. Erebus. General Mean.

Inclination observed on Ice, in latitude — 68° 28′, longitude 176° 32′, with a Needle the poles of which were reversed.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. January 8.	h m 3 20 p.m.	R 4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\left.\begin{array}{c} \\ -83 \\ 35.6 \end{array}\right.$	H. M. S. Erebus.

The inclinations observed at the four preceding stations with needle R. F. 4, with the face of the circle east, and the marked side of the needle facing the observer, were as follows:—

```
Van Diemen Island -\mathring{7}1\ 0\acute{6}\cdot 5; true inclination -\mathring{7}0\ 4\acute{0}\cdot 7; index correction -2\acute{5}\cdot 8 Auckland Island . . -73\ 41\cdot 3; true inclination -73\ 10\cdot 4; index correction -30\cdot 9 Campbell Island . . -74\ 20\cdot 3; true inclination -73\ 51\cdot 4; index correction -28\cdot 9 On ice, Jan. 8, 1841 -84\ 02\cdot 9; true inclination -83\ 36\cdot 6; index correction -27\cdot 3 Mean . . . -28\cdot 2
```

An index correction of -28' has therefore been applied in the general table to the mean of the observations on each day with needle R. F. 4, in order to give the true or correct inclination, as it would have been observed by a needle in which the complete process of observation had been gone through.

Elements of Calculation of the Intensity Observations.—Of the intensity observations made with Mr. Fox's apparatus on board the Erebus, during the period under consideration, a large proportion was of the angles of deflection produced by deflecting magnets. A spare needle belonging to the apparatus was used as a deflector, and was fitted into a cylindrical case having screws at both ends, so that the needle could be applied either as "deflector N" with its north pole opposite that division of the circle which the north pole of the dipping needle had previously indicated as the dip,—or as "deflector S" with its south pole similarly applied to the opposite division of the circle.

The deflectors belonging to the apparatus, being too weak to produce sufficient deflections when used separately, were employed only conjointly, and are designated as "deflectors N and S." The angles of deflection varied in different localities during the voyage in round numbers as follows: deflector S from 50° to 45°; deflector N from 48° to 43°; and N and S from 23° to 20°.

To obtain the equivalent weight to the deflecting force of the deflectors at these angles, we have comparative observations of the angles produced by the deflectors and by weights at Hobarton, Auckland, and Campbell Islands, on the ice on the 8th January in lat. — 68° 28′, long. 176° 32′, and on five different occasions on board ship when the weather and other circumstances were favourable, viz. on February 8th and 10th, March 22nd, April 1st and 6th. These were exclusive of an attempt on the 1st of February, which failed on account of the ship having too much motion.

Hobarton is necessarily the primary station of the whole series of observations made in this portion of the voyage, being the only station at which an independent determination of the intensity has been made. It is also very suitable for a base station, because we may expect that the absolute as well as relative intensity will be determined with great precision at the magnetic observatory established there, and will ultimately furnish a correction, should one be needed, for the provisional value which must for the present be employed.

Captain Ross commenced the experiments for measuring the absolute horizontal intensity at Hobarton, by obtaining five results with the large magnets of his observatory magnetometers on different days whilst the Expedition was refitting there. The details of these will be published with the other magnetometric observations of the voyage; the results, which have been computed by Lieutenant Goodenough of the Royal Artillery from the data received from Captain Ross, are as follows:—

```
October 13, 1840 . . . . . 4·491
May 3, 1841. . . . . . 4·626
May 21, 1841. . . . . . 4·502
June 5, 1841 . . . . . 4·579
June 25, 1841 . . . . . 4·566
```

The dip being -70° 40' at Hobarton, and the approximate value of the absolute horizontal intensity at Woolwich $3.72 \ racklet$ with the dip of 69° 03', the corresponding value of the total intensity at Hobarton in the arbitrary scale (London = 1.372) is 1.821. The previous *relative* observations, collected in No. I. of these Contributions, had given 1.819 as the mean of three determinations, viz.

The closeness in the accordance of the mean results by the two methods can only be viewed as accidental, because the probable error of the absolute determination, estimated from the differences in the partial results, is far greater than the difference of the two methods; but it fully warrants 1.82 being now taken as a provisional value of the total intensity at Hobarton, as the base station of the observations which form the subject of this number, regarding 1.82 + e as the true value, and e as a small correction to be determined hereafter, applicable to the whole series.

The weights employed in deflecting the intensity needle were from half a grain to six grains. It was soon found that half a grain was too small to give satisfactory results, and observations with that weight were discontinued. I have not therefore taken the observations made with it into account, except at Hobarton, where they

^{*} Since these pages were written I have received the results of twenty-two monthly determinations of the absolute horizontal intensity at the magnetic observatory at Hobarton (ten in 1841 and twelve in 1842) made and computed by Lieutenant Kay, R.N., and the naval officers under his direction. The mean in 1841 is 4·553, the partial results varying from 4·601 to 4·509; and the mean in 1842, 4·513, the partial results varying from 4·443 to 4·568. The discordance in the partial results of these observations is scarcely less than in those of Captain Ross: there is also a considerable disagreement in the means of the three series, which may not improbably be diminished when the particulars of the several observations shall have been carefully examined, though the partial results must still be expected to differ much more widely than could be desired. It is hoped that such differences will be reduced within much smaller limits by the use of the improved apparatus which has recently been supplied to the Hobarton as well as to the other colonial observatories.

⁺ Philosophical Transactions, 1843, Art. X.

assist in computing the angles corresponding to the weights of 4, 5, and 6 grains, which were not commenced with so soon. The observations with the weights on the days above stated, when the weights and deflecting magnets were employed in comparison, are collected in one view and given in the subjoined Table, in which are also shown the angles of deflection produced by the deflecting magnets on the same occasions.

10.10		Longitude.	Weights.		d : Intensit	Intensity	A	ngles of deflection by	
1840.	Latitude.		Grains.	Angles of deflection.	Thermo- meter.	deduced.	Deflector S.	Deflector N.	Deflectors N and S.
Sept. 18.	Hobai —42 52		$\begin{bmatrix} \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{bmatrix}$	\$ 41.4 5 22.7 8 14.6 10 49.6 16 15 22 06 28 03.5 34 21	5°2	\rightarrou\right\right\right\right\right\right\right\right\right\right	5°0 0′1	Notobserved	Notobserved.
Nov. 24.	Auckland -50 33		$\begin{bmatrix} 1 \\ 1\frac{1}{2} \\ 2 \\ 3 \\ 2 \end{bmatrix}$	5 18·4 8 02·2 10 36·8 15 58·3 10 12·1	52 52	1.844 1.867 1.856 1.851 1.930	49 29	46 50·2	Not observed.
Dec. 14. $\begin{cases} 15. \\ 1841. \end{cases}$	Campbel -52 44	169 10	$\left\{egin{array}{c} 3 \ 1 \ 2 \ 3 \end{array} ight.$	15 30·2 4 59·2 10 12·6 15 30·2		1.906 1.963 1.929 1.906 1.906	49 20·5 49 17	46 10·5 46 45·7	Not observed.
Jan. 8.	On i	ice. 176 32	$\begin{cases} 3 \\ 6 \\ 2 \end{cases}$	14 34·3 30 38·7 9 15·6	42	$\begin{bmatrix} 2.024 \\ 2.015 \\ 2.124 \end{bmatrix}$	47 16	44 17	21 55
Feb. 10.	-77 47 -77 39	187 18 187 06	$\left\{ egin{array}{c} 3 \\ 6 \\ 2 \\ 3 \end{array} \right.$	14 14·6 30 30·9 9 31 14 37	32	$\begin{vmatrix} 2.071 \\ 2.023 \\ 2.067 \\ 2.019 \end{vmatrix} $	47 03 46 55·5	44 23	22 03 21 55·9
Mar. 22.	-63 09	139 28	$ \begin{bmatrix} 6 \\ 2 \\ 3 \\ 4 \\ 5 \end{bmatrix} $	30 34·7 9 39 14 13 14 18·6 19 34·1 25 11·2	34	2.019 2.040 2.074 2.062 2.041 2.045 2.012	46 54	44 22	22 00
April 1.	-58 13	135 18	$\begin{bmatrix} 2\\3\\4\\5\\6\\1 \end{bmatrix}$	9 26·2 14 07·7 19 39·7 25 28·5 31 08·5 5 14·2	40 58	2.086	46 55	44 41	22 30
April 6.	-43 41	146 03	2 3 4 5 6	10 37·2 15 59·4 21 21 26 29·7 32 58·5		1.885 1.850 1.881 1.919 1.887	50 01	46 40	23 17

With the angles of deflection at Hobarton produced by the weights $\frac{1}{2}$, 1, $1\frac{1}{2}$, 2 and 3 grains, we obtain the equivalent weight 8·15 grains to the angle $v = 50^{\circ} \ 01'$ of deflector S at the same station; and thence the value of the constant $\frac{w}{1 \sin v} = 5.84$

in the formula for the equivalent weights to the force of the deflector observed elsewhere, viz.

$$w' = 5.84 \text{ I}' \sin v'$$
.

From the values of w' thus obtained, the subjoined Table has been formed of w' for each 20' of v for deflector N and deflector S, in the manner described in No. III. of these Contributions*; and with these values of w' we have the intensities I' relative to the force 1.820 at Hobarton computed by means of the formula

$$\mathbf{I}' = \frac{\mathbf{I}\sin v}{w} \cdot w' \operatorname{cosec} v' = 171 \ w' \operatorname{cosec} v'.$$

Defle	etor S.	Deflector N.		
v'.	w'.	v'.	w'.	
50 0' 49 40 49 20 49 00 48 40 48 20 48 00 47 40 47 20 46 20	gr. 8·15 8·23 8·30 8·37 8·44 8·51 8·56 8·61 8·65 8·65	47 20 47 00 46 40 46 20 46 00 45 40 45 20 45 00 44 40 44 20 44 00	gr. 7:90 7:95 8:00 8:06 8:11 8:16 2:21 8:25 8:30 8:33 8:37	

The results with the original magnets of the apparatus used conjointly, and designated as "N and S," are much inferior in precision to those obtained with the spare intensity needle used as a deflector. The angles of deflection were much less, owing to the force of the magnets, even when used conjointly, being very much inferior to that of the spare needle. The observations are of course given in the Table with the others, but as their results present on the one hand no systematic difference from those with the stronger deflector, and on the other hand are of inferior value, by reason of the extent of their fluctuation,—and as they could only tend therefore to impair the individual accuracy of the results with the stronger deflector and with the weights,—they have been omitted in the means.

Comparison of the Intensities deduced by the Weights and by the Deflectors at the Stations at which both were employed.

Station.	Latitude.	Longitude.	Deflector S.	Deflector N.	Weights.
Auckland Island Campbell Island On ice At sea At sea At sea At sea At sea	$ \begin{array}{r rrrr} -68 & 28 \\ -77 & 17 \\ -77 & 39 \\ -63 & 00 \\ -58 & 13 \end{array} $	187 18 187 06 139 28	1.862 1.875 2.021 2.034 2.041 2.043 2.042 1.820	1.873 1.898 2.044 2.038 2.047 2.039 2.017 1.884	1.852 1.927 2.017 2.053 2.053 2.041 2.037 1.885

^{*} Philosophical Transactions for 1842, Art. II.

General Remarks.—The Tables of the declination observations in the Erebus and Terror, and of the inclination and intensity observations in the Erebus, furnish a full opportunity, for those who may desire it, to examine how far the corrections computed in the manner which has been described fulfil their purpose.

The three charts which accompany this number of the "Contributions," exhibit to the eye the determinations contained in the Tables, arranged in their respective localities, by which their general harmony may be, in some measure, judged of. The faint lines, representing the principal curves of the magnetic elements, are drawn in approximate conformity with the observations, and are designed merely to assist the eye in taking a first general view of the results. When the determinations of the succeeding voyages shall have been laid down in a similar manner on a south polar chart, they will furnish the means of judging of the course of the magnetic curves more comprehensively and accurately, and of tracing them accordingly.

Rather more attention has been bestowed on the lines in the chart of the inclination than in the other two charts, because it has been used for the values of θ in the declination-corrections. Having had experience in drawing similar charts on former occasions, and particularly those of the Magnetic Survey of the British Islands, I have no hesitation in recognising with Captain Ross, that as great, and greater, discrepancies are to be looked for, and must frequently be experienced, in magnetic surveys conducted on land, than in those made at sea. The chart of the inclination which accompanies this paper, constructed from observations made at sea, and certainly not under the most favourable circumstances, except in the skill of the observers, exhibits by no means a greater measure of discrepancy than the magnetic chart of Scotland or of Ireland: and it may be further noticed, that the only results which have been excluded altogether from the chart, by reason of their excessive discordance as well with each other as with the general body of results, are some that were made on islands which presented themselves in the course of the voyage.

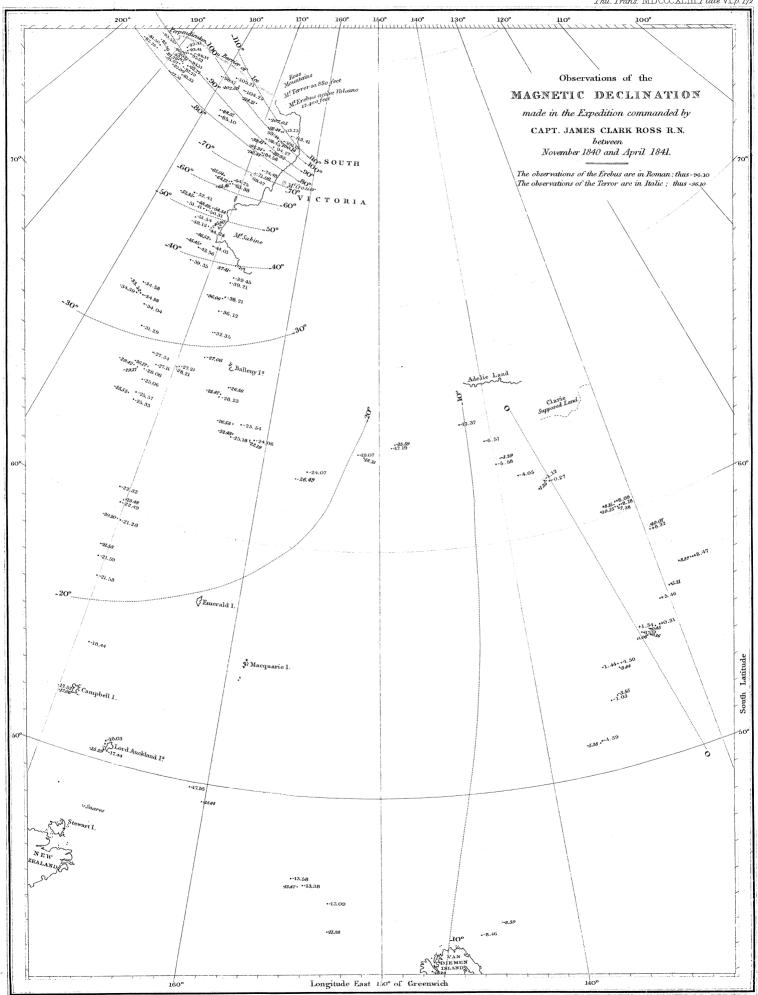
I cannot close this section without calling the attention of all who take interest in the results of these researches, to the invaluable aid for which magnetical science is indebted to Mr. Fox. Without his instrument and method, which render observations of inclination and intensity made at sea nearly or altogether equal to those which could be made on land or on ice, such were the difficulties of the navigation, and such the inaccessible though magnificent character of the coast that was discovered, that two of the three charts herewith presented, and especially that of the intensity, must have offered an appearance very different from that which they now exhibit.

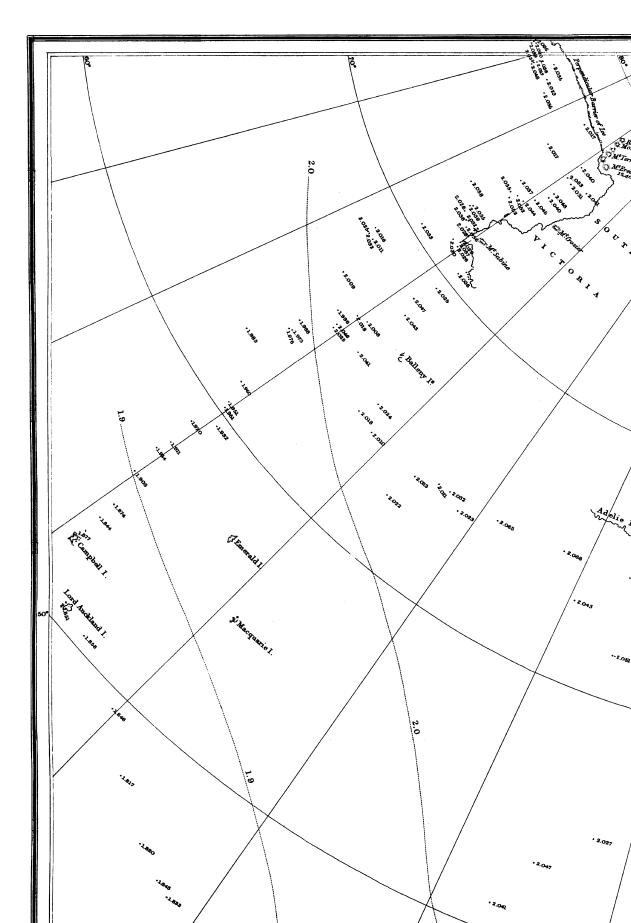
To enter into a lengthened comparison of the results now communicated with those of preceding observers, which have been embodied in magnetic maps constructed either directly from the phenomena, or by means of the mathematical theory of M. Gauss, would be to anticipate the more proper opportunity which will present itself, when the whole of the materials collected by the Antarctic Expedition shall be

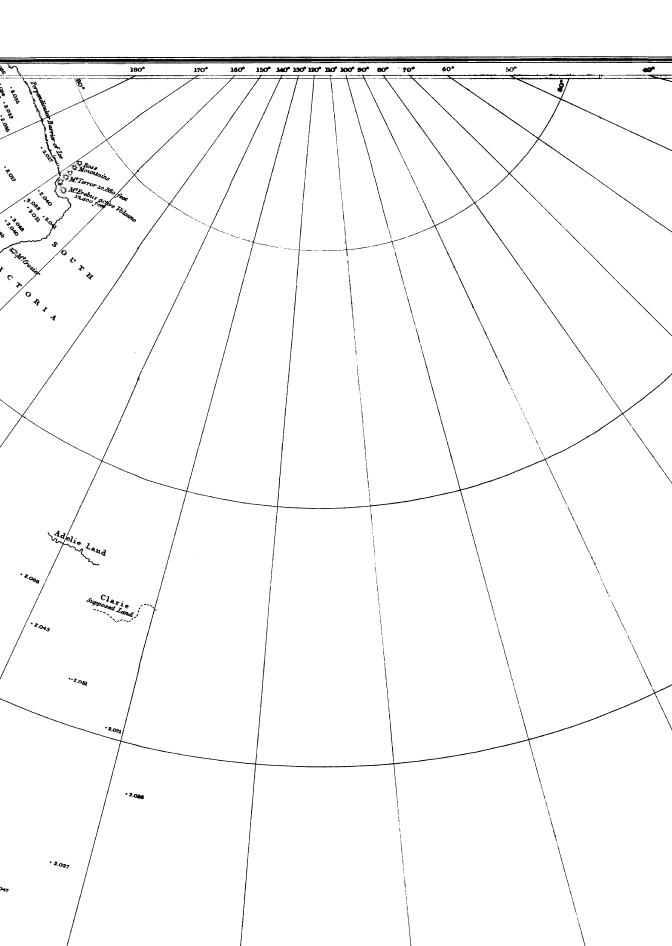
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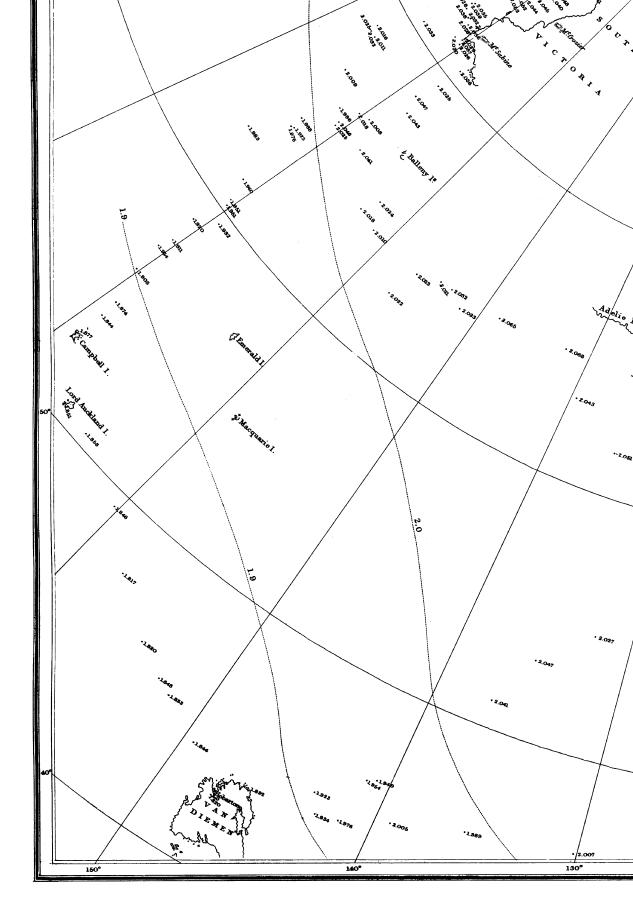
available for the comparison. A few remarks however on prominent points may be looked for on the present occasion.

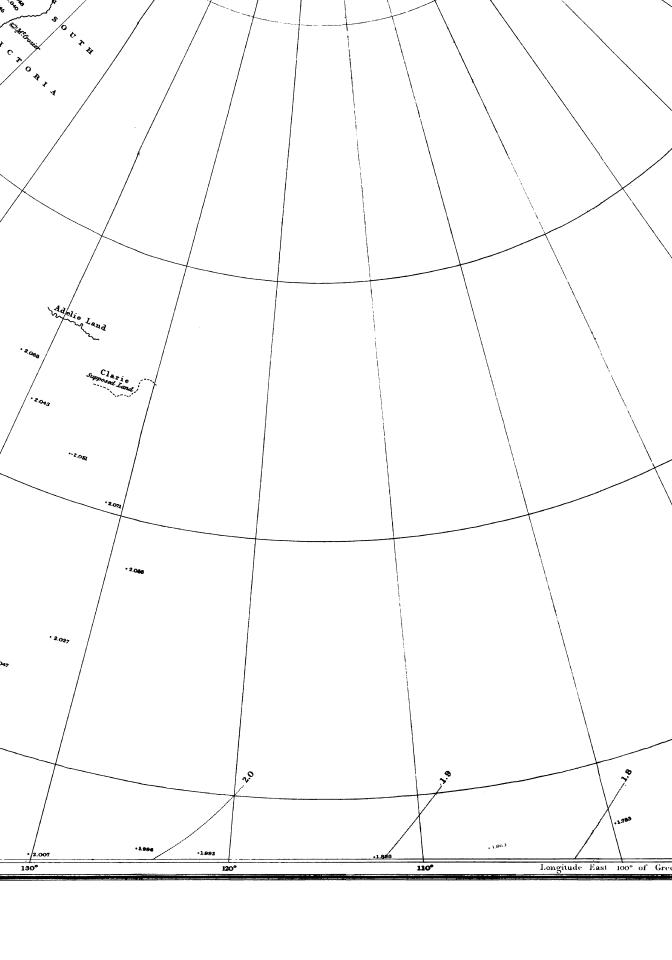
- 1. The observations of declination, particularly those which point out the course of the lines of 0 and of 10° east, indicate a more westerly position than the one assigned by M. Gauss in the "Atlas des Erdmagnetismus" for the spot in which all the lines of declination unite. The progression of the lines in the southern hemisphere generally, from secular change, is from east to west; the difference consequently is in the direction in which a change should be found in comparing earlier with more recent determinations.
- 2. The general form of the curves of higher inclination in the southern hemisphere is much more analogous to that in the northern, than appears in M. Gauss's maps. For example, the isoclinal line of 85° instead of being nearly circular, as represented in the 3^{te} Abtheilung of Pl. XVI. of the "Atlas des Erdmagnetismus," is an elongated ellipse, much more nearly resembling in form and dimensions the ellipse of 85° of inclination in the northern hemisphere in the same work, Pl. XVI. 2^{te} Abtheilung. The analogy between the two hemispheres in the characteristic feature of the elliptical form of the higher isoclinal lines is the more important to notice, on account of the particular relation which appears to subsist in the northern hemisphere, between the change in the geographical direction of the greater axis of the ellipse, and the secular changes of the inclination generally throughout the hemisphere. The present direction of the greater axis in the northern hemisphere is nearly N.N.W. and S.S.E., or that of a line passing through the two foci of maximum intensity. In the southern hemisphere the present direction of the greater axis differs little from E.S.E. and W.N.W.
- 3. Captain Ross's observations of the intensity do not appear to indicate the existence anywhere in the southern hemisphere of a higher intensity than would be expressed by 2·1 of the arbitrary scale. In this respect also the analogy between the two hemispheres appears to be closer than is shown in M. Gauss's maps, Atlas, Pl. XVIII. With respect to the direction of so much of the line of highest intensity (2·0) as it has been possible to draw with any degree of confidence from the observations now communicated, it will be found to be in almost exact parallelism with the isodynamic line of 1·7 in Plate III. of my memoir "On the Variations of the Magnetic Intensity" in the Reports of the British Association for 1838; which line was the highest of which the position could be assigned, for any considerable distance, by the aid of the then existing determinations.

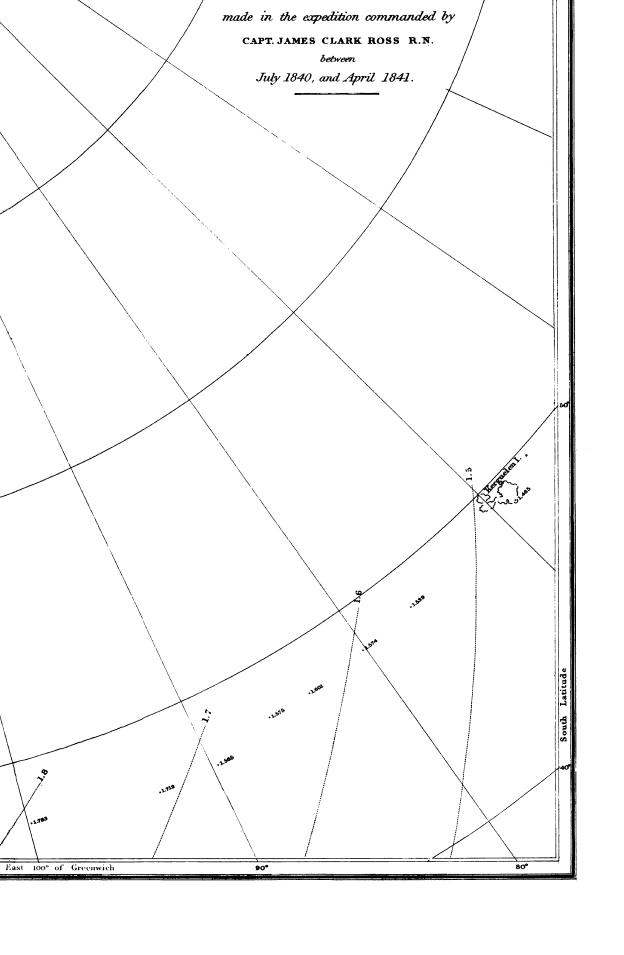


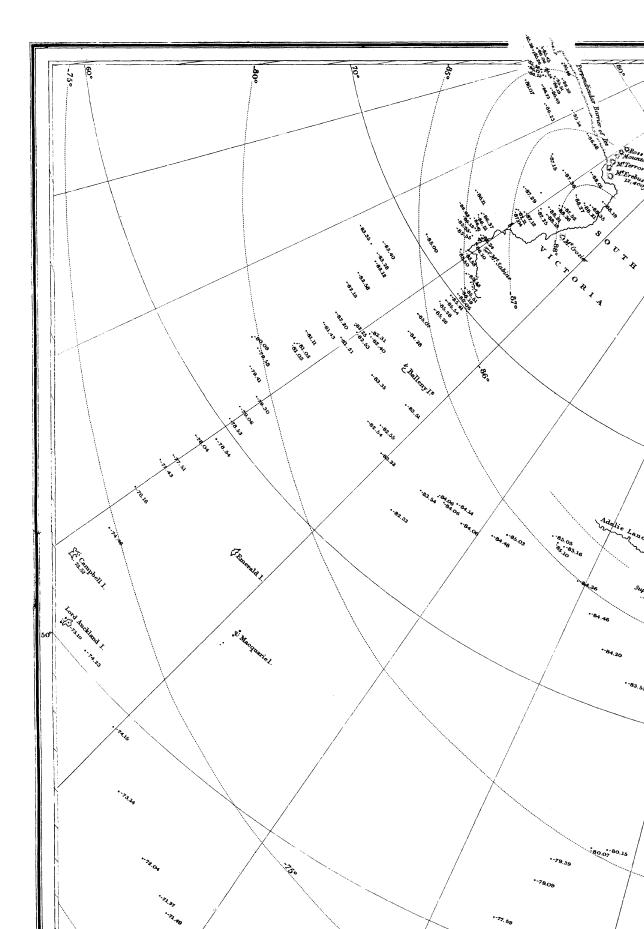


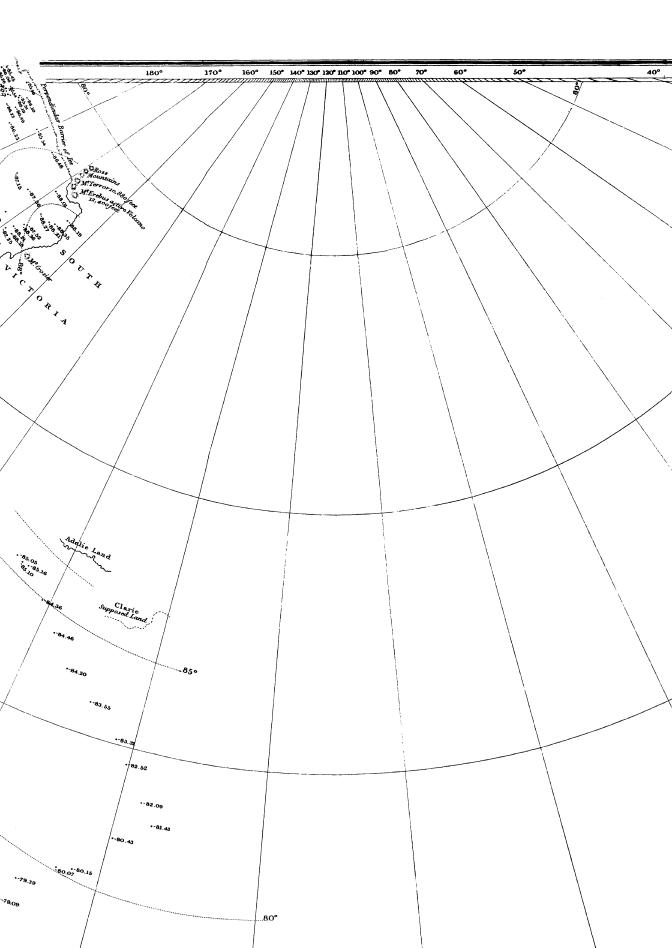


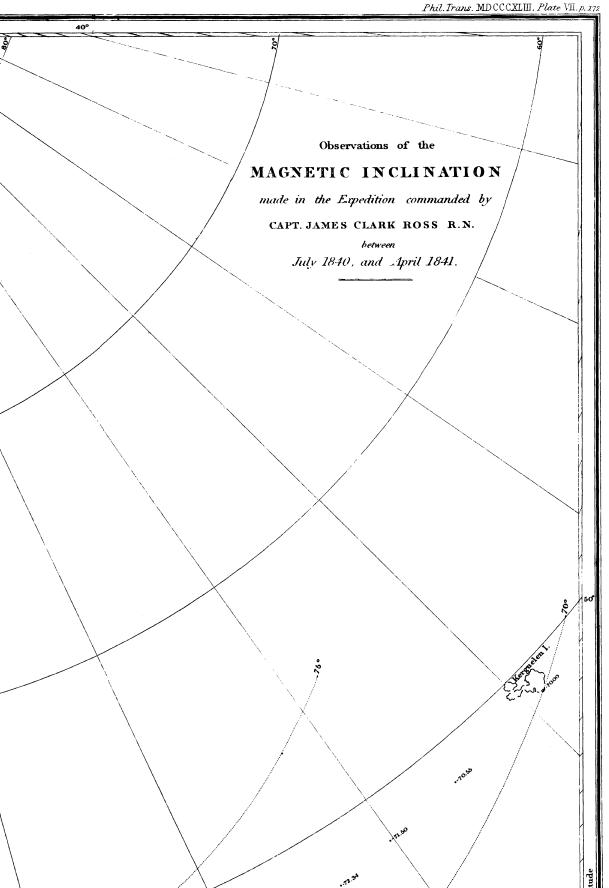


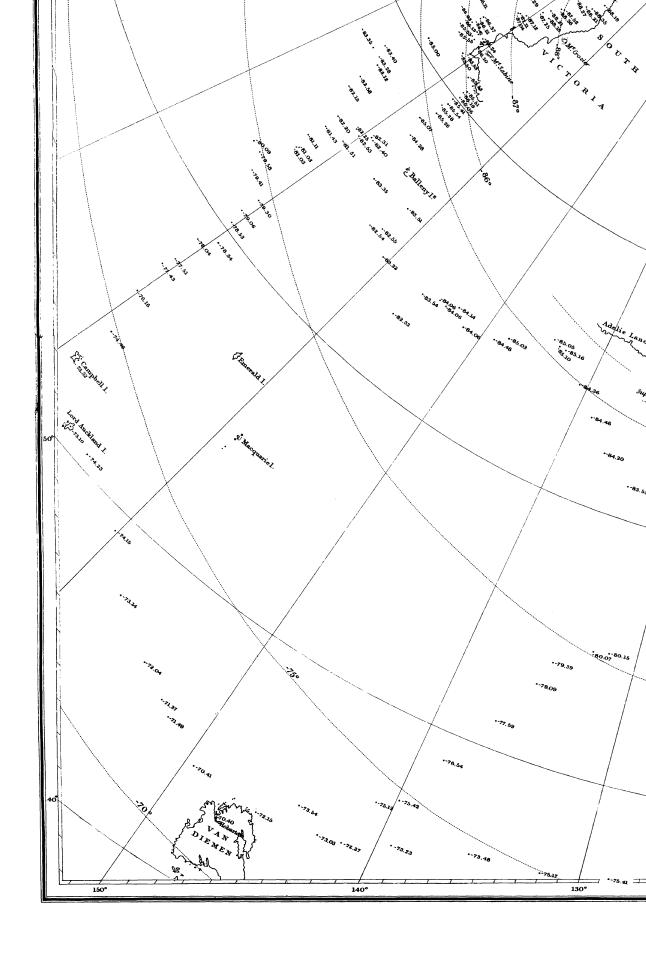


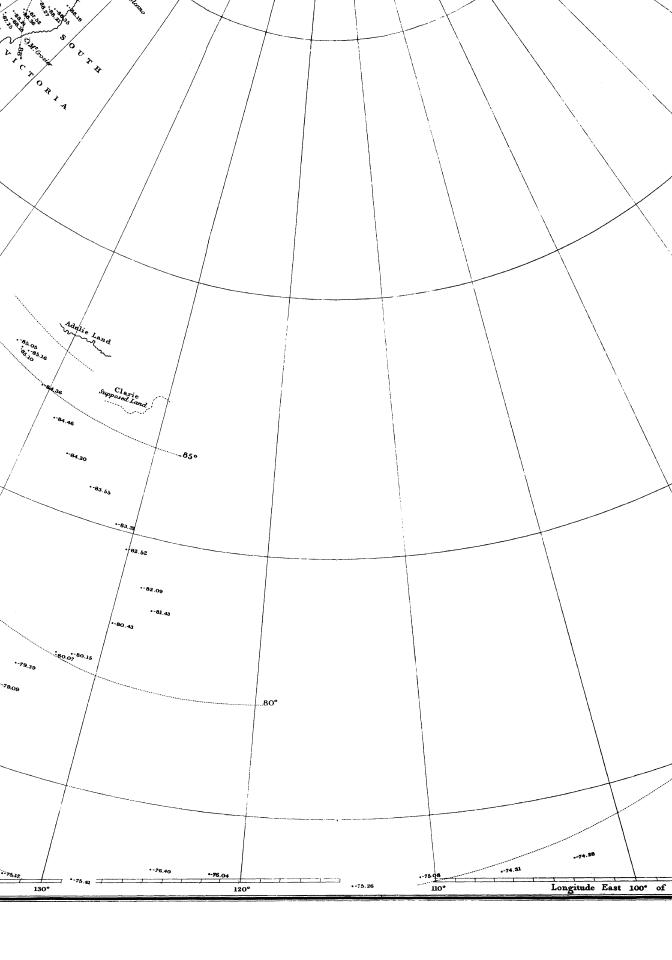


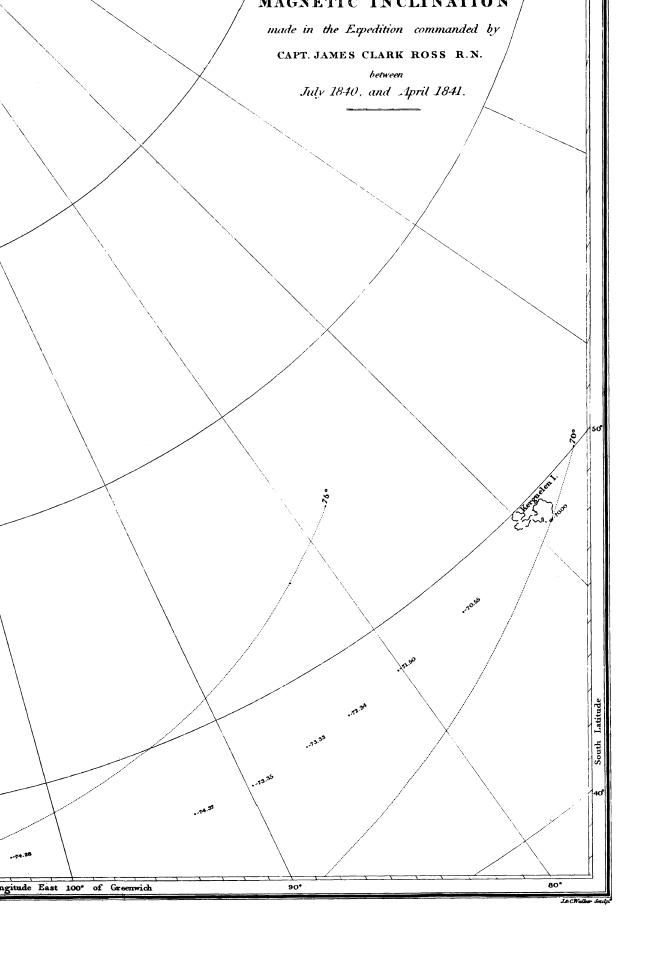












§ 9. Observations of the Magnetic Inclination and Intensity made on board Her Majesty's ship Erebus on the passage from Kerguelen Island to Van Diemen Island in July and August 1840.

These observations were made with Mr. Fox's apparatus, and with the same needle F which had been employed in the determinations made at sea on the passage from England to Kerguelen Island, discussed in § 5 and § 6 of these Contributions*. The inclinations at sea were observed with the face of the circle always to the east: the index correction for needle F in this position of the instrument has been derived by comparing similar observations made with it at the magnetic observatory at Kerguelen Island, with the results obtained at the same spot with other needles which had their poles reversed. These are contained in the following Table:—

Observations of the Inclication with needles whose poles were reversed, made at the Magnetic Observatory at Kerguelen Island, July 1840.

1840.	Hours.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
July 4. 6. 6. 6.	h m 10 A.M. 6 P.M. 6 15 P.M. 6 30 P.M. 7 20 P.M.	C 2 {	$\begin{array}{c} \alpha - 69 & 59.7 \\ \beta - 69 & 58.4 \\ \alpha - 69 & 59.0 \\ \beta - 69 & 50.2 \\ \alpha - 69 & 59.8 \\ \beta - 70 & 01.6 \\ \alpha - 69 & 59.7 \\ \beta - 69 & 48.7 \\ \alpha - 69 & 47.8 \\ \beta - 70 & 01.0 \\ \alpha - 70 & 03.1 \\ \end{array}$	$ \begin{cases} -69 & 59.0 \\ -69 & 54.6 \\ -70 & 00.7 \\ -69 & 54.2 \\ -69 & 54.4 \end{cases} $	Needles belonging to H. M. S. Terror. Observers, { Captain CROZIER, Lieut. KAY.
8. 9. 9. 10.	 45 P.M. 30 P.M. 30 P.M. A.M. 	ļ	$\begin{vmatrix} \beta - 70 & 02.0 \\ \alpha - 69 & 54.3 \\ \beta - 70 & 03.8 \\ \alpha - 69 & 57.7 \\ \beta - 70 & 04.0 \\ \alpha - 70 & 13.9 \end{vmatrix}$	$ \begin{cases} -70 & 02.5 \\ -69 & 59.1 \\ -70 & 00.8 \\ -70 & 11.4 \end{cases} $	Needles belonging to H. M. S. Erebus. Observer, Captain Ross.
		· · · · · · · · · · · · · · · · · ·	β-70 08.9	J	General Mean.

The inclination observed with needle F at the same spot with the face of the circle towards the east was $-69^{\circ} 57' \cdot 9$; whence the index correction is $-1' \cdot 7$.

The intensity of the magnetic force was determined in this portion of the voyage, on every day that the weather permitted, by the angles of deflection caused by a deflecting magnet. The observations were a continuation of the series of which the earlier portion is given in $\S 5$ and $\S 6$. The deflecting magnet employed was the deflector S. Tables are given, in the sections referred to, of the values of w' for this deflector corresponding to angles of deflection from 42° to 25° , derived from a comparison with the deflections produced by weights. The increase of the terrestrial force, in the passage between Kerguelen and Van Diemen Islands, brought the angle

^{*} Philosophical Transactions, 1842, Art. II.

of deflection with deflector S down nearly to 20° . The weather was too unsettled to admit of any comparison being made with the weights at sea, and an accident which befel the needle on or before the arrival at Hobarton prevented the comparison which otherwise would have been made there. The values of w' corresponding to the angles of deflection from 25° to 20° have, therefore, been supplied, by continuing the rate of progression at which the deflecting force of the magnet S had been found by experiment, in angles from 36° to 25° , to increase as the angle diminished, viz. 0.033 gr. for each degree; we have thus the following values:—

$$v' = 26;$$
 $w' = 2.594$
 $v' = 25;$ $w' = 2.628$
 $v' = 24;$ $w' = 2.661$
 $v' = 23;$ $w' = 2.694$
 $v' = 22;$ $w' = 2.727$
 $v' = 21;$ $w' = 2.760$
 $v' = 20;$ $w' = 2.793.$

At Kerguelen Island we have the angle of deflection with the magnet $S = 26^{\circ} 21' \cdot 3 = v$; the equivalent weight $= 2 \cdot 58 = w$; and (§ 6.) I = 1.465 (London = 1.372); whence in other localities

$$I' = I \frac{w' \sin v}{w \sin v'} = .2521 \ w' \csc v',$$

v' being furnished by the observation and w' taken from the preceding Table.

The last observation recorded to have been made with needle F was on the 11th of August, 1840, in lat. — 44° 16′, long. 142° 38′; when the angle of deflection being 21° 06′.5,

I' = 1.929 uncorrected for the ship's attraction, or (the course being E. by N. $\frac{1}{2}$ N.), I' = 1.934 corrected.

On the return of the Expedition from the Antarctic Circle in the following year, the ships regained their former track, and on the 5th of April, 1841, Captain Ross repeated the observations with different instruments within a few miles of the spot on which he had observed on the 11th of August, 1840: these observations gave I' = 1.927 in lat. $-45^{\circ}02'$, long. 143° 10′. If we examine the map in which the intensity observations are inserted, we perceive that the direction of the two geographical positions in relation to each other is very nearly that of the isodynamic lines in that quarter; and if we refer generally to the Tables, we see that the difference in the resulting intensity on the two occasions is within the limits of the differences of partial determinations with the same instrument at one spot. As far as circumstances permit us to judge, therefore, we may view the observations of the two voyages as forming parts of one connected series.

As the ship's head during the run under consideration varied but little on any occasion from her direct course, and as that course is one on which the corrections, both of inclination and intensity, are small, I have taken them from the Table computed by means of the constants deduced in the preceding section.

Observations of the Inclination with Needle F on board H.M.S. Erebus, between July 22nd and August 11, 1840, on her passage from Christmas Harbour, Kerguelen Island, to Hobarton, Van Diemen Island.

1840).	Latitude.	Longitude.	Method employed.	Inclination. Face east.	Ship's head.	Corrections for ship's attraction.	Corrected inclination.	Remarks.
June	26.	Magnetic (Kerguele -48 41	n Island.	S.	-70 02·8 -69 56·3 -69 48·3 -70 04·2	Observed on shore.		-69 59·6	Remark by Captain Ross. "From these observations the In- dex error of Needle F.(face east), as used on board ship, may
July	22.	—48 29	76 55	Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	} s.e. by e.	-18	-70 55	be obtained."
	23. 23.	-48 17	80 15	Direct.	$ \begin{array}{rrr} -71 & 48 \\ -71 & 34 \cdot 4 \end{array} $	$\left. \right $ s.e. by e. $\frac{1}{2}$ e.	-12	—71 50	·
	24. 24.	-47 55	83 51	Direct.	$ \begin{array}{rrr} -72 & 10 \\ -72 & 29 \end{array} $	$\left. \right\} \text{ s.e. by e.} \frac{1}{2} \text{ e.}$	-13	-72 34	
	25. 25.	-47 46	86 18	Direct.	$ \begin{array}{rrr} -73 & 4.5 \\ -73 & 28.5 \end{array} $	$\bigg \bigg\} \text{ s.e. by } \text{E.} \frac{1}{2} \text{ E.}$	15	-73 33	
	26. 26.	-47 12	89 45	Direct. S.	-73 13 $-73 24.5$	$\left \int_{0}^{\infty} s.e. by e. \frac{1}{2} e. \right $	-15	$-73 \ 35$	Considerable swell.
	27. 27.	-47 03	93 0	Direct. S.	-74 11.3 $-74 27.5$	$\left \right $ s.e. by $E^{\frac{1}{2}}E$.			A high sea.
	28. 30.	-47 13 $-47 39$	97 07 102 42	Direct.	-74 15	$\left.\begin{array}{c} \text{s.e. by e.} \frac{1}{2} \text{ e.} \\ \\ \text{e.s.e.} \end{array}\right.$			Too much motion to continue.
	30. 31. 31.	-47 35	106 26	S. Direct.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E.		-74 31	
Aug.	1. 1.	-47 45	110 39	Direct.	$\begin{bmatrix} -74 & 48 \\ -75 & 6 \end{bmatrix}$	E.S.E.	- 9	-75 0 8	Much motion.
	2. 2.	-47 34	114 15	Direct.	-75 20.5 $-75 6$	$\left \right $ E. by s. $\frac{1}{2}$ s.	- 1	-75 26	
	4. 4.	—47 41	121 30	Direct.	$\begin{vmatrix} -76 & 9.8 \\ -76 & 6.3 \end{vmatrix}$	$\left \right $ E. by s.	+ 6	-7604	Much motion.
	5. 5.	-47 34	124 43	Direct.	$-76 49.2 \\ -76 53.7$	$\left.\right \right\} \text{E. } \frac{1}{2} \text{ s.}$	+13	-76 40	Very unsteady.
	6. 6.	-46 44	128 26	Direct.	-76 1.6 $-75 59$	E.	+21	75 41	
	7. 7.	-4 6 13	132 0	Direct.	$ \begin{array}{rrrr} -75 & 43.7 \\ -75 & 45 \end{array} $	$\left.\begin{array}{c} \\ \\ \end{array}\right\} \qquad \text{E. } \frac{1}{2} \text{ N.}$	+29	-75 17	
	8. 8.	-45 59	135 38	Direct.	$ \begin{array}{rrr} -74 & 33.5 \\ -74 & 11 \end{array} $	E. by N.		-73 48	
	9. 9.	-45 17	139 19	Direct.	$ \begin{vmatrix} -74 & 17.5 \\ -74 & 0.4 \end{vmatrix} $	E.N.E.	+48	-73 23	
	10. 10.	-44 24	141 39	Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.E. by E.	+59	$-72 \ 37$	·
	11.	-44 16	142 38	Direct.	$ \begin{array}{r} -73 & 37.15 \\ -73 & 49 \end{array} $		+42	-73 03	

The index correction -1^{l} ? has been applied in the final column.

Observations of the Magnetic Intensity with Needle F, on board H.M.S. Erebus, between July 22nd and August 11th, 1840, in her passage from Christmas Harbour, Kerguelen Island, to Hobarton, Van Diemen Island.

Remarks.		At the Magnetic Observatory.			-		Considerable swell.	A high sea.	Much motion.			Much motion.		Very unsteady.	Very unsteady.	1					
Corrected intensity. London=1.372.		1.465	1.539	1.574	1.601	1.575	1.565	1.712	1.712	1.855	1.863	1.815	1.970	1.992	1.996	2.034	1.980	1.989	2.005	1.976	1.934
Corrections for ship's attraction.			024	020-	020-	020-	020-	020-	020-	017	017	017	014	010	900-	003	0	200. +	+ • • • • •	+.014	+.005
Intensity.		1.465	1.563	1.594	1.621	1.595	1.585	1.732	1.732	1.872	1.880	1.832	1.984	2002	2002	2.037	1.980	1.987	1.997	1.962	1.929
Ship's head.	Observed)	on shore.	s.e. by E.	s.e. by e. ½ E.	s.e. by e. ½ E.	s.e. by E. ½ E.	E.S.E.	E.S.E.	E.S.E.	E. by s. $\frac{1}{2}$ s.	E. by s.	E. 3 S.	ğ	E. 2 N.	E. by N.	E.N.E.	N.E. by E.	E. by N. ½ N.			
Tempe-	34.5	34.5	34	33	39	35	34	44	44	43	44	35	42	40	41	42	49	51	55	20	48
Angle of deflection.	1. 4.	20 19·6 26 21·3		24 39.4	24 20	24 38.5	24 46.5	23 04	23 04	21 37.5	21 33.6	22 01.7	20 37	20 27.7	2.82 02	20 10.5	z.68 0z	20 34.7	20 31.1	20 48.7	21 06.5
Method employed.	W. $1\frac{1}{2}$ gr.	W. 2 grs.	s,	s,	s,	s,	s.	s,	s,	Š	s.	s.	s.	s.	s.	v.	s.	S.	š	s,	ø
Longitude.	On shore at Kerguelen	Island. I 68 54		80 15	83 51	86 18	89 45	93 0	20 26	102 42	106 26	110 39	114 15	121 30	124 43	128 26	132 0	135 38	139 19	141 39	142 38
Latitude.	On shore at	Isla — 48 41		-48 17	-47 55	-47 46	-47 12	-47 03	-47 13	-47 39	-47 35	-47 45	-47 34	-47 41	-47 34	-46 44	-46 13	-45 59	-45 17	-44 24	-44 16
1840.	June 26 [and 28.	July 22.	23.	24.	25.	.98	27.	28.	30.	31.	Aug. 1.	e;	4.	5.	.9	7.	%	6	10.	11.

DECLINATIONS observed on board Her Majesty's Ship Erebus between November 15, 1840, and April 6, 1841.

The Observers are distinguished in the column of Initials as follows:—R. Captain Ross; S. Lieut. Sibbald; W. Lieut. Wood; T. Mr. Tucker, Master; Sm. Mr. Smith, and O. Mr. Oakley, Mates; Y. Mr. Yule, Second Master. East Declination is characterised by the sign —.

1840.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.	Ini	obscived.	snip's nead.		attraction.	Decimation.	Decimation.	Rer
Nov. 15. p.m.	$ \begin{array}{r rrr} -45 & 33 \\ -45 & 33 \\ -45 & 33 \end{array} $	152 49 152 49 152 49	R. T. R. T.	- 8 55 - 8 37 - 8 23 - 8 25	E.S.E. E.S.E. E.S.E.	_71 40 <	- 4 39 - 4 39 - 4 39 - 4 39	$\begin{bmatrix} -\mathring{1}3 & 34 \\ -\mathring{1}3 & 16 \\ -\mathring{1}3 & 02 \\ -\mathring{1}3 & 04 \end{bmatrix}$	—13 09	
16 а.м.		152 55 152 55 153 02	Sм. R. R. R. T. Y.		E.S.E. E.S.E. E.S.E. S.E. by E. $\frac{1}{2}$ E.		 4 39 4 39 4 39 4 39 4 34 4 34 	$\begin{bmatrix} -12 & 49 \\ -13 & 11 \\ -13 & 01 \\ -13 & 19 \\ -13 & 05 \\ -13 & 13 \end{bmatrix}$	-10 03	
	-46 05 $-46 09$ $-46 09$ $-46 09$	154 11 154 14 154 14 154 14 154 14	S. S. Y. T. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. by E. $\frac{1}{2}$ E. S.E. by E. $\frac{1}{2}$ E.	-72 04 ₹	 4 23 4 34 4 34 4 34 4 34 	$ \begin{array}{c cccc} -13 & 19 \\ -13 & 51 \\ -13 & 57 \\ -14 & 14 \\ -13 & 05 \end{array} $	-13 38	
16 г.м.	-46 30 $-46 30$	154 54 154 54 154 54 154 54 154 54	S. T. S. T. T. R.	$ \begin{array}{rrrrr} -13 & 29 \\ -14 & 55 \\ -12 & 57 \\ -8 & 05 \end{array} $	s.e. by E. $\frac{1}{2}$ E. $\frac{1}{2}$ N. N. by E. N.N.E. s.e. by E. $\frac{1}{2}$ E. s.e. by E. $\frac{1}{2}$ E.	-72 04	- 4 34 0 00 - 0 46 - 1 30 - 4 34 - 4 34	$ \begin{array}{c cccc} -14 & 24 \\ -13 & 29 \\ -15 & 41 \\ -14 & 27 \\ -12 & 39 \\ -13 & 46 \end{array} $	—13 5 8	
18 р.м.	-49 42 $-49 48$	155 01 160 52 160 56 161 00	R. T. R. R. R.	$ \begin{array}{ccccc} - & 9 & 19 \\ - & 13 & 11 \\ - & 12 & 27 \\ - & 11 & 49 \end{array} $	S.E. by E. $\frac{1}{2}$ E. S.E. by E. $\frac{1}{2}$ E. E.S.E. E.S.E. E.S.E.		- 4 34 - 4 34	-13 49 -13 53		`
Dog 5 Av	-49 49 -49 49 -49 52 -49 52	161 00 161 08 161 08	T. T. R. S.	$ \begin{array}{c cccc} -12 & 18 \\ -12 & 03 \\ -12 & 06 \\ -11 & 18 \\ -10 & 27 \\ \end{array} $	E.S.E. E.S.E. E.S.E. E.S.E.	—74 00	- 5 19 + 4 05	-17 16 -18 24	—17 16	with the Mag- vatory.
Dec. 5. A.M.	At an		R{	$ \begin{array}{c cccc} -22 & 29 \\ -22 & 26 \\ -17 & 49 \\ -17 & 44 \\ -17 & 45 \end{array} $	s.w. s.w. Observed		+ 4 05	-18 21	—17 44·1	Declination observed on shore with the Mag- netometers of the Observatory.
	-50 32 At an	166 12 nchor.		$ \begin{array}{c cccc} -17 & 42 \\ -17 & 43 \\ -17 & 42 \\ -16 & 44 \\ -16 & 20 \end{array} $	on shore.		+ 2 17	1 1	-	
8 р.м.	At an At an At an At an At an	ichor. ichor. ichor.	T. T. W. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.W. N.N.W. N.N.W. ¹ / ₂ W. N.N.W.		+ 3 10 + 1 39 + 2 03 + 1 39	-18 47 -19 25 -18 38 -17 53 -18 15		Mean declination observed on board at anchor.
	At an At an At an At an	chor.	T. T. T. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.E. N.E. E.N.E. E.	−7 3 15≺	- 1 39 - 3 10 - 4 23 - 5 05	$ \begin{array}{c cccc} -17 & 17 \\ -18 & 56 \\ -17 & 59 \\ -17 & 57 \end{array} $	—17 53	Mean declina board a

1840.	Posit	tion.	ials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean	Remarks.
1040.	Lat.	Long.	Initials	observed.	ship's head.		attraction.	Declination.	Declination.	Rem
Dec. 11. A.M.	Aucklan At ar		T. T. T. T. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w.n.w. by w. w. by n. w. w. by n.	-73 15≺	+ 4 23 + 3 50 + 5 05 + 4 50 + 5 05 + 4 50	$\begin{array}{c c} -1\mathring{7} & 4\mathring{3} \\ -17 & 49 \\ -17 & 44 \\ -18 & 29 \\ -17 & 56 \\ -17 & 36 \end{array}$	- î7 5́3	
12 A.M.	-50 33 -50 33 -50 33 -50 48 -50 48 -50 48	166 24 166 24 166 42 166 43	T. R. S. T. T. S. Y.	-21 32 -12 33 -12 15 -12 30 -10 15 -11 06 - 9 46	N.W. $\frac{1}{2}$ N. S.E. by E. S.E. by E. $\frac{1}{2}$ E. S.E. by E. S.E. by E. S.E. by E. S.E. by E.	-73 30	+ 2 48 - 4 46 - 4 58 - 4 46 - 4 46 - 4 46	$egin{array}{c c} -18 & 44 \ -17 & 19 \ -17 & 13 \ -17 & 16 \ -15 & 01 \ -15 & 52 \ -14 & 32 \ \end{array}$	-16 03	
16 р.м.	-52 14 -52 33 Campbel at ancl -54 12	166 43 169 09 l Island, hor. 169 06	S. R. R. R.	-10 37 $-22 19 $ $-23 14 $ $-15 53$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$-73 52 \left\{ \begin{array}{c} \\ \\ \end{array} \right.$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$egin{array}{cccc} -15 & 05 \ -17 & 47 \ -17 & 57 \ \end{array} \ egin{array}{cccc} -18 & 22 \ \end{array}$	-17 52	
19 A.M. 21 A.M.	$\begin{array}{rrrr} -54 & 12 \\ -54 & 13 \\ -54 & 16 \\ -54 & 16 \\ -55 & 22 \\ -57 & 25 \end{array}$	169 06 169 06 169 07	S. R. T. S. S. SM.	$ \begin{array}{rrrr} -15 & 41 \\ -15 & 21 \\ -17 & 31 \\ -15 & 42 \\ -18 & 47 \\ -20 & 40 \end{array} $	$ \begin{array}{c c} S.S.E. \\ S.S.E. \frac{1}{2} E. \\ S.S.E. \\ $	-74 46	$ \begin{array}{rrrrr} - & 2 & 29 \\ - & 3 & 00 \\ - & 2 & 29 \\ - & 2 & 29 \\ + & 0 & 40 \\ - & 3 & 01 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-18 44	
•	$ \begin{array}{rrrr} -57 & 25 \\ -57 & 27 \\ -57 & 27 \\ -57 & 31 \\ -57 & 35 \end{array} $		T. Y. T. SM. S. O.	$ \begin{array}{cccc} -19 & 39 \\ -20 & 43 \\ -18 & 18 \\ -20 & 43 \\ -17 & 09 \\ -19 & 06 \end{array} $	S.S.E. S.S.E. S.S.E. S.S.E. S.S.E. S. <u>1</u> 2 E.	-77 00 ₹	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} & 22 & 40 \\ & -23 & 44 \\ & -21 & 19 \\ & -23 & 44 \\ & -20 & 10 \\ & -19 & 50 \end{array} $	-21 58	
	-57 36 -57 38 -57 38 -57 40 -57 45	170 21 170 27 170 27 170 28 170 28	T. R. S. R. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by E. $\frac{1}{2}$ E. s. s. s. $\frac{1}{2}$ E. s. by W. $\frac{1}{2}$ W.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-21 59	
22 A.M.	-59 00 -59 01 -59 36 -59 45 -59 47	170 02 170 02	T. T. T. Y. Y.	$ \begin{array}{c cccc} -19 & 34 \\ -19 & 08 \\ -23 & 25 \\ -21 & 54 \\ -21 & 12 \end{array} $	s. by w. $\frac{1}{2}$ w. s.s.e. s.e. by s. s. by w. $\frac{1}{2}$ w. s. $\frac{3}{4}$ w. s. by w.	$-78 \ 04 \left\{ \begin{array}{c} \\ \\ \\ \\ \end{array} \right.$	$\begin{array}{c cccc} + & 2 & 30 \\ + & 1 & 15 \\ + & 1 & 40 \end{array}$	$ \begin{array}{c cccc} -22 & 17 \\ -22 & 46 \\ -23 & 37 \\ -20 & 55 \\ -20 & 39 \\ -19 & 32 \\ \end{array} $	-21 28	
24 A.M.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	169 17 169 19 170 24 170 24 170 24	Т. Т. Sм. Т.	$ \begin{array}{c cccc} -17 & 57 \\ -17 & 19 \\ -15 & 01 \\ -20 & 07 \\ -20 & 17 \\ -21 & 33 \end{array} $	s.e. by s. s.s.e. s.s.e. s.s.e. s. by e. s.	33	$ \begin{array}{c cccc} & 3 & 18 \\ & 6 & 03 \\ & & 3 & 21 \\ & & 1 & 43 \end{array} $	$ \begin{array}{c cccc} -22 & 36 \\ -20 & 37 \\ -21 & 04 \end{array} $ $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
-	$ \begin{array}{ccccc} -60 & 10 \\ -60 & 12 \\ -60 & 12 \\ -60 & 12 \\ -60 & 18 \end{array} $	170 24 170 24 170 24 170 24 170 24 170 27	T. Y. S. O. T. R.	$ \begin{array}{c cccc} -21 & 38 \\ -20 & 01 \\ -18 & 03 \\ -20 & 21 \\ -21 & 27 \\ -20 & 13 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-78 53	+ 0 25 - 6 03 - 2 30 - 3 21 - 1 43 - 3 21	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-22 49	
	-60 20	170 27		-19 31	s.s.e.	U		-22 52J		

1840.	Posi Lat.	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declina- tion.	Remarks.
Dec. 24 р.м.	$-60 42 \\ -60 46$	170 55 170 55	R. R. R.	$-16\ 49$ $-18\ 03$ $-18\ 06$	s.e. by s. s.e. by s.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} -22 & 55 \\ -22 & 55 \\ -22 & 58 \end{array} $	o /	
	$ \begin{array}{rrr} -60 & 46 \\ -60 & 48 \\ -60 & 48 \end{array} $	170 55 170 55 170 55 170 55	R. S. T. R. T.	$ \begin{array}{r} -18 & 23 \\ -19 & 37 \\ -18 & 42 \\ -18 & 02 \\ -17 & 35 \\ \end{array} $	s.e. by s. s. by $\frac{1}{2}$ e. s.s.e. \Rightarrow s.e. by s. s.e. by s.	$-79 \ 06$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$egin{array}{c cccc} -23 & 15 & & & \\ -22 & 17 & & & \\ -22 & 07 & & & \\ -22 & 54 & & & \\ -22 & 27 & & & \\ 22 & 27 & & & \\ \end{array}$	-22 32	
29 г.м.	$-60 50 \ -60 55 \ -64 10 \ -64 10$	170 41 172 28 172 28	S. R. R. R. R.	$\begin{array}{rrrr} -17 & 33 \\ -17 & 57 \\ -16 & 46 \\ -30 & 28 \\ -29 & 24 \\ -27 & 34 \end{array}$	s.e. by s. s.e. by s. s.s.e. ½ e. s.s.w. s.s.w. s. by w.		$ \begin{array}{rrrrr} - & 4 & 52 \\ - & 4 & 52 \\ - & 4 & 07 \\ + & 4 & 06 \\ + & 2 & 06 \end{array} $	$egin{array}{c c} -22 & 25 \\ -22 & 49 \\ -20 & 53 \\ -26 & 22 \\ -25 & 18 \\ -25 & 28 \\ \end{array}$		
30 A.M.	$ \begin{array}{r} -64 & 10 \\ -64 & 12 \\ -64 & 12 \\ -64 & 27 \\ -64 & 27 \end{array} $	172 29 172 29 172 29 172 36	SM. S. S. S. S.	$ \begin{array}{rrrrr} -27 & 34 \\ -25 & 30 \\ -25 & 32 \\ -23 & 32 \\ -30 & 04 \\ -31 & 18 \end{array} $	$\begin{array}{c} \text{S. by w.} \\ \text{S. } \frac{1}{2} \text{ W.} \\ \text{S. } \frac{1}{2} \text{ W.} \\ \text{S. E.} \\ \text{S.W. } \frac{1}{2} \text{ S.} \\ \text{S.W. } \frac{1}{2} \text{ S.} \\ \end{array}$	$-81 \ 03$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$egin{array}{c c} -24 & 28 \\ -24 & 30 \\ -30 & 56 \\ -23 & 20 \\ -24 & 34 \\ \hline \end{array} ight\}$	-25 33	
	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	172 36 172 40 172 40 172 40	Т. Ү. Sм. R. Т.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} s.w. \ _{2} \ s.\\ s.w. \ _{1} \ _{2} \ w.\\ s.s.w. \ _{8} \ _{8} \ _{8} \ .\\ \end{array}$		+ 7 30 + 8 04 + 4 11 0 00 0 00	$ \begin{array}{c cccc} -25 & 06 \\ -22 & 57 \\ -27 & 43 \\ -23 & 26 \\ -24 & 08 \end{array} $	25.55	
30 p.m. 31 a.m.	$ \begin{array}{r} -64 & 37 \\ -64 & 44 \\ -64 & 46 \\ -64 & 48 \end{array} $	172 40 172 50 172 50	S. R. R. R. S.	$ \begin{array}{r} -26 & 01 \\ -25 & 03 \\ -23 & 04 \\ -22 & 43 \\ -22 & 13 \end{array} $	S. S.S.E. S.S.E. S.S.E. S.S.E.	-81 16	0 00 - 4 11 - 4 11 - 4 11 - 4 25	$ \begin{array}{c cccc} -26 & 01 \\ -29 & 14 \\ -27 & 15 \\ -26 & 54 \\ -26 & 38 \end{array} $	-25 57	
	$ \begin{array}{rrr} -65 & 22 \\ -65 & 23 \\ -65 & 25 \\ -65 & 25 \end{array} $	172 25 172 21 172 21 172 21 172 16	O. S. O. S. T.	$ \begin{array}{rrrr} -19 & 39 \\ -22 & 06 \\ -21 & 33 \\ -22 & 15 \\ -22 & 36 \end{array} $	S.S.E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E. s. by E. s. by E. s. by E.	$-81 \ 45 < $	- 5 24 - 3 20 - 2 15 - 2 15 - 2 15	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-25 06	
31 p.m.	$ \begin{array}{r} -65 & 31 \\ -65 & 31 \\ -65 & 32 \end{array} $	172 16 172 16 172 16 172 14 171 34	T. Y. S. T. T.	$\begin{array}{c c} -23 & 00 \\ -27 & 33 \\ -22 & 33 \\ -24 & 02 \\ -29 & 03 \end{array}$	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ W. S.		$\begin{array}{cccc} - & 1 & 05 \\ + & 1 & 05 \\ & 0 & 00 \\ & 0 & 00 \\ & & 0 & 0 \end{array}$	$ \begin{array}{c cccc} -24 & 05 \\ -26 & 28 \\ -22 & 33 \\ -24 & 02 \\ -29 & 03 \end{array} $		
1841.	$ \begin{array}{c cccc} -66 & 07 \\ -66 & 09 \end{array} $	171 34 171 34 171 32	SM. S. T. R.	$ \begin{array}{rrrr} -29 & 23 \\ -30 & 05 \\ -30 & 38 \\ -30 & 39 \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-82 30 \	+ 2 30	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-27 11	
Jan. 1 A.M. 1 P.M. 2 A.M.	$ \begin{array}{rrrr} -66 & 20 \\ -66 & 28 \\ -66 & 20 \\ -66 & 20 \end{array} $	170 48 169 13 169 13	W. S. R. T. T.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.w. by w. s.s.w. s.s.w. s.e. E.s.e.		$\begin{array}{c} + 9 & 18 \\ + 4 & 50 \\ + 4 & 50 \\ - 8 & 47 \\ -11 & 11 \end{array}$	$ \begin{array}{c cccc} -26 & 27 \\ -27 & 30 \\ -27 & 54 \\ -29 & 05 \\ -28 & 46 \end{array} $	-28 21	
	$ \begin{array}{rrrr} -66 & 20 \\ -66 & 20 \\ -66 & 20 \end{array} $	169 13 169 13 169 41 169 41	SM. T. Y. S. T.	$\begin{array}{rrrrr} -22 & 21 \\ -18 & 44 \\ -17 & 53 \\ -17 & 08 \\ -17 & 01 \end{array}$	s.e. by e. s.e. by e. s.e. by e. e.s.e.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$egin{array}{c c} -31 & 08 \\ -28 & 55 \\ -28 & 04 \\ -27 & 19 \\ -28 & 12 \\ \end{array}$		
	$ \begin{array}{c cccc} -66 & 20 \\ -66 & 24 \end{array} $		R. R.	$ \begin{array}{c cccc} -16 & 33 \\ -17 & 52 \end{array} $	E.S.E.	$-82 30 \Big\langle \Big $	-11 11 -11 11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-27 21	

1841.	Posit	tion.	Initials.	Declination observed.	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
	Lat.	Long.	Init	observed.	ship's head.		attraction.	Declination.	tion.	Ren
Jan. 2 A.M.	-66 30	169 44	T. W.	$-35 \ 14$ $-35 \ 45$	w.n.w. $\frac{1}{2}$ w. n.w. by w.	−82 30 ⟨	+10 55 + 9 18	$ \begin{array}{c c} -2\mathring{4} & 19 \\ -26 & 27 \\ -26 & 13 \end{array} $	$-\mathring{2}$ 7 $\acute{2}$ 1	
4 а.м.	$ \begin{array}{rrrr} -66 & 30 \\ -66 & 30 \\ -66 & 29 \\ -65 & 28 \\ -65 & 28 \end{array} $	169 46 169 48 171 47	R. S. O. S. O.	$ \begin{vmatrix} -35 & 31 \\ -34 & 28 \\ -31 & 46 \\ -20 & 09 \\ -18 & 33 \end{vmatrix} $	N.W. by W. N.N. W. $\frac{1}{2}$ W. N.N.W. S.E. by S. S.E.		$\begin{vmatrix} + & 9 & 18 \\ + & 5 & 11 \\ + & 4 & 11 \\ - & 6 & 35 \\ - & 8 & 15 \end{vmatrix}$	$\begin{bmatrix} -26 & 13 \\ -29 & 17 \\ -27 & 35 \end{bmatrix}$ $\begin{bmatrix} -26 & 44 \\ -26 & 48 \end{bmatrix}$	i i	
	$ \begin{array}{r rrr} -65 & 28 \\ -65 & 28 \\ -65 & 28 \\ -65 & 28 \end{array} $	171 47 171 47 171 47 171 56	W. T. T. W.	$ \begin{array}{r rrrr} -19 & 43 \\ -17 & 46 \\ -17 & 28 \\ -16 & 43 \end{array} $	s.e. by e. e. by s. $\frac{3}{4}$ s. e. by s. $\frac{3}{4}$ s. E. by s. $\frac{1}{2}$ s.	-82 0	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{vmatrix} -29 & 16 \\ -28 & 24 \\ -28 & 06 \\ -27 & 28 \end{vmatrix} $	$-27 \ 34$	
4 р.м.		172 50 173 06 173 06	R. R. T. T.	$ \begin{array}{r rrrr} -15 & 21 \\ -15 & 44 \\ -16 & 14 \\ -17 & 00 \end{array} $	s. 79° E. s. 74° E. E. by s. E.S.E.		$ \begin{array}{c cccc} -11 & 00 \\ -10 & 45 \\ -11 & 00 \\ -10 & 30 \end{array} $	$ \begin{array}{c cccc} -26 & 21 \\ -26 & 29 \\ -27 & 14 \\ -27 & 30 \end{array} $		
		173 32 173 32	R. W. R. R.	$ \begin{array}{r rrr} -18 & 22 \\ -14 & 08 \\ -17 & 26 \\ -18 & 59 \\ -18 & 25 \\ \end{array} $	s. 67° e. E.S.E. S. 72° E. S. 63° E.		$ \begin{array}{c cccc} -10 & 30 \\ -10 & 12 \\ -10 & 17 \\ -9 & 45 \\ 10 & 10 \end{array} $	$egin{bmatrix} -28 & 52 \ -24 & 20 \ -27 & 43 \ -28 & 44 \ -28 & 47 \ \end{bmatrix}$		
		173 32 173 55 173 55	Sм. Т. R. R. Y.	$ \begin{array}{r rrr} -18 & 35 \\ -17 & 55 \\ -18 & 08 \\ -19 & 42 \\ -19 & 16 \end{array} $	E.S.E. E.S.E. S. 68° E. S.E. by E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	-81 45	$ \begin{array}{r rrrr} -10 & 12 \\ -10 & 12 \\ -10 & 12 \\ -9 & 45 \\ -8 & 38 \end{array} $	$egin{array}{c c} -28 & 47 \\ -28 & 07 \\ -28 & 20 \\ -29 & 27 \\ -27 & 54 \\ \end{array}$	-28 08	
5 A.M.	$ \begin{array}{rrr} -65 & 32 \\ -65 & 34 \\ -66 & 39 \end{array} $	173 55 173 55 174 14	Т. R. Y. Sм.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by E. $\frac{1}{2}$ E. s.E. s.E. $\frac{1}{2}$	-82 30 {	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} & 27 & 34 \\ & -27 & 10 \\ & -30 & 44 \\ & -36 & 50 \\ & -30 & 28 \end{array} $		
5 р.м.	$ \begin{array}{r rrr} -67 & 12 \\ -67 & 12 \end{array} $	174 41 174 42 174 42	R. T. Y.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. s.s.e. s. by e. s. $\frac{3}{4}$ e.		$ \begin{array}{c cccc} - & 8 & 47 \\ - & 5 & 11 \\ - & 2 & 42 \\ - & 2 & 01 \\ \hline \end{array} $	$ \begin{array}{c cccc} -33 & 16 & \\ -32 & 31 & \\ -32 & 11 & \\ \end{array} $		
		174 42 174 42	Y. R. T. T.	$ \begin{array}{r} -27 & 59 \\ -18 & 03 \\ -17 & 25 \\ -18 & 05 \end{array} $	S.S.E. ½ E. E.S.E. E.S.E. S.E. by E.	-83 00<	$\begin{array}{rrrr} - & 6 & 25 \\ -11 & 57 \\ -11 & 57 \\ -10 & 53 \end{array}$	$ \begin{array}{c cccc} -34 & 24 \\ -30 & 00 \\ -29 & 22 \\ -28 & 58 \end{array} $	-31 29	
	$ \begin{array}{rrrr} -67 & 23 \\ -67 & 23 \\ -67 & 27 \\ -67 & 28 \end{array} $	174 42 174 42 174 51	T. R. R. R.	$ \begin{array}{rrrr} -17 & 13 \\ -18 & 07 \\ -18 & 44 \\ -21 & 06 \end{array} $	E.S.E. E.S.E. S.E.		$ \begin{array}{rrrr} -11 & 57 \\ -11 & 57 \\ -11 & 57 \\ -9 & 23 \end{array} $	$ \begin{array}{c cccc} -29 & 10 \\ -30 & 04 \\ -30 & 41 \\ -30 & 29 \end{array} $		
6 л.м.	$ \begin{array}{r r} -67 & 29 \\ -67 & 30 \end{array} $	174 51 174 51	T. R. R. O.	$ \begin{array}{r} -26 & 53 \\ -29 & 42 \\ -26 & 31 \\ -29 & 01 \end{array} $	S.S.E. S. ³ / ₄ E. S.S.E. S.S.E.		$ \begin{array}{rrrrr} & 5 & 11 \\ & 2 & 01 \\ & 5 & 11 \\ & 5 & 33 \end{array} $	$ \begin{array}{c cccc} -32 & 04 \\ -31 & 43 \\ -31 & 42 \\ -34 & 34 \end{array} $		
	$ \begin{array}{r rrr} -67 & 50 \\ -67 & 52 \\ -67 & 52 \end{array} $	175 00 175 01 175 01	S. S. O. T.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S.S.E. S.S.E. S.S.E. S.S.E. ½ E.		$ \begin{array}{rrrrr} & 5 & 33 \\ & 5 & 33 \\ & 5 & 33 \\ & 6 & 46 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
	$ \begin{array}{r rrr} -68 & 00 \\ -68 & 00 \\ -68 & 00 \end{array} $	175 00 175 00 175 00	Y. S. T. W.	$ \begin{array}{c cccc} & 27 & 00 \\ & -27 & 01 \\ & -27 & 42 \\ & -26 & 58 \end{array} $	S.S.E. S.S.E. S.S.E. S.S.E. \frac{1}{2} E.	-83 30	$ \begin{array}{rrrrr} & 5 & 33 \\ & 5 & 33 \\ & & 5 & 33 \\ & & 6 & 46 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-34 04	
	$ \begin{array}{rrr} -68 & 05 \\ -68 & 05 \\ -68 & 05 \end{array} $	175 10 175 14 175 14	T. R. R.	$ \begin{array}{rrr} -28 & 18 \\ -29 & 51 \\ -43 & 7 \end{array} $	S.S.E. S.S.E. N.W.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
	-08.12	175 14	R.	-24 56	S.E. $\frac{I}{2}$ S.	Ų	- 9 02	-33 58		

1841.	Posid		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
1841. Jan. 7 P.M. 8 A.M. 9 A.M. 10 P.M.	Lat. -68 32 -68 32 -68 32 -68 32 -68 32 -68 32 -68 32 -68 30 -68 30 -68 30 -68 55 -68 55 -68 55 -70 31 -70 32 -70 34 -70 34 -70 34 -70 34 -70 52 -71 02	Long. 175 49 175 49 175 49 175 49 175 49 175 55 176 35 176 35 176 35 176 32 176 24 176 24 176 24 176 28 172 53 172 53 172 52 172 25 172 25 172 27 172 27 172 27	T. T. W. SM. T. R. R. T. T. S. T. Y. R. S. Y. O. T. W. R. R. R. T. Y. SM. T. SM. T. S. R. R. T. Y. SM. T. S. R. R. T. Y. SM. T. S. C. R. R. T. T. S. T. S. T. S. C. R. R. T. T. S. T. S. T. S. C. R. R. T. T. S. T. S.			-83 35 \\ -83 45 \\ -85 02* \\ -85 50 \	for ship's attraction.	Declination. -32 37 -33 45 -32 28 -35 08 -33 18 -35 01 -34 09 -35 51 -33 06 -34 16 -33 32 -33 18		Observed on ice.
11 р.м.	$\begin{array}{ c c c c c } -71 & 21 \\ -71 & 21 \\ -71 & 21 \\ -71 & 21 \\ -71 & 22 \\ -71 & 22 \\ -71 & 24 \\ -71 & 24 \\ -71 & 24 \end{array}$	170 52 170 52 170 52 170 52 170 56 170 56	R. T. W. Y. T. S. O. T. S.	-48 45	s. by w.	-85 53	+ 4 20	-44 25 -43 42 -41 07 -44 35 -44 41 -43 25 -43 05 -45 14	-44 01	
12 P.M. 13 P.M. 15 A.M.	$ \begin{bmatrix} -71 & 52 \\ -71 & 52 \\ -72 & 07 \\ -71 & 46 \\ -71 & 46 \\ -71 & 46 \\ -71 & 54$	171 11 171 11 172 18 171 57 171 57	S.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N.E. by E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. S. by W. $\frac{1}{2}$ W. S. by W. $\frac{1}{2}$ W. S. by W. $\frac{1}{2}$ W. S. by S. E. by S	-86 00 { -86 00 {	-13 38 -13 38 -21 06 + 6 40 + 6 40 + 8 52 -22 11 -22 11 -22 11 -21 36 -22 19	-41 22 -44 14 -48 46 -42 42 -41 42 -44 54 -42 32 -46 24 -47 02 -47 11 -45 08 -46 34	-44 24 -48 12	

*
$$\psi'$$
 at West = -59° 05' ψ' at South = -41 12 Diff. 17° 53' = ship's attraction at West:
$$\frac{\sin 17^{\circ} 53'}{a} = \tan \theta; \frac{\sin 17^{\circ} 53'}{\cdot 0267} = 1.150 = \tan 85^{\circ} 02'.$$

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean	Remarks.
1011.	Lat.	Long.	Init	observed.	ship's head.		attraction.	Declination.	Declination.	Rem
Jan. 15 P.M.	$ \begin{array}{rrr} -71 & 53 \\ -71 & 53 \\ -71 & 53 \end{array} $	172 01 172 01 172 01 172 01 172 01 171 36	S. O. T. W. R.	$ \begin{vmatrix} -29 & 28 \\ -27 & 43 \\ -25 & 33 \\ -26 & 08 \\ -59 & 31 \end{vmatrix} $	E. $\frac{1}{2}$ S. E. $\frac{3}{4}$ N. E. $\frac{1}{2}$ N. E. S.S.W. $\frac{1}{2}$ W.	_86° 00́<	$\begin{array}{ccccc} -22 & 19 \\ -22 & 00 \\ -22 & 08 \\ -22 & 27 \\ +10 & 50 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-48 12	
17 г.м.	-7200	171 32 174 00 174 02	R. W. T. T. S.	$\begin{array}{r} -26 & 05 \\ -33 & 28 \\ -31 & 37 \\ -32 & 41 \\ -35 & 05 \\ -35 & 58 \end{array}$	E. $\frac{1}{2}$ S. S.E. by E. S.E. $\frac{3}{4}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	-86 00	-22 19 -19 02 -18 20 -17 40 -17 40 -17 40	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-51 41	
18 р.м.	$ \begin{array}{rrrr} & 72 & 17 \\ & 73 & 00 \\ & 73 & 02 \\ & -73 & 02 \\ & -73 & 02 \\ & -73 & 02 \\ \end{array} $	174 14 176 14 176 10 176 10 176 10	O. R. T. R. S. O.	$\begin{array}{c} -33 & 15 \\ -35 & 12 \\ -65 & 04 \\ -64 & 35 \\ -65 & 52 \\ -65 & 50 \end{array}$	s.e. $\frac{1}{2}$ e. E.s.e. s.w. by s. s.w. by s. s.w. by s.		$ \begin{array}{rrrr} -17 & 40 \\ -22 & 02 \\ +13 & 23 \\ +13 & 23 \\ +13 & 23 \end{array} $	$ \begin{array}{c cccc} -50 & 55 \\ -57 & 14 \\ -51 & 41 \\ -51 & 12 \\ -52 & 29 \end{array} $		
	$ \begin{array}{rrr} -73 & 02 \\ -73 & 02 \\ -73 & 02 \\ -73 & 02 \\ -73 & 01 \end{array} $	176 03 176 03 175 57	R. T. R. R. R.	-65 54 -68 09 -65 02 -63 34 -63 37 -62 45	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-86 10		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-52 41	
19 а.м.	-72 59 $-72 36 $ $-72 36 $ $-72 36$	175 11 173 40 173 40 173 40 173 40	R. T. W. Y. T.	$ \begin{array}{rrrr} -62 & 43 \\ -64 & 15 \\ -66 & 21 \\ -66 & 12 \\ -64 & 49 \\ -64 & 11 \\ -67 & 43 \end{array} $	$ \begin{array}{c c} s.s.w. & \frac{3}{4} & w. \\ s.w. & \frac{1}{2} & w. \\ s.w. & by & s. \\ s.w. & \frac{3}{4} & s. \end{array} $	$-86 00 \begin{cases} \\ \\ \\ \\ \\ \end{cases}$	$ \begin{array}{r} +12 & 22 \\ +16 & 15 \\ +17 & 37 \\ +12 & 49 \\ +13 & 45 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-50 31	
19 р.м.	$ \begin{array}{rrrr} -72 & 31 \\ -72 & 34 \\ -72 & 34 \\ -72 & 34 \\ -72 & 34 \end{array} $	173 40 173 42 173 42 173 45 173 45	O. T. T. Y. O.	-53 57 -43 53 -44 43 -41 10 -43 34	S.S.E.	$-86 \ 10$	$ \begin{array}{ccccc} + & 6 & 27 \\ - & 6 & 55 \\ - & 6 & 55 \\ - & 9 & 14 \\ - & 9 & 14 \end{array} $	$ \begin{array}{c cccc} -51 & 28 \\ -47 & 30 \\ -50 & 48 \\ -51 & 38 \\ -50 & 24 \\ -52 & 48 \end{array} $	-51 54	
22 а.м.	$ \begin{array}{rrrr} -72 & 34 \\ -72 & 36 \\ -72 & 50 \\ -74 & 10 \\ -74 & 10 \\ -73 & 53 \end{array} $	173 40 173 10 169 28 169 28 170 57	R. R. R. S. O. S.		s.s.e. s. by e. s. by e. $\frac{1}{2}$ e. e. $\frac{3}{4}$ s. e. $\frac{1}{4}$ s. w. by N. $\frac{1}{2}$ N.		$ \begin{array}{c cccc} - & 6 & 55 \\ - & 28 & 37 \\ - & 28 & 53 \end{array} $	$ \begin{array}{c cccc} -52 & 57 \\ -53 & 01 \\ -56 & 10 \\ -63 & 02 \\ -60 & 40 \\ -61 & 01 \end{array} $		
-	$ \begin{array}{rrrr} -73 & 53 \\ -73 & 53 \\ -73 & 57 \\ -73 & 57 \\ -73 & 57 \\ -73 & 54 \\ -73 & 54 \end{array} $	170 57 170 57 171 40 171 40 171 40 171 55	S. S. T. T. Y. T.	-78 56 -35 43 -48 46 -38 00 -36 56 -37 13	N.N.W. E. by N. N.N.E. $\frac{3}{4}$ E. E. by N. E. $\frac{3}{4}$ N. E. by s. E. by s.	-86 50	$egin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-63 38	
22 P.M.	$ \begin{array}{rrrr} -73 & 54 \\ -73 & 55 \\ -73 & 58 \\ -73 & 59 \\ -73 & 59 \\ -74 & 00 \\ \end{array} $	172 00 172 04 172 16 171 58 171 58 171 43	O. O. S. S. T. R.	-31 25 -36 52 -61 29 -65 50 -67 45 -66 08	E. by s. ½ s. E.s.E. s. by w. s. ½ w. s. by w.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} -59 & 06 \\ -63 & 45 \\ -61 & 29 \\ -60 & 11 \\ -64 & 56 \\ -60 & 29 \end{array} $		
	$ \begin{array}{rrrrr} -74 & 00 \\ -74 & 01 \\ -74 & 04 \\ -74 & 04 \\ -74 & 04 \\ -74 & 04 \\ \end{array} $	171 34 171 27 171 27 171 27	R. R. T. W.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by w. E. $\frac{1}{2}$ s. E. by s. $\frac{1}{2}$ s. E. $\frac{3}{4}$ s. E. $\frac{1}{2}$ N. E. by s.	-30 30	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c c} -63 & 43 \\ -67 & 16 \\ -67 & 45 \\ -64 & 37 \\ -67 & 25 \\ -66 & 15 \end{array} $	-64 25	

1841.	Position.	ials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
1041.	Lat. Long	Initials.	observed.	ship's head.		attraction.	Declination.	tion.	Rem
Jan. 25 а.м.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 T. 6 T. 8 T. 12 Y.	$ \begin{array}{r rrrr} - & 77 & 36 \\ - & 37 & 17 \\ - & 37 & 25 \\ - & 39 & 15 \end{array} $	E.S.E.	$\begin{bmatrix} & & & & \\ & & & & \\ & -87 & 20 \end{bmatrix}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} & 69 & 11 \\ & 68 & 15 \\ & 68 & 55 \\ & 66 & 32 \\ & & 71 & 43 \end{array} $	。, — 69 47	
25 p.m.	-74 41 169 -74 41 169 -74 45 169 -74 45 169 -74 47 168 -74 47 168 -74 47 168	2 T. R. R. R. R. S. S.	- 43 14 - 81 36 - 81 08 - 86 28 - 87 19	S.E. by E. $\frac{1}{2}$ E. S.E. by E. $\frac{1}{4}$ E. S.S.W. S.S.W. S.S.W. S.S.W. S.S.W.		$\begin{array}{r} -30 \ 45 \\ -30 \ 00 \\ +12 \ 23 \\ +12 \ 23 \\ +15 \ 13 \\ +12 \ 23 \\ +15 \ 13 \end{array}$	$ \begin{array}{ccccc} & -70 & 39 \\ & -73 & 14 \\ & -69 & 13 \\ & -68 & 45 \\ & -71 & 15 \\ & -74 & 56 \\ & -70 & 22 \end{array} $		
26 a.m. 27 a.m.	$egin{array}{cccccccccccccccccccccccccccccccccccc$	22 R. 22 R. 0 T. 08 R. 25 T. 50 S.	- 85 15 - 93 49 - 91 01 - 43 39 - 94 09 - 75 49	$ \begin{array}{c} s.s.w. \\ s.w. \frac{1}{2} w. \\ s.w. by s. \\ s.e. \frac{1}{2} E. \\ s.w. by s. \end{array} $	-87 10	$\begin{array}{r} +12 & 23 \\ +25 & 10 \\ +20 & 33 \\ -25 & 10 \\ +18 & 03 \\ -15 & 04 \end{array}$	$ \begin{array}{c cccc} & 72 & 52 \\ & 68 & 39 \\ & 70 & 28 \\ & 68 & 49 \\ & 76 & 06 \\ & 90 & 53 \end{array} $	— 71 08	
	$\begin{vmatrix} -75 & 36 & 168 \\ -75 & 36 & 168 \end{vmatrix}$	50 S. R. 23 Y. 23 T. R.	-100 55 -100 26 - 99 06 - 45 19 - 46 18	$\begin{array}{c c} \text{S.s.w.} & \frac{1}{2} \text{ w.} \\ \text{S.s.w.} & \\ \text{S.s.w.} & \\ \text{E.s.e.} & \\ \text{S.e. by E.} & \frac{1}{2} \text{ E.} \end{array}$	−87 40 ₹	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{vmatrix} -84 & 02 \\ -83 & 01 \\ -81 & 58 \end{vmatrix}$	— 84 58	
29 а.м.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	33 R. 43 SM 59 T. 59 T. 00 T.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. $\frac{1}{2}$ E. N. $\frac{1}{4}$ W. N. by W. $\frac{1}{2}$ W. N. N. W. $\frac{1}{2}$ W. N. by W. $\frac{1}{2}$ W.	-87 00{	$ \begin{vmatrix} -35 & 40 \\ -33 & 37 \\ -2 & 48 \\ +1 & 24 \\ +8 & 20 \\ +13 & 38 \\ +8 & 20 \end{vmatrix} $	$ \begin{vmatrix} -83 & 35 \\ -81 & 18 \end{vmatrix} $ $ \begin{vmatrix} -107 & 07 \\ -104 & 20 \\ -105 & 51 \\ -105 & 15 \\ -100 & 00 \end{vmatrix} $	-104 25	
29 р.м. 30 а.м.	$ \begin{array}{c cccc} -77 & 49 & 177 \\ -77 & 50 & 178 \\ -77 & 51 & 178 \end{array} $	00 T. 30 T. 46 T. 13 R. 33 R.		S.E. by S. $N \cdot \frac{1}{4} W \cdot N \cdot \frac{1}{2} W \cdot N \cdot \frac{3}{4} E \cdot$	$\begin{bmatrix} -86 & 40 \\ -86 & 20 \end{bmatrix}$	$\begin{vmatrix} + & 8 & 20 \\ + & 4 & 12 \\ -15 & 22 \\ + & 1 & 15 \\ + & 2 & 30 \\ - & 3 & 45 \\ +10 & 35 \end{vmatrix}$	$ \begin{bmatrix} -108 & 06 \\ -100 & 18 \end{bmatrix} $ $ -106 & 16 \\ -103 & 37 \\ -107 & 37 \\ -103 & 55 \\ -96 & 17 $	105 21 96 17	
31 A.M. 31 P.M.		41 S. 00 T. 00 T. 00 SM 57 S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. $\frac{1}{2}$ N. N.E. by E. $\frac{1}{4}$ E. N.E. by N. N.N.E. N.N.E.		$ \begin{array}{c cccc} -13 & 39 \\ -19 & 13 \\ -11 & 58 \\ -8 & 10 \\ -10 & 04 \\ -10 & 04 \end{array} $	$\begin{bmatrix} -84 & 34 \\ -80 & 10 \end{bmatrix}$		
Feb. 1 A.M	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	01 SM 01 T. 00 T. 00 T. 00 O	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.w.byw.½w. s.w. by w. w. by s.½ s. N.N.W. s.E. by s. s. s.E. by s.	86 00	$\begin{array}{c} -10 & 04 \\ +20 & 02 \\ +19 & 02 \\ +21 & 36 \\ +8 & 10 \\ -12 & 49 \\ -12 & 49 \end{array}$	 - 83 56 (82 29	
1 Р.М	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26 R. 26 R. 24 R.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by E. 5 s.s.E. s. s.e. by s.	-85 50 \	$\begin{bmatrix} -4 & 17 \\ -8 & 30 \\ -12 & 18 \\ -21 & 27 \end{bmatrix}$	$ \begin{vmatrix} -90 & 09 \\ -92 & 55 \\ -92 & 07 \end{vmatrix} $	_ 91 0 7	

T	1841.	Posi	tion.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's	Corrected Declination.	Mean Declina-	Remarks.
	·····	Lat.	Long.	Ini	observed.	sinp s nead.	:	attraction.	Decimation.	tion.	Ren
	Feb. 1 P.M.	-7709	188 24 188 24 188 24	R. R. R.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	E.S.E. > S.E. S.S.E.	-85 50<	$ \begin{vmatrix} $	$ \begin{vmatrix} -90 & 32 \\ -91 & 15 \\ -90 & 52 \end{vmatrix} $	_91 ó 7	
	2 A.M.	-77 09 $-77 09$ $-77 34$ $-77 34$	188 15 188 15 186 56 186 03	R. T. S. O.	- 79 56 - 79 14 - 72 39 - 70 42	s.e. by s. s.e. by s. e.s.e. s.e. by e. ½ e.		$ \begin{array}{c cccc} -12 & 18 \\ -12 & 18 \\ -22 & 02 \\ -20 & 58 \end{array} $	$ \begin{array}{c cccc} -92 & 14 \\ -91 & 32 \\ -94 & 41 \\ -91 & 40 \end{array} $		
		-77 34 $-77 35 $ $-77 35 $ $-77 35$	186 15 186 15 186 55 186 55 186 55	S. O. T. T.	-7309 -7537	s.e. by e. $\frac{1}{4}$ e. s.e. by e. $\frac{1}{2}$ e. s.e.	−86 10 ₹	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{vmatrix} -92 & 41 \\ -93 & 41 \\ -92 & 59 \\ -94 & 07 \\ -92 & 37 \end{vmatrix} $	-93 22	
	2 р.м.	$ \begin{array}{rrr} -77 & 43 \\ -77 & 45 \\ -77 & 45 \\ -77 & 47 \end{array} $	187 00 187 00 186 52	S. W. R. R. T.	- 76 49 - 72 04 - 69 50 - 72 25 - 69 57	s.e. by $e. \frac{1}{2} e.$ E. by $s. \frac{1}{2} s.$		$ \begin{array}{rrrr} -17 & 00 \\ -22 & 02 \\ -19 & 55 \\ -20 & 58 \\ -22 & 39 \end{array} $	$ \begin{array}{c c} -93 & 49 \\ -94 & 06 \end{array} $ $ -89 & 45 \\ -93 & 23 \\ -92 & 36 \end{array} $		
Market Committee of the Property Confession of		$-77 ext{ } 45 \\ -77 ext{ } 46$	186 52 186 52 186 52 186 51 186 51	Sм. R. R. S. T.	$\begin{array}{ c c c c c } - & 72 & 53 \\ - & 73 & 10 \\ - & 72 & 56 \\ - & 74 & 47 \\ - & 74 & 38 \\ \end{array}$	E.S.E. E.S.E. E.S.E. S.E. by E. $\frac{1}{2}$ E.	-86 10	$\begin{array}{rrrr} -22 & 02 \\ -22 & 02 \\ -22 & 39 \\ -22 & 02 \\ -20 & 58 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-94 14	
		$-77 ext{ } 47 \\ -77 ext{ } 56$	186 51 186 51 186 51 186 44 186 44	R. R. T. R. R.	$\begin{array}{rrrrr} -&75&01\\ -&74&22\\ -&72&32\\ -&71&21\\ -&75&38 \end{array}$	E.S.E. E. E. $\frac{1}{2}$ N. E. E.N.E.		-22 02 -23 36 -23 16 -23 36 -21 23	$ \begin{array}{c cccc} -97 & 03 \\ -97 & 58 \\ -95 & 48 \\ -94 & 57 \\ -97 & 01 \end{array} $		
	3 а.м.	$ \begin{array}{rrr} -77 & 57 \\ -77 & 59 \\ -78 & 00 \\ -77 & 32 \end{array} $	186 44 186 47	Т. R. R. Sм. T.	$\begin{array}{ccccc} - & 74 & 27 \\ - & 72 & 03 \\ - & 72 & 10 \end{array}$	$\begin{bmatrix} E & \frac{1}{4} & N & \\ E & & \\ E & & \\ E & & \\ $	−86 10 ≺	$ \begin{array}{r} -23 & 26 \\ -23 & 36 \\ -22 & 02 \\ +22 & 40 \\ +22 & 02 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-96 14	
	4 A.M.	$ \begin{array}{rrr} -77 & 05 \\ -77 & 06 \\ -77 & 06 \\ -77 & 54 \end{array} $	192 32 192 33 192 33 192 30	S. T. O. Y.	$\begin{array}{rrrrr} - & 77 & 52 \\ - & 77 & 44 \\ - & 76 & 31 \\ - & 62 & 21 \end{array}$	s. by E. s. ½ E. s. ½ E. E.N.E.	$-85\ 50$	_ 4 18 _ 1 04 _ 2 08 _ 19 31	$ \begin{array}{c cccc} -82 & 10 \\ -78 & 48 \\ -78 & 39 \\ -81 & 52 \\ \end{array} $		
and an address of the second second second	4 P.M.	$ \begin{array}{rrr} -77 & 54 \\ -76 & 57 \\ -77 & 6 \end{array} $		S. O. T. R. R. R.	-61 29 $-62 14$	E.N.E. by E. N.E. by N. $\frac{1}{2}$ E. by N. $\frac{1}{2}$ N. E. by N.		$ \begin{array}{cccc} -19 & 31 \\ -17 & 24 \\ -18 & 27 \\ -19 & 24 \\ -20 & 04 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-81 50	an and a state of the state of
	5 A.W.	$ \begin{array}{rrr} -77 & 9 \\ -77 & 13 \\ -77 & 13 \end{array} $	192 43 192 51 192 51 192 49	R. T.	-62 31 $-68 53$ $-67 45$	E. by N. E. by N. $\frac{1}{2}$ N. N.E. by E. $\frac{3}{4}$ E. S.S.W. $\frac{1}{2}$ W.	$-85 \ 40 \left\{ \begin{array}{c} -85 \ 40 \end{array} \right\}$	$ \begin{array}{c cccc} -20 & 04 \\ -19 & 24 \\ -18 & 13 \\ +10 & 00 \end{array} $			
AND TO SELECT SECURITY OF THE PROPERTY OF THE		$ \begin{array}{rrr} -77 & 8 \\ -77 & 8 \\ -77 & 8 \\ -77 & 8 \end{array} $	192 59 192 59 192 59 192 59 192 59 192 59	O. T. T. T.	- 63 33 - 77 06 - 83 12 - 92 23	s. by E. s. s. s.s.w. ½ w.	_85 40		$ \begin{array}{c cccc} -84 & 11 \\ -81 & 14 \\ -83 & 12 \\ -82 & 22 \end{array} $	82 26	
The State of the S		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	192 50 191 32 191 32	т. R.	- 83 00 - 89 26	s.s.w. $\frac{1}{2}$ w. s. $\frac{1}{4}$ w. s. by w. $\frac{1}{2}$ w. s. by E. $\frac{1}{2}$ E. s.E. $\frac{1}{2}$ s.	$-85 \ 40 \left\{ \right $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-83 56	
-			191 32	к.	$\begin{array}{cccc} & 63 & 24 \\ & 66 & 30 \end{array}$	E. $\frac{1}{2}$ S. S.E. by E.		$ \begin{array}{c cccc} -20 & 30 \\ -17 & 34 \end{array} $	$ \begin{bmatrix} -83 & 54 \\ -84 & 04 \end{bmatrix} $		

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
	Lat.	Long.	lii Lii	observed.	ship's head.		attraction.	Declination.	tion.	Rem
Feb. 6 а.м.	$\begin{array}{c cccc} -\mathring{7}7 & 14 \\ -77 & 05 \\ -77 & 09 \\ -77 & 09 \\ -77 & 09 \end{array}$	189 2 188 50 188 50	S. Т. Sм. Т. Т.	- 87 49 - 88 18 - 83 07 - 85 52 - 58 23	s. by w. s. by w. s. ³ / ₄ w. s. ³ / ₄ w. E. by N.	_86 00	$\begin{array}{c} & & & \\ & + & 4 & 28 \\ & + & 4 & 28 \\ & + & 3 & 20 \\ & + & 3 & 20 \\ & -21 & 50 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-82 0 9	
7 А.М.	$ \begin{array}{rrr} -76 & 58 \\ -76 & 58 \\ -76 & 58 \\ -76 & 56 \end{array} $	186 40 186 40 186 40 186 40	T. T. T. S. O.	- 80 58 - 94 54 - 91 17 - 87 10 - 59 46 - 59 16 - 56 07	s.s.w. s. by w. $\frac{1}{2}$ w. E. $\frac{1}{2}$ s.	$-86 \ 05$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	- 83 12 - 84 52 - 82 15 - 80 25 - 82 38 - 82 08 - 79 00	-81 33	
7 г.м.	$\begin{array}{rrrr} -76 & 56 \\ -76 & 56 \\ -76 & 57 \\ -77 & 11 \\ -77 & 12 \\ \end{array}$	186 39 186 39 186 36 187 03 187 03	T. O. S. T. R. T. T.	- 57 38 - 57 12 - 60 09 - 68 38 - 68 31 - 70 01	E. $\frac{1}{2}$ S. E. by S. E. by S. $\frac{1}{2}$ S. E. by S. $\frac{1}{4}$ S. E. by S. $\frac{1}{2}$ S. S.E. by E. $\frac{1}{2}$ E.		-22 52 -22 43 -22 06 -21 54 -21 36 -20 02	- 80 30 - 79 55 - 82 15 - 80 32 - 90 07 - 90 03		
	-77 12 -77 12 -77 12 -77 14 -77 14 -77 14 -77 13	187 03 187 03 187 01 187 01 187 01	R. R. R. R. T. W.	- 66 16 - 67 27 - 81 21 - 74 43 - 72 20 - 72 00 - 71 29	s.e. by e. s.s.e. s.e. by s. s.e. s.e.	-86 00	$\begin{array}{rrrr} -19 & 02 \\ -19 & 02 \\ -8 & 52 \\ -12 & 49 \\ -16 & 15 \\ -16 & 15 \\ -16 & 15 \end{array}$	- 85 18 - 86 29 - 90 13 - 87 32 - 88 35 - 88 15 - 87 44	-87 29	
8 A.M.	$ \begin{array}{rrrr} -77 & 24 \\ -77 & 24 \\ -77 & 21 \\ -7$	186 19 186 22 186 22 186 22 186 22	S. O. T. Y. Y. T. O.	$ \begin{array}{r rrrr} - & 67 & 35 \\ - & 71 & 43 \\ - & 69 & 19 \end{array} $	E.S.E. E. by S. ½ S. E. ½ S. E.S.E. E.S.E.	-86 00	$\begin{bmatrix} -21 & 02 \\ -21 & 02 \\ -21 & 37 \\ -22 & 19 \\ -21 & 02 \\ -21 & 02 \\ -21 & 02 \\ -21 & 02 \\ \end{bmatrix}$	- 86 26 - 86 34 - 89 56 - 89 54 - 92 45 - 90 21 - 88 31	-89 19	
8 р.м.	-77 21 -77 30 -77 30 -77 30 -77 37	186 22 186 40 186 40 186 40 186 36	S. T. W. T. R. R.	- 67 38 - 71 42 - 70 31 - 69 39 - 67 40	E.S.E. E.S.E. E.S.E.	-86 00 {	$ \begin{array}{c cccc} -21 & 62 \\ -21 & 02 \\ -21 & 02 \\ -21 & 02 \\ -22 & 27 \\ -21 & 50 \\ -21 & 6 \end{array} $	- 88 40 - 91 44 - 91 33 - 92 06 - 89 30 - 93 57	-90 21	
	-77 47 -77 48 -77 48 -77 50 -77 50		S. O. T. W. R.	$\begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E. E.N.E. N.E. by E. $\frac{1}{2}$ E.	_86 00	$\begin{array}{c cccc} -20 & 23 \\ -20 & 23 \\ -20 & 23 \\ -19 & 18 \\ -20 & 23 \\ -20 & 23 \end{array}$	$ \begin{vmatrix} -94 & 27 \\ -94 & 40 \\ -95 & 58 \\ -95 & 56 \\ -100 & 13 \end{vmatrix} $	-95 52	
9 А.М.	-77 49 -77 50 -77 51 -77 53 -77 57	187 25 187 31 187 36 187 44 7 188 06 2 191 16	R. R. R. T. W.	- 79 29 - 75 32 - 77 19 - 80 42 - 95 31	N.E. by E. N.E. by E. N.E. by E. ½ E. N.E.	-86 00	$ \begin{array}{c ccccc} -18 & 11 \\ -18 & 11 \\ -19 & 18 \\ -15 & 20 \\ 0 & 00 \\ +13 & 57 \end{array} $	$ \begin{vmatrix} -97 & 40 \\ -93 & 43 \\ -96 & 37 \\ -96 & 02 \\ -95 & 31 \end{vmatrix} $	—96 00	
		191 16 191 07 191 07 190 23	T. Y. T.	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c c} S.w. \frac{1}{2} S. \\ S.w. \frac{1}{2} S. \\ S.w. by S. \end{array} $	$-85\ 50$	$\begin{vmatrix} +13 & 57 \\ +13 & 57 \\ +12 & 18 \end{vmatrix}$	$\begin{vmatrix} -95 & 20 \\ -94 & 46 \end{vmatrix}$	-93 43	

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
	Lat.	Long.	Init	observed.	ship's head.		attraction.	Declination.	tion.	Ren
Feb. 9 г.м.	$-\mathring{7}7 \ 57$ $-77 \ 56$ $-77 \ 56$ $-77 \ 54$ $-77 \ 54$	188 40 188 40 188 36	R. R. R. R.	-102 30 -110 29 -106 13 -105 51 -103 13	$\begin{array}{c} \text{s.s.w.} \\ \text{s.w.} \ \frac{1}{2} \text{ s.} \\ \text{s.s.w.} \ \frac{3}{4} \text{ w.} \\ \text{s.w. by s.} \\ \text{s.s.w.} \ \frac{1}{2} \text{ w.} \end{array}$	° ′ −86 00 {	+ 8 52 + 14 32 + 11 50 + 12 49 + 10 50	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	。	
10 а.м.	-77 51 $-77 50$ $-77 50$	188 24 188 06 188 06 187 59 187 38	R. R. S. S. T. Y.	-103 18 - 94 04 - 94 38 - 94 12 -110 56 - 97 53	S.S.W. $\frac{1}{2}$ W. S. $\frac{1}{4}$ W. S. S. W. $\frac{1}{2}$ W. S. S. W. $\frac{1}{2}$ W. S. by W.		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 92 28 - 93 00 - 94 38 - 94 12 - 93 18 - 93 25		
11 а.м.	$\begin{array}{rrrr} -77 & 38 \\ -77 & 40 \\ -77 & 48 \\ -77 & 48 \\ -77 & 48 \end{array}$	188 07 188 00 188 00 188 00 188 04	Т. Sм. S. O. T. O.	-101 54 -108 00 -108 49 -105 38 -106 04 - 74 47	s.s.w. by s. s.w. by s. s.w. $\frac{1}{2}$ s. s.w. by s.	-86 00	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 93 02 - 95 11 - 96 00 - 91 06 - 93 15 - 75 53	— 93 41	
11 A.M.	-76 46 -76 46 -76 46	188 40 188 40 188 40	S. S. S.		$ \begin{array}{c} s. \frac{1}{4} E. \\ s. by W. \frac{1}{2} W. \\ s. \\ s. W. \frac{1}{2} s. \\ N.W. \frac{1}{2} N. \end{array} $	-86 00	$ \begin{array}{r} -1 & 00 \\ +6 & 40 \\ 0 & 00 \\ +14 & 32 \\ +13 & 39 \end{array} $	$ \begin{bmatrix} -73 & 33 \\ -80 & 16 \\ -80 & 11 \\ -80 & 39 \\ -72 & 27 \end{bmatrix} $	— 77 53	
14 A.M. 15 P.M.	-7624	176 26 168 56	S. R. R. S.	$ \begin{array}{r rrrr} - & 98 & 02 \\ - & 91 & 24 \\ - & 85 & 31 \end{array} $	s. by w. $\frac{1}{2}$ w. s. by w. $\frac{3}{4}$ w. s. by e. $\frac{1}{4}$ e. s. by e. $\frac{1}{2}$ e.	-87 00 {	$\begin{vmatrix} + & 8 & 50 \\ + & 10 & 17 \\ - & 10 & 13 \\ - & 12 & 13 \end{vmatrix}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	- 85 10	
16 л.м.	-76 05 $-76 16$	168 11 165 33	O. R. S. T.	- 86 55	s. by E. $\frac{1}{2}$ E. s. by E. $\frac{3}{4}$ E. E. $\frac{1}{2}$ N.	-87 50	$ \begin{array}{c cccc} -12 & 13 \\ -14 & 13 \\ -45 & 47 \\ -37 & 32 \end{array} $	$ \begin{array}{c cccc} & 99 & 08 \\ & 99 & 23 \\ & 106 & 41 \\ & 106 & 44 \end{array} $	— 98 45	·
16	-76 20 $-76 20$ $-76 20$ $-76 30$	165 33 165 33 166 39	O. Y. T. R.	- 67 08 - 65 20 - 64 59 - 58 06	E.S.E. E.S.E.	$-87 53 \left\{ \right.$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c cccc} -104 & 40 \\ -107 & 38 \\ -107 & 17 \\ -104 & 19 \end{array} $	—106 13	
16 р.м.	-76 36 -76 36 -76 36 -76 36 -76 36 -76 36 -76 36 -76 37 -76 37	166 17 166 16 166 16 166 16 166 16 166 17 166 17 166 16	R. R. Y. Y. Y. R. R. R. R.	$ \begin{array}{rrrrr} -156 & 05 \\ -154 & 06 \\ -142 & 54 \\ -67 & 01 \\ -67 & 53 \end{array} $	E. by s. ½ s. N.N.W. ½ W. W.N.W. N.W. by N. W. W. by s. ½ s. s.W. ¼ W. s.W. ½ s. E.N.E. E. by s.	−87 53* ≺	-44 03 +19 46 +41 38 +23 31 +46 13 +44 03 +37 32 +29 45 -41 38 -45 19	-108 26 -116 33 -108 26 -114 53 -112 38 -112 55 -123 01 -116 34 -113 09 -108 39 -111 51	—113 <i>2</i> 3	
	$-76 37 \\ -76 37 \\ -76 37$	166 16	S. T. R.	- 66 32 - 73 45 - 73 40	E.S.E.		-45 19 -42 18 -37 32	$ \begin{array}{c cccc} -113 & 12 \\ -116 & 03 \\ -111 & 12 \end{array} $		

^{*} The inclination on the 16th of February is computed from the observed declinations with the head West -158° 51', and E. by S. -67° 12'. From these we have the approximate inclination $\theta = -87^{\circ}$ 52'. With this value of θ , $\psi' = -66^{\circ}$ 27' at East. Whence $\psi = -\frac{158^{\circ}}{2} \frac{51' + 66^{\circ}}{2} \frac{27'}{2} = -112^{\circ}$ 39'; δ at East or West $= 46^{\circ}$ 12'; and $\tan \theta = \frac{\sin 46^{\circ}}{a} \frac{12'}{a} = \frac{.7218}{.0267} = -87^{\circ}$ 53'.

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
1041.	Lat.	Long.	Init	observed.	ship's head.	incimation.	attraction.	Declination.	tion.	Rem
Feb. 17 A.M.	-76 44 $-76 44$	165 48 165 48	S. O. Y.	$-12\overset{\circ}{2}$ 02 -123 18 -124 51	s. by w. s. by w. s. by w.	。 /	+ 9 18 + 9 18 + 9 18	$ \begin{array}{c cccc} -11\overset{\circ}{2} & 4\overset{\checkmark}{4} \\ -114 & 00 \\ -115 & 33 \end{array} $	۰ /	
17 р.м.	-76 27 $-76 26$	164 18 164 11 164 02 164 02 164 02	R. R. R. T.	-7351	S. S. $\frac{1}{2}$ E. S. E. by E. $\frac{1}{4}$ E. S. E. $\frac{1}{2}$ E.	-88 05 {	0 00 0 00 -38 49 -43 52 -38 49	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-113 41	
18 а.м.	-76 16 -76 05 -76 06 -76 03	165 53 165 53 166 11 166 11 166 23 166 23	T. T. T. S. S.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. by s. E. by s. ½ s N.E. by N. W. N.W. W. N.W.	-88 0 4*{	$ \begin{array}{rrrr} -51 & 20 \\ -49 & 37 \\ -25 & 56 \\ +52 & 20 \\ +46 & 47 \\ +51 & 20 \end{array} $	$ \begin{array}{c cccc} -100 & 26 \\ -100 & 51 \\ -97 & 01 \\ -100 & 26 \\ -96 & 08 \\ -93 & 18 \end{array} $	— 99 41	
	-75 58 -75 58 -75 49 -75 45	167 04 167 04 167 32 167 32 167 30	T. T. R. R.	$\begin{array}{rrrrr} -&71&05\\ -149&32\\ -134&35\\ -132&32\\ -135&47 \end{array}$	s.w. by w. s.w. by w. s.w. by w.	-88 04	$ \begin{array}{rrrr} -25 & 56 \\ +52 & 20 \\ +42 & 07 \\ +42 & 07 \\ +42 & 07 \end{array} $	- 97 01 - 97 12 - 92 28 - 90 25 - 93 40	— 94 27	
19 p.m. 22 p.m.	-7446	167 30 167 53 167 53 166 40 166 40	R. R. T. R.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	_88 02 {	+37 47 +34 12 +34 12 -20 57 -20 13	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	- 74 48	
24 A.M. 24 P.M.	-70 14 $-70 14$ $-70 24$ $-70 26$	168 13 168 13 167 20 167 19	Y. T. S. R.	- 50 20 - 49 18 - 41 55 - 42 49	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-85 50	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	— 39 45	
25 p.m.	-70 07 -70 07 -70 06 -70 06 -70 04 -70 02 -70 02	167 32 167 35 167 11	R. T. R. T. T. R. S.	- 49 16 - 56 14 - 52 55 - 42 51	S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ W. S. N. by W. $\frac{3}{4}$ W. N.N.W. N.W.by W. $\frac{1}{2}$ W. S. by W. S. by W.	-85 50	+ 2 08 + 2 08 0 00 + 6 52 + 7 50 +18 27 +17 24 + 4 17	- 38 16 - 38 08 - 41 14 - 37 14 - 41 26 - 37 47 - 35 31 - 38 34	— 39·21	
26 A.M. 27 P.M.	-69 54 $-69 17$ $-69 17$ $-69 16$	168 00 167 49	R. S. R. O. S. P.	- 46 21 - 61 35 - 48 44 - 50 39 - 45 13	s. by w.	$-85 \ 28 \ \left\{ \right.$	+417 $+1816$ $+1327$ $+1512$ $+358$	- 42 04 - 43 19 - 35 17 - 35 27 - 41 15		
28 A.M.	$ \begin{vmatrix} -69 & 40 \\ -69 & 40 \\ -69 & 40 \\ -69 & 40 \end{vmatrix} $	167 39 167 14 167 14 167 25 167 25 167 27	R. SM. T. T. O. S.		s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E.	-85 45 \	$ \begin{array}{rrrrr} + & 3 & 58 \\ - & 4 & 12 \\ - & 6 & 18 \\ - & 6 & 18 \\ - & 4 & 12 \\ - & 2 & 05 \end{array} $	- 36 41 - 38 33 - 41 46 - 41 35 - 41 03 - 39 11	— 38 21	
28 р.м.	-6947		R. R.	-5647			$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} -39 & 11 \\ -37 & 40 \\ -33 & 19 \end{bmatrix}$		

^{*} The inclination is computed from the observed declination at West -152° 46', and at E. by S. -49° 06'; with the approximate inclination which these give we have ψ' at East -48° 06'; $\psi = -\frac{152^{\circ}}{2} \frac{46' + 48^{\circ}}{2} \frac{06'}{2} = -100^{\circ}$ 26'; δ at East and West 52° 20'; and $\theta = -\frac{\sin 52^{\circ}}{0267} = -88^{\circ}$ 04'.

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
	Lat.	Long.	Init	observed.	ship's head.		attraction.	Declination.	tion.	Ren
Mar. 1 л.м. 1 р.м.	-68 51 -68 56 -68 56 -68 55 -68 55 -68 55 -68 55	167 49 167 49 167 46 167 46 167 49 167 49 167 46	S. R. O. S. W. S. T. R. T. R.	-33 25 -33 40 -35 23 -36 27 -31 54 -30 30 -32 46 -30 24	N.W. N.W.byW. $\frac{1}{2}$ W. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. by E. S.S.E. S. $\frac{1}{2}$ E. S. by E. $\frac{1}{2}$ E.	-85 10	+12 31 +15 45 0 00 -1 52 -1 52 -1 52 -3 45 -7 22 -1 52 -5 33	-34 50 -33 08 -33 25 -35 32 -37 15 -37 19 -35 39 -37 52 -34 38 -35 57	-36 12	
2 p.m. 3 A.m. 3 p.m.	$\begin{array}{c cccc} -68 & 12 \\ -68 & 12 \\ -68 & 12 \\ -68 & 09 \\ -67 & 40 \end{array}$	167 41 167 56 167 53 167 53 167 45 167 40 166 34	R. R. T. W. T. R. T. R. S.	-30 30 -56 02 -49 58 -50 32 -48 26 -46 36 -45 44 -48 33 -47 00 -46 12	s.e. by s. $w.\frac{1}{2}$ s. w. by N. $w.\frac{1}{4}$ s. $w.\frac{1}{4}$ N. $w.\frac{1}{2}$ N. $w.\frac{1}{2}$ N. $w.\frac{1}{2}$ s. $w.$ by s. $\frac{1}{2}$ s. $w.$ by s. $\frac{1}{2}$ s.	$-84 \ 20$ $-84 \ 15$	-10 40 +18 19 +15 07 +15 38 +15 30 +15 30 +15 22 +15 20 +14 52 +15 15	$ \begin{vmatrix} -41 & 10 \\ -37 & 43 \\ -34 & 51 \\ -34 & 54 \\ -32 & 56 \\ -31 & 06 \\ -30 & 22 \\ -33 & 13 \\ -32 & 08 \\ -30 & 57 \end{vmatrix} $	-32 35	
5 P.M. 6 A.M.	$ \begin{array}{rrrr} -65 & 30 \\ -65 & 40 \\ -65 & 42 \\ -65 & 42 \end{array} $	167 34 165 06 164 56 164 56 164 56	Я. Т. Т. Sм. О. Т.	$\begin{array}{r rrrr} -32 & 28 \\ -36 & 36 \\ -35 & 04 \\ -32 & 27 \\ -30 & 51 \\ -33 & 09 \end{array}$	S.W. $\frac{1}{2}$ S. S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W. S. by W. S. by W. $\frac{1}{2}$ W.		$egin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccc} -23 & 05 \\ -29 & 36 \\ -29 & 19 \\ -25 & 27 \\ -27 & 54 \\ -28 & 48 \end{array} $	• .	-
	$\begin{array}{rrrr} -65 & 44 \\ -65 & 44 \\ -65 & 44 \\ -65 & 50 \\ -65 & 50 \end{array}$	165 05 165 05 165 05 165 05 164 41 164 42	Y. S. W. S. R. R.	$ \begin{vmatrix} -38 & 41 \\ -33 & 03 \\ -37 & 39 \\ -37 & 02 \\ -35 & 55 \\ -38 & 38 \end{vmatrix} $	s. by w. $\frac{1}{2}$ w. s.w. $\frac{1}{2}$ s. s.s.w. $\frac{1}{2}$ w. s.w. by s. s.w. by s. s.s.w. s.w. by s.	-83 45	+ 4 21 + 9 23 + 7 00 + 8 17 + 8 17 + 5 45 + 8 17	$ \begin{array}{c cccc} -30 & 56 \\ -29 & 18 \\ -26 & 03 \\ -29 & 22 \\ -28 & 45 \\ -30 & 10 \\ -30 & 21 \end{array} $	-28 23	
7 A.M. 8 P.M.	$\begin{array}{rrrr} -65 & 25 \\ -65 & 25 \\ -65 & 25 \\ -65 & 25 \\ -64 & 37 \\ -64 & 37 \end{array}$	162 06 162 06 162 06 163 07 163 07	Y. T. O. W. T. S. R.	-15 13	$ \begin{array}{c c} N.W. \frac{1}{2} N. \\ N. \frac{3}{4} W. \\ N. by W. \\ N.N.W. \frac{1}{2} W. \\ N.N.W. \\ E. by N. \frac{1}{2} N. \\ E. by N. \frac{1}{2} N. \\ \end{array} $	-83 50 $-83 00$	$ \begin{array}{r} + 8 & 38 \\ + 1 & 12 \\ + 2 & 32 \\ + 6 & 22 \\ + 5 & 09 \\ -11 & 42 \\ -11 & 42 \\ \end{array} $	$ \begin{array}{ccccc} -23 & 34 \\ -25 & 57 \\ -28 & 20 \\ -24 & 15 \\ -25 & 41 \\ -26 & 38 \\ -26 & 55 \\ -27 & 07 \end{array} $	-25 54	
9 P.M. 10 P.M. 11 A.M.	$\begin{array}{r} -64 & 17 \\ -64 & 16 \\ -64 & 16 \\ -64 & 16 \\ -64 & 16 \end{array}$	163 31 163 17 163 18 163 18 163 18 163 18	R. S. T. T. Y. W. SM. T	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. $\frac{3}{4}$ w. N.w. N.w. $\frac{1}{2}$ w. N.w. by w. N.w. by w. w.n.w.	-83 00 <	$ \begin{array}{r} + 7 & 39 \\ + 2 & 00 \\ + 8 & 26 \\ + 9 & 12 \\ + 9 & 59 \\ + 11 & 17 \\ + 11 & 17 \end{array} $	-27 07 -24 40 -24 25 -25 23 -27 51 -25 17 -25 29 -24 53	-25 18	
11 p.m. 12 a.m.	$ \begin{array}{rrrr} -64 & 02 \\ -64 & 04 \\ -64 & 04 \\ -64 & 03 \\ -63 & 57 \end{array} $	163 06 163 02 163 49 162 45 161 11	T. S. O. T. S. W. T.	-28 07	w.n.w. s.w. by s. s.s.w. ½ w. s.w. by s. s.w. by w. s.w. by w. s.w.by w. s. by w.	-00 00	+739 $+625$ $+739$ $+1053$ $+1125$ $+242$	$ \begin{array}{c cccc} -24 & 59 \\ -25 & 39 \\ -25 & 54 \\ -25 & 29 \\ -22 & 58 \\ -25 & 25 \end{array} $	— #3 18	
12 г.м.	_	161 15 161 16	S. T.	$\begin{vmatrix} -34 & 04 \\ -35 & 27 \end{vmatrix}$	s.w. by s.	−83 00 ₹	$\begin{array}{c cccc} + & 7 & 39 \\ + & 11 & 17 \end{array}$	$ \begin{array}{c c} -26 & 25 \\ -24 & 10 \end{array} $	-24 06	

1841.	Posi	tion.	als.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
1041.	Lat.	Long.	Initials.	observed.	ship's head.	incination.	attraction.	Declination.	tion.	Rem
Mar. 12 p.m.	$ \begin{array}{rrr} -64 & 07 \\ -64 & 07 \\ -64 & 07 \\ -64 & 06 \end{array} $		W. R. T. T. R.	-35 19 -36 25 -36 17 -35 30 -35 11 -35 02	w.N.w. w. by N. ½ N. w. ½ N. w. ½ S. w. by s. w. by s.	-83° 00́<	$\begin{array}{c cccc} & & & & 1\\ & + & 1 & 17 \\ & + & 11 & 42 \\ & + & 12 & 20 \\ & + & 12 & 30 \\ & + & 12 & 30 \\ & + & 12 & 30 \end{array}$	$ \begin{array}{c cccc} -24 & 02 \\ -24 & 43 \\ -23 & 57 \\ -23 & 00 \\ -22 & 41 \\ -22 & 32 \end{array} $	-24 ó6	
14 P.M. 17 A.M.	$\begin{array}{rrrr} -62 & 48 \\ -62 & 48 \\ -62 & 48 \\ -62 & 50 \\ -62 & 50 \\ -62 & 50 \end{array}$	157 14 157 14 157 14 157 14 157 14 157 14 157 02 153 40	R. O. S. R. Y. W. T. W.	$ \begin{vmatrix} -18 & 31 \\ -21 & 04 \\ -21 & 31 \end{vmatrix} $	s.e. by s. s.s.e. s. by e. ½ e. s.e. by e. s.s.e. s. by e. s.s.e. s. by e. s.w. by s. s.w. by s.	$-82 \ 33$ $\left\{ -84 \ 00 \right\}$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-25 38 -25 57 -26 24 -22 43 -22 35 -28 16 -25 01 -19 56 -20 36	-24 07	
18 а.м.	$\begin{array}{rrrr} -63 & 54 \\ -63 & 54 \\ -63 & 54 \\ -63 & 50 \\ -63 & 50 \\ -63 & 50 \end{array}$	151 56 151 52 151 52 151 48 151 48 151 48	SM. S. O. T. SM. S.	$ \begin{vmatrix} -6 & 11 \\ -5 & 25 \\ -7 & 29 \\ -7 & 33 \\ -7 & 15 \\ -8 & 05 \end{vmatrix} $	E.N.E. E. S.E. by E. S.E. by E. S.E. by E.	-84 06	$\begin{array}{c cccc} -13 & 28 \\ -14 & 55 \\ -12 & 48 \\ -12 & 48 \\ -12 & 48 \\ -12 & 48 \end{array}$	$ \begin{vmatrix} -19 & 39 \\ -20 & 20 \\ -20 & 17 \\ -20 & 21 \\ -20 & 03 \\ -20 & 53 \end{vmatrix} $	—20 15	
18 p.m.	$\begin{array}{rrrr} -63 & 50 \\ -63 & 50 \\ -63 & 50 \\ -63 & 50 \\ -63 & 51 \end{array}$	151 48 151 48	O. R. T. S. R. R.	- 8 21 -18 02 -19 05 -17 08 -14 09 -13 20	s.e. by e. ½ e. s. by e. s. by w. s. s.s.s.e. s. by e. ½ e.	-84 00	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{vmatrix} -21 & 37 \\ -21 & 02 \\ -16 & 05 \\ -17 & 08 \\ -20 & 09 \\ -17 & 50 \end{vmatrix} $	—18 59	
19 а.м. 19 р.м.	$ \begin{array}{r rrr} -64 & 16 \\ -64 & 16 \\ -64 & 18 \\ -64 & 24 \end{array} $	149 09 148 27	T. R. W. R. R.	$ \begin{array}{r rrrr} -27 & 16 \\ -27 & 13 \\ -26 & 08 \\ -25 & 43 \\ -26 & 04 \end{array} $	$\left\{\begin{array}{l} \text{s.w. by s.} \\ \text{s.w. by s.} \\ \text{s.w. by s.} \\ \text{s.w. } \frac{1}{2} \text{ s.} \\ \text{s.w. by s.} \end{array}\right\}$	$-84 \ 20 \left\{$	$\begin{vmatrix} + & 9 & 08 \\ + & 9 & 08 \\ + & 9 & 08 \\ + & 10 & 20 \\ + & 9 & 08 \end{vmatrix}$	$ \begin{vmatrix} -18 & 08 \\ -18 & 05 \\ -17 & 00 \\ -15 & 23 \\ -16 & 56 \end{vmatrix} $	-16 41	
20 p.m. 21 a.m.	$ \begin{array}{r rrr} -65 & 03 \\ -64 & 26 \\ -64 & 26 \end{array} $	142 49 142 46 140 46 140 46 140 46	R. R. SM. Y. SM.	$ \begin{vmatrix} -31 & 29 \\ -30 & 34 \\ -24 & 11 \\ -21 & 11 \\ -22 & 47 \end{vmatrix} $	$\begin{cases} w. \\ s.w. by w.\frac{1}{2}w. \end{cases}$ $w.n.w. \\ w.n.w. \\ w.n.w. \end{cases}$	$-85 \ 25 \left\{ \right.$	$\begin{vmatrix} +19 & 26 \\ +17 & 23 \\ +15 & 50 \\ +15 & 50 \\ +15 & 50 \end{vmatrix}$	$egin{bmatrix} -12 & 03 \ -13 & 11 \ -8 & 21 \ -5 & 21 \ -6 & 57 \ \end{bmatrix}$	-12 37	
	$ \begin{array}{r} -64 & 26 \\ -64 & 18 \\ -64 & 01 \\ -63 & 18 \end{array} $	140 46 140 27	O. S. W. S. O.	$ \begin{array}{rrrr} -21 & 18 \\ -19 & 40 \\ -23 & 56 \\ -3 & 46 \\ -1 & 55 \end{array} $	N.w. by w. N.w. by w. W.N.w.	$igg -84 \ 55 \Big<$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{bmatrix} -7 & 18 \\ -5 & 40 \\ -8 & 06 \end{bmatrix} $ $ \begin{bmatrix} -3 & 46 \\ -3 & 18 \end{bmatrix} $	— 6 57	
:	$ \begin{vmatrix} -63 & 18 \\ -63 & 18 \\ -63 & 18 \\ -63 & 20 \\ -63 & 14 \\ -63 & 14 \end{vmatrix} $	3 140 04 3 140 04 3 140 04 0 139 52 4 139 43	T. T.	$ \begin{vmatrix} -6 & 16 \\ -19 & 52 \\ -18 & 31 \\ -20 & 19 \end{vmatrix} $	N. by w. w. by N. ½ N. w.N.w. w.N.w. N.w.byw.½w. w.	_84 0 5	1 0 11	- 3 32 - 5 55 - 5 04 - 6 52 - 7 32 - 7 34 - 7 34	— 5 58	
22 p.m		139 28 139 38 139 38 139 38 139 06 2 139 05 2 137 40	R. R. R. R. R.		N.W. $\frac{3}{4}$ W.	-84 00	$\begin{vmatrix} +13 & 27 \\ +12 & 37 \\ +9 & 04 \\ +14 & 54 \\ +11 & 39 \\ +11 & 14 \\ +14 & 43 \end{vmatrix}$	$ \begin{bmatrix} -3 & 13 \\ -5 & 37 \\ -7 & 07 \end{bmatrix} $ $ \begin{bmatrix} -3 & 38 \\ -3 & 29 \end{bmatrix} $	_ 4 05	

1841.	Posi	tion.	ials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
1041.	Lat.	Long.	Initials.	observed.	ship's head.	incimation.	attraction.	Declination.	tion.	Rem
Mar. 22 p.m.	$ \begin{array}{c cccc} -62 & 32 \\ -62 & 28 \\ -62 & 28 \end{array} $		R. R. R.	-16 55 -18 35 -18 29	w. by $n. \frac{1}{2} n.$ w. by $s. \frac{1}{2} s.$ w. by $n.$	$-8\mathring{4} 0\acute{0}$	$\begin{vmatrix} +13 & 46 \\ +14 & 17 \\ +14 & 15 \end{vmatrix}$	$\begin{vmatrix} -3 & 09 \\ -4 & 18 \\ -4 & 14 \end{vmatrix}$	- °4 0′5	
23 A.M.		136 05 136 25	Sм. Т. W.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. $\frac{1}{2}$ W. N.W. by W. N.W. by W.		$ \begin{array}{r} +10 & 18 \\ +11 & 08 \\ +11 & 08 \end{array} $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		
	-62 20 -62 17 -62 16	136 27 136 29	R. R. R.	$ \begin{vmatrix} -11 & 53 \\ -11 & 41 \\ - 9 & 59 \end{vmatrix} $	N.w. by w. N.w. by w. N.w. by w.	−83 45	$\begin{vmatrix} +11 & 08 \\ +11 & 08 \\ +11 & 08 \end{vmatrix}$	$ \begin{vmatrix} -0 & 45 \\ -0 & 33 \\ +1 & 09 \end{vmatrix} $	_ 1 12	
23 p.m.	-62 07	136 08 136 08	R. R. R.	-14 02	N.w. by w. $\begin{bmatrix} N.w. \text{by w.} \\ N.w. \text{byw.} \frac{1}{2} \text{w.} \\ w. \frac{1}{4} \text{ s.} \end{bmatrix}$		+11 08 $+11 27$ $+13 32$	$ \begin{array}{c cccc} & - & 0 & 11 \\ & + & 0 & 22 \\ & - & 0 & 30 \\ & & & & & & \\ \end{array} $		
	$ \begin{array}{rrr} -62 & 06 \\ -62 & 06 \\ -62 & 06 \\ -62 & 06 \end{array} $	136 07 136 07	R. O. S. T.	$ \begin{array}{r rrr} -11 & 00 \\ -14 & 49 \\ -10 & 59 \\ -12 & 41 \end{array} $	s.w. by w. w. by n. n.w. by w. n.w.byw.½w.	$-83 \ 30 < $	$\begin{vmatrix} +11 & 39 \\ +13 & 07 \\ +10 & 42 \\ +11 & 27 \end{vmatrix}$	$ \begin{vmatrix} + & 0 & 39 \\ - & 1 & 42 \\ - & 0 & 17 \\ - & 1 & 14 \end{vmatrix} $	- 0 27	
25 A.M.		131 47 131 47	S. O. Y.	$\begin{vmatrix} + & 0 & 15 \\ + & 1 & 13 \\ + & 0 & 16 \end{vmatrix}$	N.W.) N.W.) N.W.)		$\begin{vmatrix} + & 1 & 2 \\ + & 8 & 40 \\ + & 8 & 40 \\ + & 8 & 40 \end{vmatrix}$	$\begin{vmatrix} + & 8 & 55 \\ + & 9 & 53 \\ + & 8 & 56 \end{vmatrix}$		8
	$ \begin{array}{r} -60 & 30 \\ -60 & 30 \\ -60 & 23 \end{array} $	131 47 131 47 131 28	W. T. R.	$\begin{vmatrix} + & 0 & 50 \\ - & 0 & 35 \\ - & 1 & 51 \end{vmatrix}$	$ \begin{array}{c c} N.W. \\ N.W. \\ 1 & W. \end{array} $	-83 10	$\begin{vmatrix} + & 8 & 40 \\ + & 8 & 40 \\ + & 9 & 24 \end{vmatrix}$	$\begin{vmatrix} + & 9 & 31 \\ + & 8 & 05 \\ + & 7 & 33 \end{vmatrix}$	+ 8 09	
	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	131 28 131 28 131 28 131 27	R. T. W. R.		w. n.w.		$\begin{vmatrix} +12 & 53 \\ + & 8 & 40 \\ + & 8 & 40 \end{vmatrix}$	$\begin{vmatrix} + & 7 & 02 \\ + & 5 & 30 \\ + & 6 & 49 \\ + & 9 & 13 \end{vmatrix}$,
25 p.m.		131 22 131 22	R. T. T.	$\begin{vmatrix} + & 0 & 33 \\ + & 1 & 00 \\ + & 18 & 20 \\ + & 18 & 12 \end{vmatrix}$	N.W. by N. E.N.E. E. ½ S.		$\begin{vmatrix} + & 8 & 40 \\ + & 6 & 44 \\ -11 & 17 \\ -12 & 31 \end{vmatrix}$	$\begin{vmatrix} + & 9 & 13 \\ + & 7 & 44 \\ + & 7 & 03 \\ + & 5 & 41 \end{vmatrix}$		
	-60 20 $-60 20$	131 22	R. R. Sм.	$\begin{vmatrix} +14 & 06 \\ +18 & 59 \end{vmatrix}$	$N.E. \text{ by N.}$ $N.E. \text{ by E.} \frac{3}{4}E.$ $E.N.E.$	−83 00 ₹	$ \begin{vmatrix} -6 & 44 \\ -10 & 57 \\ -11 & 17 \end{vmatrix} $	$\left \begin{array}{ccc} + & 7 & 22 \\ + & 8 & 02 \\ + & 7 & 44 \end{array} \right $	+ 7 38	
	$\begin{bmatrix} -60 & 20 \\ -60 & 20 \end{bmatrix}$)	R. Sм. Т.	$\begin{vmatrix} +22 & 22 \\ +17 & 35 \\ +18 & 36 \end{vmatrix}$	E. N.E. by E. E.N.E.		$ \begin{array}{r rrrr} -12 & 33 \\ -9 & 59 \\ -11 & 17 \end{array} $	$\begin{vmatrix} + & 9 & 49 \\ + & 7 & 36 \\ + & 7 & 19 \end{vmatrix}$		1
		I.	S. W. R. R.	$\begin{vmatrix} +18 & 17 \\ +20 & 05 \\ +18 & 49 \\ +16 & 36 \end{vmatrix}$	N.E. by E. E. $\frac{1}{2}$ N. N.E. by E. $\frac{1}{2}$ E. N.E.	-83 00	$ \begin{vmatrix} -9 & 59 \\ -12 & 20 \\ -10 & 37 \\ -8 & 26 \end{vmatrix} $	$\left \begin{array}{c} + & 8 & 18 \\ + & 7 & 45 \\ + & 8 & 12 \\ + & 8 & 10 \end{array} \right $	+ 8 18	
26 a.m	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1	R. R. R.	$\begin{vmatrix} + & 3 & 47 \\ + & 8 & 33 \\ + & 3 & 21 \end{vmatrix}$	n.w. by n. N.w. by n. N.w. by n.	}	$\begin{vmatrix} - & 6 & 20 \\ + & 6 & 44 \\ & 0 & 00 \\ + & 6 & 12 \end{vmatrix}$	$ \begin{vmatrix} + & 3 & 10 \\ + & 10 & 31 \\ + & 8 & 33 \\ + & 9 & 33 \end{vmatrix} $		
	-59 13 -59 13 -59 13	3 130 02 3 130 02 1 130 00	R. S. R.	$\begin{vmatrix} + & 7 & 01 \\ + & 4 & 42 \\ + & 1 & 49 \end{vmatrix}$	N. N.N.W. N.N.W.	 _82 36≺	$\begin{vmatrix} 0 & 00 \\ + & 4 & 10 \\ + & 4 & 10 \\ + & 4 & 10 \end{vmatrix}$	$\begin{vmatrix} + & 7 & 01 \\ + & 8 & 52 \\ + & 5 & 59 \end{vmatrix}$		
	$\begin{bmatrix} -59 & 10 \\ -59 & 10 \end{bmatrix}$	129 56 129 56 129 56			N.N.W. N.N.W.		$\begin{vmatrix} + & 4 & 10 \\ + & 4 & 10 \end{vmatrix}$	$\left \begin{array}{c} + 6 & 42 \\ + 5 & 58 \\ + 6 & 58 \end{array} \right $	+ 8 32	
27 A.M	-58 0 $-58 0$	3 129 40 8 128 46 8 128 46 6 128 43	S.	$\begin{vmatrix} + & 4 & 59 \\ + & 8 & 55 \\ + & 5 & 44 \\ + & 6 & 53 \end{vmatrix}$	N.N.W. N.N.W. N.N.W.	-82 00 3	$ \begin{array}{r} + 4 10 \\ + 3 54 \\ + 3 54 \\ + 3 54 \end{array} $	$\begin{vmatrix} + 9 & 09 \\ +12 & 49 \\ + 9 & 38 \\ +10 & 47 \end{vmatrix}$		
28 а.м	57 2	127 50 4 127 50 4 127 50	W.		$ \begin{array}{c c} N.N.W. \\ W. \frac{1}{2} S. \\ W. \frac{1}{2} S. \end{array} $	$-81 \ 45$	$\begin{vmatrix} + & 3 & 34 \\ +10 & 41 \\ +10 & 41 \end{vmatrix}$	$\begin{vmatrix} +10 & 47 \\ +8 & 20 \\ +10 & 46 \end{vmatrix}$	+ 8 47	

1841.	Posi	tion.	Initials.	Declination	Direction of	Inclination.	Correction for ship's	Corrected	Mean Declina-	Remarks.
	Lat.	Long.	Init	observed.	ship's head.		attraction.	Declination.	tion.	Rem
Mar. 28 A.M.	-57 19 -57 19 -57 20 -57 20	127 49 127 47 127 47	R. T. R. W.	- °1 35 - 2 16 - 2 56 - 1 20	w. by s. $w \cdot \frac{1}{2} s \cdot w \cdot \frac{1}{2} N \cdot$	+81 45	$+10 \ 40 \ +10 \ 41 \ +10 \ 41 \ +10 \ 29$	$\begin{pmatrix} + & 9 & 05 \\ + & 8 & 25 \\ + & 7 & 45 \\ + & 9 & 09 \end{pmatrix}$	+ °8 47	
29 p.m.	-56 21 -56 21 -56 16 -56 14 -56 05		T. R. S. R. S. R. R. T.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by s. \frac{1}{4} s. w. \frac{1}{2} N. w. \frac{1}{2} N. w. N.E. N.E. N.E. N.E. N.E.	-81 00	+10 48 +10 29 +10 29 +10 41 - 6 27 - 6 27 - 6 27 - 6 27 - 6 27 - 6 27	+ 7 43 + 8 24 + 6 55 +11 20 + 3 13 + 6 45 + 2 37 + 6 37 + 5 00 + 7 40	+ 5 46	motion; observations uncertain two or three degrees.
30 а.м.	$\begin{array}{rrrr} -55 & 00 \\ -55 & 00 \\ -55 & 00 \\ -55 & 16 \\ -55 & 16 \\ -55 & 14 \end{array}$	131 43 131 43 131 43 131 09 131 09 131 12	W. R. SM. T. SM. S. R. R. R. T.	+1350 $+1138$ $+857$ $+627$ $+543$ $+627$ $+805$ $+1155$ $+855$	N.E. by N. N.E. \frac{1}{2} E. N.E. by N. N.E. by E. N.E. by E. N.E. by E. N.E. \frac{1}{2} E.	-80 20	- 5 01 - 6 27 - 6 33 - 4 38 - 7 06 - 7 06 - 8 59 - 6 33	+ 8 49 + 5 11 + 2 24 + 1 49 + 1 05 - 0 39 + 0 59 + 2 56 + 2 22	+ 1 34	Very much mo to two
30 p.m.	$\begin{array}{rrrrr} -55 & 14 \\ -55 & 14 \\ -55 & 14 \\ -55 & 14 \\ -55 & 14 \\ -55 & 11 \\ -55 & 05 \end{array}$	131 12 131 12 131 12 131 18 131 18 131 15 131 15 132 48	S. O. Y. W. R. T. W.	+ 6 27 + 4 16 + 4 28 + 6 00 + 5 28 + 6 33 + 6 04 + 3 18	N.E. $\frac{1}{2}$ N. N.E. by N. N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ E. N.E. by N. N.E. by N. N.E. by N. N.E. by N.	-80 20	- 5 17 - 4 38 - 5 17 - 6 33 - 4 38 - 4 38 - 4 38 - 5 05	$ \begin{vmatrix} + & 1 & 10 \\ - & 0 & 22 \\ - & 0 & 49 \\ - & 0 & 33 \\ + & 0 & 50 \\ + & 1 & 55 \\ + & 1 & 26 \\ - & 1 & 47 \end{vmatrix} $	+ 0 31	
	$-55 05 \\ -55 05$	132 48 132 48 132 48 132 37 132 40 132 40 132 42	T. S. T. R. R. Y. R. T.	$\begin{array}{c} + 4 & 16 \\ - 2 & 50 \\ + 7 & 07 \\ + 8 & 14 \\ + 5 & 57 \\ + 8 & 43 \\ + 4 & 56 \\ + 4 & 55 \end{array}$	N.N.E. N. N.E. by N.	−80 00 ₹	- 3 00 0 00 - 4 27 - 4 27 - 4 27 - 4 27 - 4 27 - 4 27	+ 1 16 - 2 50 + 2 40 + 3 47 + 1 30 + 4 16 + 0 29	+ 1 05	
31 A.M.	$\begin{array}{rrrr} -54 & 07 \\ -54 & 07 \\ -54 & 07 \\ -54 & 01 \\ -54 & 01 \\ -54 & 01 \end{array}$	134 31 134 21 134 21 134 35 134 35	S. T. O. T. S. S. O.	+ 4 23 + 5 06 + 5 52 + 5 57 + 6 33	N.E. by N. E.N.E. N.E. by E. E. by N. E. \frac{1}{2} S. E. by N. \frac{1}{2} N.	-79 30 	- 4 27 - 6 29 - 7 26 - 6 29 - 7 57 - 8 16 - 7 38 - 7 26	+ 0 28 - 2 06 - 2 14 - 0 37 - 2 00 - 1 43 - 2 23 - 3 53	— 1 50	
	-54 04 -54 05 -54 04 -54 04	134 40 134 40 134 43 134 47 134 54	W. W. R. R. R. R. R.	$\left(\begin{array}{ccc} + & 6 & 32 \\ + & 5 & 26 \\ + & 6 & 25 \end{array} \right)$	E.N.E. E. by N. E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	-79 30 3 0	- 7 26 - 7 57 - 7 38 - 7 38 - 8 06 - 8 06	$ \begin{array}{c cccc} & -0 & 48 \\ & -2 & 31 \\ & -1 & 13 \\ & -1 & 08 \\ & -1 & 31 \\ & -1 & 02 \end{array} $	— 1 44	
April 1 р.м.		135 23	R. R.	$\begin{array}{ccccc} + & 0 & 52 \\ + & 1 & 49 \end{array}$	N.N.E.	$-78\ 50$	$ \begin{array}{c cccc} & 2 & 42 \\ & 2 & 42 \end{array} $	$-150 \\ -053$	— 1 03	

1841.	Posi Lat.	tion. Long.	Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declina- tion.	Remarks.
2 p.m. 5 p.m. 6 a.m.	-52 55 -52 51 -52 49 -52 46 -51 12 -51 12 -51 06 -51 06 -51 06 -44 52 -44 52 -44 51 -44 09 -44 09 -44 06	135 24 135 26 135 29 135 29 135 29 136 50 136 55 136 55 136 59 143 30 143 28 143 34 145 33 145 35 145 42 145 43 145 53	S. T. T. R. R. T. R. S. T. R. R. R. T. R. R. R. T. R. R. R. T. R. R. R. T. T. R. R. R. T. T. T. R.	+ 1 34 + 0 30 + 3 13 + 2 24 + 1 10 - 1 37 - 1 00 - 5 26 - 7 08 - 0 49 - 0 06 - 1 11 - 5 41 - 6 33 - 5 35 - 7 01 - 7 09 - 6 50 - 5 58	N.N.E. N.N.E. N.N.E. N.N.E. N.E. by N. N.N.E. N.E. by E. N.E. by E.	-78 50 $-77 40$ $-73 20$ $-71 40$	- 2 42 - 2 42 - 2 42 - 2 42 - 3 30 - 2 8 0 00 + 1 12 - 2 28 - 3 51 - 3 51 - 3 17 - 4 38 - 3 42 - 3 26 - 3 26 - 3 36 -	- 1 08	- i oís - 4 39 - 8 46	1

Observations of the Inclination in H.M.S. Erebus, from September 1840 to April 1841, made with Needle R. F. 4.

Observers Captain Ross and Lieutenant Smith, R.N.

1840.	Position.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attrac-	Mean Inclination. Face east.	True Inclination.	Remarks.
	Lat. Long.					tion.			
	Mågnetic Öbserva- tory, Van Diemen	h m		0 /		,	o /	0 /	
Sept. 17.	Island42 52 147 24	2 Р.М.	Direct. S. at 20°. N. at 20°.	$ \begin{array}{rrrr} -71 & 06.8 \\ -71 & 13.4 \\ -71 & 12.1 \end{array} $					
19. 28.		11 A.M. 2 P.M.	S. Direct. Direct.		Observed)				
29.		3 P.M. 1 P.M.	Direct. Direct.	$ \begin{array}{r rrr} -70 & 58.4 \\ -71 & 05.2 \end{array} $	on shore.		-71 06	-70 38	
		3 P.M.	S. at 20°. S. at 20°. N. at 20°. Direct.	$ \begin{array}{rrrr} -71 & 09.9 \\ -71 & 07.2 \\ -70 & 58.5 \\ -71 & 02.6 \end{array} $:		
Oct. 17.	At anchor.	1 30 P.M.	Direct. S.	$ \begin{array}{r rrrr} -70 & 39.1 \\ -70 & 42.8 \end{array} $	s.e. by s.	-43	-71 24		
		2 P.M.	Direct. S. Direct.	$ \begin{array}{r rrrr} -71 & 46.7 \\ -71 & 48.5 \\ -70 & 29.9 \end{array} $	} w.	+24	-71 24		
		Z P.M.	S. Direct.		s. by E. s.s.e.	-61 -53	$\begin{vmatrix} -71 & 33 \\ -71 & 33 \end{vmatrix}$		
21.		2 30 р.м.	S. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.e.	-32	-71 35 -71 27		
		1 45 р.м.	Direct. Direct.	$ \begin{array}{r rrrr} -72 & 06.7 \\ -72 & 12.6 \end{array} $	} w.n.w.	+46	-71 24		
29.		6 а.м.	Direct. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$) N.	+74	-71 06		
			S. Direct.	-72 07.8 $-72 10.3$	N.N.E.	$ +70 \\ +64$	-71 00 $-70 58$,	
			S. Direct. S.	$ \begin{array}{r rrrr} -71 & 54.8 \\ -72 & 01.6 \\ -71 & 59.6 \end{array} $	E.N.E.	+46	_70 38 _71 15		
			Direct. S.		} E.	+24	-71 02		
			Direct. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	} N.N.W.	+71	-71 12		
			S. Direct.		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	+64 - 3	-71 27 $-71 26$	$\left \begin{array}{c} -70 & 45 \end{array} \right $	
			S. Direct. S.	$ \begin{array}{r rrrr} -71 & 24.5 \\ -71 & 38.0 \\ -71 & 44.7 \end{array} $	} w.	+24	-71 17		
			Direct. S.		} w.n.w.	+46	-71 00		
			Direct. S. Direct.	$ \begin{vmatrix} -70 & 52.0 \\ -70 & 43.7 \\ -70 & 38.5 \end{vmatrix} $	s.w.	-32	-71 20		
			S. Direct.	$\begin{bmatrix} -70 & 32.3 \\ -70 & 16.9 \end{bmatrix}$	s.s.w.	-52 -61	$\begin{vmatrix} -71 & 27 \\ -71 & 18 \end{vmatrix}$		
			S. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.e.	-53	-71 09		

1840.	Position.	Time of	Method	Observed Inclination.	Ship's head.	Correction for ship's	Mean In- clination.	True	Remarks
	Lat. Long.	day.	employed.	Face east.	omp s nead.	attrac- tion.	Face east.	Inclination.	Remarks
Oct. 29.	At anchor.	h m 6 A.M.	Direct. S. Direct. S.	$ \begin{vmatrix} -\mathring{7}0 & 46.5 \\ -70 & 44.6 \\ -71 & 12.8 \\ -71 & 12.8 \end{vmatrix} $	S.E. E.S.E.	-31 - 3	-71 17 -71 16	-70 45	
Nov. 13.	-44 16 149 29	1 15 p.m. to 2 15 p.m.	Direct. S. N.	$ \begin{vmatrix} -71 & 03.1 \\ -71 & 05.8 \\ -71 & 10.6 \end{vmatrix} $	E.S.E.	- 3	—71 09	-70 41	
14.	—45 13 151 57	10 40 A.M. to 11 25 A.M.	Direct. S. N.	$ \begin{array}{c cccc} -71 & 42.7 \\ -71 & 47.0 \\ -71 & 43.5 \end{array} $	s.e.	-33	-72 17	-71 49	
15.	—45 33 152 45	11 20 A.M. to Noon.	Direct. S. N.	$ \begin{vmatrix} -72 & 26.0 \\ -72 & 18.3 \\ -72 & 39.0 \end{vmatrix} $	} E.	+23	-72 05	-71 37	
16.	—46 18 154 30	1 30 P.M. to 2 20 P.M.	Direct. S. N.	$\begin{vmatrix} -72 & 22.5 \\ -72 & 21.2 \\ -72 & 37.1 \end{vmatrix}$	E.S.E.	– 5	-72 32	-72 04	
17.	—47 46 157 40	10 45 A.M. to 11 45 A.M.	Direct. S. N.	$\begin{bmatrix} -73 & 20.2 \\ -73 & 24.7 \\ -73 & 37.7 \end{bmatrix}$	s.e. by e. $\frac{1}{2}$ e.	-14	73 42	-73 14	
18.	-49 20 160 13	to Noon.	Direct. S. N.	-74 22·7 -74 41·0 -74 21·8	s.e. by e. $\frac{1}{2}$ e.	-15	-74 43	-74 15	
19.	-50 28 164 9	11 20 A.M. to Noon.	Direct. S. N.	-75 16·8 -75 12·5 -75 11·0	} E.	+22	-74 51	-74 23	
	Auckland Island50 33 166 19	1 15 p.m. to 4 p.m.	Direct. S. N. Direct.	-74 25·5 -74 19·5 -75 02·5	J	+47	-73 49	-73 21 -73 21	
24.		11 30 A.M. to 0 30 P.M.	Direct. S. N.	$ \begin{array}{rrrrr} -74 & 33.6 \\ -75 & 05.1 \\ -75 & 03.6 \\ -74 & 49.6 \end{array} $	N.w.by w. (Record omitted.)	+59	—73 35	—73 07	ose poles
-	At the Magnetic Observatory.	2 00 P.M. to 5 30 P.M.	Direct. S. N.	-73 40·8 -73 39·8 -73 43·3	Observed on shore.		73 41·3	−73 13·3	Mean of needles whose poles were inverted -73° 10'.
26.	Pig Island50 32 166 12	9 00 A.M. to 10 00 A.M.	Direct. S. N. Direct.	-73 38·4 -73 33·3 -73 34·4 -73 39·1	Observed on shore.		−73 36·3	-73 08·3	
	Shoe Island. { 200 yards west	1 30 p.m. to 2 30 p.m.	Direct. S. N.	-77 27·5 -77 33·1 -77 31·3	Observed on shore.	• • • • •	-77 31	-77 03	Excessive local attraction.
	of the preceding station.		Direct.	-74 10.6	$\left\{ \begin{array}{l} \text{Observed} \\ \text{on shore.} \end{array} \right\}$		-74 11	-73 43	EX

1840.	Posi	tion.	Time of day.	Method	Observed Inclination.	Ship's head.	Correc- tion for ship's	Mean In- clination.	True Inclination.	Remarks
	Lat.	Long.	•	employed.	Face east.		attrac- tion.	Face east.		
Nov. 26.	o 'At an	$\stackrel{\circ}{\operatorname{chor.}}'$	h m 6 00 to 6 40 p.m.	Direct.	$\begin{bmatrix} -\mathring{7}2 & 42.8 \\ -72 & 48.0 \end{bmatrix}$	} s.s.w.		。 , 73 43	-73 15	
		ι	6 45 P.M.	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	} w.s.w.	- 6	-73 43	-73 15	
30.		d Island, { Point. {	7 45 A.M.	Direct. S.	$\begin{bmatrix} -73 & 29 \cdot 1 \\ -73 & 26 \cdot 0 \end{bmatrix}$			-73 28	-73 00	
	Sandy	· · · · · · · · · · · · · · · · · · ·	2 00 р.м.	Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Observed on shore.		-73 54	-73 26	
	155 yard the pr station	$\operatorname{eceding} \langle$	2 30 р.м.	Direct. S. N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$			-73 54	—73 26	And the second second
Dec. 2.	Aucklan	d Island.	1 20 p.m. to 2 30 p.m.	Direct. S. N.	-65 39·5 -65 28·0 -65 13·0	Observed on shore.		-65 30	-65 02	Excessive local attraction.
6.	At a	nchor.	7 15 A.M.	Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	} s.w.	_37		-73 13	Exce
	in chandren en exp.		8 30 л.м.	S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. s.s.w.	59	-73 44	-73 16 -73 16	
7.			11 00 а.м.	S. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by s.	+ 8	-74 05	-73 37	
8	The state of the s		9 00 а.м.	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.	-67	-73 35	-73 07	
				Direct. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	} s.s.e.	-59	-73 32	-73 04	
				Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e.	-37	-73 43	-73 15	
				Direct. S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E.	- 7	-73 37	-73 09	
				S. Direct.	-73 49.8 $-74 10.6$	} E.	+22	-73 32	-73 04 72 57	
				S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E.	$\begin{vmatrix} +47 \\ +66 \end{vmatrix}$	$\begin{vmatrix} -73 & 25 \\ -73 & 35 \end{vmatrix}$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
				S. Direct.	$\begin{vmatrix} -74 & 42.5 \\ -74 & 33.2 \end{vmatrix}$	N.N.E.	+76	-73 21	-72 53	
				S. Direct. S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	\\ N.	+79	-73 33	-73 05	
	den regeration de la constanta			Direct. S.	-75 01.5 $-75 02.3$	N.N.W.	+76	-73 46	-73 18	
				Direct.	-74 48·5 -74 39·2	N.W.	+66	$\begin{vmatrix} -73 & 38 \\ -73 & 48 \end{vmatrix}$	-73 10	
12				Direct.	$\begin{bmatrix} -73 & 10.7 \\ -73 & 55.8 \end{bmatrix}$		$\begin{vmatrix} -37 \\ +36 \end{vmatrix}$	$\begin{bmatrix} -73 & 48 \\ -73 & 20 \end{bmatrix}$	$\begin{array}{ c c c c c c } -73 & 20 \\ -72 & 52 \end{array}$	
12	•			Direct. Direct.	$-73 37.4 \\ -74 30.0$	E. N.E.	$+22 \\ +66$	$-73 15 \\ -73 24$	$-72 47 \\ -72 56$	
				Direct. Direct. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.N.E.	+ 59 + 47 + 7	$ \begin{vmatrix} -73 & 10 \\ -73 & 18 \\ -73 & 17 \end{vmatrix} $	$ \begin{array}{c cccc} -72 & 42 \\ -72 & 50 \\ -72 & 49 \end{array} $	
				Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.S.E.	$\begin{bmatrix} -7 \\ -22 \end{bmatrix}$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	

1840.	Pos	ition.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attrac-	Mean In- clination. Face east.	True Inclination.	Remarks.
	Lat.	Long.			2 400 0450		tion.	Tuco cast.		
Dec.14.	Campbel — 52 34	l Island. 169 10 nchor.	h m 10 00 A.M. 11 00 A.M.	Direct. S. Direct.	-75 42.8 -75 48.3 -74 53.7	} N.W.	+67	° ' -74 38	-74 10	
-	nt a	nenor.	1 00 г.м.	S. Direct.	$ \begin{array}{rrrr} -75 & 02.4 \\ -73 & 18.4 \\ -73 & 13.1 \end{array} $	} w. } s.s.w.	$\begin{vmatrix} +22 \\ -60 \end{vmatrix}$	$\begin{vmatrix} -74 & 36 \\ -74 & 16 \end{vmatrix}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
15.	At the M Obser	lagnetic vatory.	2 00 P.M. to 4 15 P.M. 6 15 A.M. to 8 30 A.M.	Direct. S. N. Direct. Direct. S. N. Direct.	-73 44·5 -74 29·7 -74 27·8 -74 30·2 -74 24·5 -74 24·4 -74 18·5 -74 23·1	Observed on shore. Observed on shore.		-74 18 -74 23	-73 50 -73 55	Mean on shore -73 55. Mean on board -73 56.
	At Anch Running Harbo	out of f	1 00 p.m. 9 30 A.M.	Direct. S. Direct. Direct.	-73 18·4 -73 13·1 -73 42·1 -73 16·0	s.s.w. E. by s. s.	-60 + 7 -69		$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
18.	$\begin{bmatrix} -53 & 47 \\ -54 & 25 \end{bmatrix}$		4 30 A.M. 5 00 P.M.	Direct. S. Direct. N.	$\begin{array}{ c c c c c }\hline -74 & 21 \cdot 0 \\ -74 & 33 \cdot 8 \\ -73 & 39 \cdot 9 \\ -74 & 27 \cdot 0\end{array}$	$\left.\begin{array}{c} \text{S.S.E.} \\ \text{S.S.E.} \ \frac{1}{2} \text{ E.} \end{array}\right.$	-61 -57	-75 28 -75 00		Uncertain. Very much motion.
19.	-55 50	170 6	10 15 A.M. to 11 10 A.M.	Direct. N. S.	$ \begin{vmatrix} -75 & 26 \cdot 1 \\ -75 & 40 \cdot 5 \\ -75 & 32 \cdot 5 \end{vmatrix} $	s. by w.	-71	-76 44	-76 16	
21.	-57 15	170 40	4 20 а.м.	Direct. N. N.S.	-77 14·0 -77 01·2 -76 58·0	s.s.e.	-67	-78 11	-77 43	Ship pitching.
	-57 54	170 25	5 10 P.M. to 5 50 P M.	Direct. N. N.S.	-77 15·0 -77 00·5 -77 00·1	s. by E.	-74	-78 19	-77 51	
22.	-58 57	170 57	10 15 A.M. to 11 10 A.M.	s.	-77 24·2 -77 19·0 -77 10·8 -77 05·2	8.	-77	-78 32	-78 04	
23.	_59 41 _59 48		10 15 A.M. to 11 20 A.M. 6 40 P.M.	Direct. S. N. N.S.	-78 05·0 -78 08·5 -78 06·7 -77 59·0 -78 57·8		-69	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\left \right\rangle$ -78 34	
24.	-60 14		5 00 A.M.		$ \begin{vmatrix} -78 & 59.0 \\ -78 & 27.3 \end{vmatrix} $	} E.	+20 {	$\begin{bmatrix} -78 & 38 \\ -78 & 39 \end{bmatrix}$ $\begin{bmatrix} -79 & 19 \end{bmatrix}$		
	60_21	170 30	to 6 00 A.M. 11 00 A.M. to	N. N.S. Direct. S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \text{S.E.} \frac{1}{2} \text{ s.} \\ \\ \text{S.S.E.} \end{array}$	$\begin{vmatrix} -52 \\ -70 \end{vmatrix}$	$ \begin{array}{rrrrr} -79 & 05 \\ -79 & 16 \\ -79 & 15 \\ -79 & 57 \\ -79 & 24 \end{array} $	\\ \>-78 53	
	-60 31	170 32	Nøon.	N. N.S.	$ \begin{vmatrix} -78 & 13.6 \\ -78 & 01.0 \end{vmatrix} $	1 1	-/0			

1840.	Pos	ition.	Time of day.	Method employed.	Observed Inclination.	Ship's head.	Correc- tion for ship's	Mean Inclination.	True Inclination.	Remarks.
	Lat.	Long.			Face east.		attrac- tion.	Face east.		
Dec. 24.	_6°0 46	170 44	h m 5 15 p.m. to 6 10 p.m.	Direct. S. N. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s.	-59	-79 34	-79 0 6	
25.	-61 34	170 40	2 15 A.M. to 3 15 A.M.	Direct. N. N.S.	$ \begin{array}{ c c c c c c } -78 & 43.4 \\ -78 & 40.1 \\ -78 & 32.9 \end{array} $	s.	-79	-79 58	-79 30	
	-62 04 $-62 10$		Noon.	Direct. ? ? Direct.	$ \begin{vmatrix} -81 & 29 \cdot 2 \\ -81 & 25 \cdot 0 \\ -81 & 27 \cdot 2 \\ -79 & 28 \cdot 3 \end{vmatrix} $	N. s.s.w.	$+88$ $\begin{cases} -71 \end{cases}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\left \right\rangle$ -79 41	
	-62 40		10 30 а.м.	Direct.	-80 53·3	$W. \frac{1}{2} N.$		-80 26	-79 58	
28.	$-62 ext{ } 40$ $-62 ext{ } 52$		10 30 A.M. to 11 45 A.M. 3 00 P.M.	Direct. S. N. N.S. Direct. N.S.	-79 26·4 -79 21·4 -79 18·4 -78 32·7 -79 37·2 -79 22·8	s.	-80	-80 37	-80 09	
29.	-64 00	172 44	8 40 A.M. to 10 20 A.M.	Direct. S. N. N.S.	-80 25·0 -80 24·1 -80 28·2 -80 18·8		-67	81 31	—81 03	
	—64 06	172 38	10 30 A.M. to 11 45 A.M.	Direct. S. N. N.S. Direct.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.w. s. by w.	$egin{array}{c} -73 \left\{ -80 \left\{ ight. ight. ight.$	$ \begin{array}{c cccc} -81 & 41 \\ -81 & 30 \\ -81 & 41 \\ -81 & 08 \\ -81 & 37 \end{array} $		
30.	-64 30 -64 31	172 51 173 00	6 45 A.M. 10 45 A.M. to 11 45 A.M.	Direct. N.S. Direct. S. N. N.S.	-80 23·9 -80 16·2 -80 16·3 -80 14·4 -80 17·9 -80 54·3	s.w. by s.	$\begin{vmatrix} -61 \\ -82 \\ \end{vmatrix}$	-81 25 -81 17 -81 38 -81 36 -81 40 -82 16	-81 11	
31.	65 58	171 47	10 45 A.M. to 11 50 A.M.	Direct. S. N. N.S.	-81 23·8 -81 25·6 -81 29·3 -81 18·2	s.	-84	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
	-66 17	170 57	3 45 P.M. to 4 40 P.M.	Direct. S. N. N.S.	-81 25.0 -81 23.9 -81 34.7 -81 49.4		-77	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$-82\ 25$	
1841. Jan. 1.	-66 30	169 13	10 00 A.M.	Direct. S. N. N.S.	-81 36·4 -81 39·0 -81 49·6 -81 49·2	$\left.\right $ s.	-85	-83 08	-82 40	

1841.	Position. Lat. Long.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Incli- nation. Face east.	True Inclination.	Remarks.
Jan. 1.	_66 32 169 45	h m 11 25 A.M. to 0 30 P.M.	Direct. S. N. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	} N.	+91	-82 59	-82 31*	
2.	-66 23 170 12	10 40 A.M. to 11 45 A.M.	Direct. S. N. N.S.	-84 16·3 -85 01·6 -85 05·6 -84 29·6		+82	-83 21	-82 53	
3.	65 39 170 44	11 00 A.M. to Noon.	Direct. S. N. N.S.	-83 28·7 -83 46·0 -83 58·0 -83 46·5	N.N.W.	+86	-82 19	—81 51	Much motion.
4.	65 22 172 40	10 15 A.M. to 11 40 A.M.	Direct. S. N. N.S.	-82 18·3 -82 06·0 -82 19·0 -82 39·1	E. ½ S.	+ 9	-82 11	81 43	Much motion.
5.	-66 55 174 31	10 30 а.м.	Direct. Direct. Direct.	$ \begin{vmatrix} -82 & 03.7 \\ -82 & 19.9 \\ -82 & 06.1 \end{vmatrix} $	S.E. by E. E.S.E. S.E. $\frac{1}{2}$ E.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ -82 \ 13 $	iling amongst loose ice.
	-67 27 174 51	7 10 P.M. to 7 50 P.M.	Direct. S. N. N.S.	-83 03·6 -83 11·3 -83 09·2 -83 15·5	E.S.E.	-16	-83 26	-82 58	Sailing in the Sailing amongst Much motion.
6.	-68 17 175 0	11 00 а.м.	Direct. S. Direct. Direct. Direct.	-83 40·0 -83 35·0 -82 23·1 -82 35·4 -82 26·1	E.S.E. E.S.E. s.E. by s. s.E. s.S.E.		-83 57 -83 52 -83 26 -83 25 -83 41	-83 12	Sailing in the pack.
7.	-68 32 175 49	9 30 A M. to 10 15 A.M. to 11 00 A.M.	Direct. S. N. Direct. S. N.	-84 04·4 -84 10·3 -84 19·6 -84 10·8 -84 18·1 -84 22·3	E. W.	+18	-83 53 -83 59	-83 28	Standing off and on in a pool of water in the pack. Smooth water,
8.	-68 28 176 31	11 00 A.M. to Noon.	Direct. S. N. N.S. Direct.	-83 35·2 -83 57·7 -84 03·5 -84 03·2 -83 43·2	$\begin{cases} w. \text{ by s. } \frac{1}{2} \text{ s.} \\ w. \end{cases}$	-8 $\left +18\right $	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	83 17	
	On ice. -68 28 176 32	1 20 P.M. to 2 00 P.M. 3 00 P.M.	Direct. S. N. N.S. Direct.	-84 01:2 -84 06:8 -84 09:3 -83 55:7 -84 01:5	Observed on ice.		-84 02.9	83 34·9	The ice was slightly in motion.

^{*} The accordance of the results on the 1st of January with the ship's head on the north and south points, is extremely satisfactory with reference to the corrections, which on those points are very large and have opposite signs.

1841.	Posi	Long.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Incli- nation. Face east.	True Inclination.	Remarks.
Jan. 9.	-68 48 $-69 15$	17 ⁶ 25	h m 2 45 A.M. to 4 00 A.M.	Direct. S. N. N.S. Direct.	-82 41·8 -82 41·4 -82 48·6 -82 57·0 -83 09·4	S.S.E.		-84 0 8	-83 40	
10.	-70 23	174 50	10 35 A.M. to 11 40 A.M.	Direct. S. N. N.S.	-84 01·8 -83 51·4 -84 16·2 -83 52·5	s.	-88	-85 28	-85 00	
11.	—71 15	171 15	9 30 A.M. to 11 00 A.M.	Direct. S. N. N.S.	-84 48·4 -84 48·5 -84 49·3 -84 49·3	s.	-89	_86 18	—85 50	
	-71 24	170 44	4 40 P.M. to 5 50 P.M.	Direct. S. N. N.S.	-84 55·4 -84 56·9 -84 56·2 -84 51·4	s. by w.	-86	-86 21	—85 53	ations
12.	-71 47	170 52	10 46 A.M. to 11 40 A.M.	Direct. S. N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	w.s.w.	-14	-86 38	-86 10	Much motion; observations indifferent,
13.	-72 07	172 19	10 15 A.M. to 11 40 A.M.	Direct. S. N. N.S.	$\begin{bmatrix} -87 & 14.7 \\ -87 & 44.5 \\ -87 & 32.6 \\ -87 & 17.6 \end{bmatrix}$	\rightarrow E. by N. $\frac{1}{2}$ N.	+46	-86 41	-86 13	
	$ \begin{array}{c cccc} -71 & 51 \\ -71 & 54 \end{array} $		9 00 а.м.	Direct.	$ \begin{vmatrix} -87 & 04.5 \\ -85 & 03.8 \end{vmatrix} $	E. by N. ½ N. S.S.W.	+46 -79	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Much motion.
	—71 55	171 51	11 00 A.M. to Noon.	Direct. S. N. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.	+23	-86 23	-85 55	j
16.	-72 12	172 13	9 15 A.M. to 11 00 A.M.	Direct. S. N. N.S.	-85 48·2 -85 40·3 -85 48·5 -85 32·2	s. by w.	-87	-87 09	—86 41	
17.	-72 09	173 35	7 30 A.M. to 8 30 A.M.	Direct. N. N.S.	-86 53·3 -86 50·2 -87 01·0) E.	+24	-86 31	-86 03	Much motion.
18.	—72 57	176 06	11 00 а.м.	Direct. S. N. N.S. Direct.	-86 03.5 -86 32.2 -86 32.3 -86 04.0 -86 22.9	1	$egin{array}{c} -33 \ -14 \ -4 \ \end{array}$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	86 11	1
19.	-72 35	173 34	10 00 A.M. to 11 00 A.M.	Direct. S. N. N.S.	$ \begin{vmatrix} -86 & 12.4 \\ -86 & 21.8 \\ -86 & 22.2 \\ -87 & 07.0 \end{vmatrix} $	s.w. by w.	-33	-87 04	-86 36	

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1841.	Position.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attrac-	Mean Incli- nation. Face east.	True Inclination.	Remarks.
	Lat. Lor	g.				tion.			
Jan. 19.	-72 31 173 :	h m 4 30 p.m. to 5 30 p.m.	S.	-85 58·4 -85 55·5 -86 04·1 -85 45·8		-83	-87 19	-86 51	
20.	-73 47 171 4 -73 50 171 4	to 11 15 A.M.	S. N. N.S.	-86 56.7 -86 59.8 -86 58.4 -86 59.1 -86 49.0	S.E.	-51 $\left\{ -51 \right\}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-87 04	
	70 00 171	7 30 P.M. 7 50 P.M.	Direct.	$\begin{bmatrix} -86 & 04.7 \\ -87 & 45.0 \end{bmatrix}$	s.w. by w.	-34	-86 39 $-87 06$		
21.	-74 10 170 g	0 30 A.M. to 1 30 A.M.	S.	-86 39.6 -86 37.4 -86 38.5 -86 30.5	s. by E.	$-87 \Biggl\{$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		Direct. Direct. Direct.	-87 48·1 -88 04·7 -88 46·3 -88 51·2	E.	+24 +66 +85 +90	-87 24 $-86 59$ $-87 21$ $-87 21$		
	-73 56 170 5	to 4 20 P.M.	Direct. S. N. N.S.	-88 40·4 -88 57·1 -88 57·5 -88 58·2	N. by E.	+91	-87 22	\87 11	
22.	-73 56 172 2	11 25 A.M. to 0 15 P.M.	S.	$ \begin{vmatrix} -86 & 26 \cdot 1 \\ -86 & 32 \cdot 3 \\ -86 & 34 \cdot 2 \\ -86 & 21 \cdot 7 \end{vmatrix} $	s. by E.	-87	-87 56	J	Very unsteady.
23. 24.	-74 23 175 3 -74 35 173 0	5 Noon. 1 20 A.M. to 11 50 A.M.	N.	-86 59·0 -86 36·8 -86 23·0 -86 35·2	E. by s. s. by E.		-86 53 -87 59	$\left. \begin{array}{c} -87 & 29 \end{array} \right.$	
	-74 36 173 0		Direct. S.	-86 49·9 -86 41·4 -86 54·3		88	-88 16	j	
25.	-74 38 170 0 -74 44 169 4		N.S. Direct. S. N. N.S.	-86 39·7 -88 12·4 -88 21·0 -88 17·0 -88 05·0	S. ½ w.	$-88 \\ +24 \left\{ \right.$	-88 08 $-87 48 $ $-87 57 $ $-87 53 $ $-87 41$	-87 25	
	-74 47 168 2		Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. ½ w. s.w. by s.	-68	-88 50 -88 44	-88 18	
	-74 44 168 2	3 7 20 р.м.	Direct. Direct.	$\begin{bmatrix} -87 & 34.0 \\ -87 & 49.2 \end{bmatrix}$	S.S.W. ½ W. S.W.	$ \begin{array}{c c} -74 \\ -52 \end{array} $	-88 48 -88 41		
	-74 54 169 0 -74 58 169 0	7 45 A.M.	Direct. Direct. Direct.	-87 34·7 -87 46·4 -88 37·3	s. $\frac{1}{2}$ E. s.w. by s. E. by s.	$ \begin{array}{c c} -89 \\ -68 \\ + 7 \end{array} $	$ \begin{array}{r rrr} -89 & 04 \\ -88 & 54 \\ -88 & 30 \end{array} $	-88 21	
27.	75 22 168 4	8 2 20 A.M. to 4 10 A.M.	Direct. S. N. N.S.	-87 45·2 -87 45·2 -87 45·6 -87 23·3	s.s.e.	-84	-89 04	-88 36	

1841.	Position. Lat. Long.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
Jan. 27.	-76 06 168 11	h m 4 20 p.m. to 5 20 p.m.	Direct. S. N. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.E.	-52	-88 55	-88 27	
28.	-76 46 169 22 -77 29 170 30	11 15 A.M. 7 00 P.M.	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E.S.E. N.W. by N.	-12 +85	-88 52 -88 05	-88 00	
29.	-77 47 175 43	6 00 A.M.	Direct. S. N. N.S.	-88 44·7 -88 54·6 -88 50·2 -88 36·7	N. by w.	+91	-87 16	-86 48	Cd
30.	$\begin{bmatrix} -77 & 47 & 180 & 28 \\ -77 & 35 & 181 & 20 \end{bmatrix}$	3 10 A.M. Noon.	Direct. Direct.	-87 51·4 -87 43·9	n.n.w. n.w. by n.	+88 +83	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\left85 54 \right.$	Much motion
31.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9 30 A.M. to 11 30 A.M. 7 00 P.M.	Direct. S. N. N.S. Direct.	-87 30·3 -87 36·4 -87 26·0 -88 07·6 -85 28·8	s. by E. ¹ / ₄ E.	$+83$ $\left\{\begin{array}{c} +83 \\ -82 \end{array}\right\}$	$ \begin{array}{rrrr} -86 & 07 \\ -86 & 13 \\ -86 & 03 \\ -86 & 45 \\ -86 & 51 \end{array} $		CE
Feb. 1.	$\begin{bmatrix} -77 & 04 \\ 188 & 30 \\ -77 & 11 \\ 189 & 01 \end{bmatrix}$	10 30 A.M. to 11 30 A.M. 7 45 A.M.	Direct. S. N. N.S. Direct.	-85 45.9 -85 56.7 -85 52.5 -85 47.4 -86 02.5	1	-51	1	-86 12	
SECURIOR SEC		5 10 P.M. to 8 15 P.M.	Direct. N. N.S. Direct.	-85 59·2 -85 52·4 -85 36·3 -85 30·9	s.e. by s.		-86 51	-86 23	
2	-77 45 187 00 -77 56 186 35	11 35 A.M. to Noon. 10 P.M. 10 30 P.M.	Direct. Direct. Direct. Direct. Direct.	-86 27·2 -85 46·9 -85 37·5 -85 43·0 -85 34·4	s.e. by s. s.w. by s.		-86 04 -86 38 -86 43 -86 49 -86 57	86 10	
3.	77 17 185 26	10 00 A.M. to 11 15 A.M.	Direct. S. N. N.S.	-86 57·4 -87 02·3 -87 04·4 -87 07·0	w.s.w.	_14	87 17	-86 49	
4	77 00 192 18	9 30 а.м.	Direct. Direct. S. N. ?	-86 52·8 -86 43·5 -86 30·3 -86 35·3 -85 03·8	E. by N.	$\begin{vmatrix} +53 \\ +39 \\ -86 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left.\right $ -85 36	
	-77 06 192 34 -77 08 192 19	2 00 P.M. to 4 00 P.M.	Direct. Direct. S. N.	-86 29·5 -86 50·6 -86 49·0 -86 54·0	E.N.E.	+52	-85 54	-85 26	
5	77 24 192 56	3 00 A.M. to 4 00 A.M.	Direct. S. N. N.S.	-86 27·2 -86 36·0 -86 34·7 -86 46·5	} E.	+23	_86 13	-85 45	

1841.	Position.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attrac-	Mean Inclination. Face east.	True Inclination.	Remarks
	Lat. Long.					tion.			
Feb. 5.		h m 11 45 A.M. 2 30 P.M. to 4 00 P.M.	Direct. Direct. S. N. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	} s.	-89	-86 34	-86 06	
6.	-77 9 188 50	9 00 A.M. to 10 45 A.M.	Direct. S. N. N.S. Direct.	-86 52·2 -87 03·0 -87 14·4 -87 29·8 -85 03·5	E.N.E.	-89	-85 59 -86 10 -86 21 -86 37 -86 33		
	-77 12 188 08	10 55 а.м.	Direct.	-85 12.1	s.s.w.	-79	$-86 \ 31$	IJ	
7.	-76 58 186 40 -77 01 186 35	6 00 A.M. to 7 15 A.M. 11 30 A.M.	Direct. S. N. N.S. Direct.	-85 27·6 -85 38·6 -85 35·8 -85 29·3 -86 05·1	s. by w.	$\begin{vmatrix} -86 \\ -14 \end{vmatrix}$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		
8.	$-77 ext{ 40} 187 ext{ 05} $ $-77 ext{ 47} 187 ext{ 18}$	11 40 A.M. 1 30 P.M. to 3 45 P.M.	Direct. Direct. S. N.	-87 02·5 -87 10·6 -87 04·5 -87 29·6	$\begin{cases} \text{E.N.E.} \\ \text{N.E. by E.} \frac{1}{2} \text{ E.} \end{cases}$	$\left +53 \right +59 \left\{$	$-86 ext{ } 10 $ $-86 ext{ } 12$ $-86 ext{ } 06$ $-86 ext{ } 31$		
			N.S.	-87 35·1	}	Ĺ	$-86 \ 36$	J	
9.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10 35 A.M. 0 20 P.M.	Direct. Direct.	-87 16·3 -85 27·9	N.E. s.e. by s.	$^{+75}_{-66}$	$-86 01 \\ -86 34$		
	-77 39 187 06 -77 32 186 38	5 45 A.M. to 8 00 A.M. 11 40 A.M.	Direct. S. N. N.S. Direct.	-85 15·1 -85 26·8 -85 34·4 -85 24·6 -86 33·7	s. by E. w. by s.	-86 $+5$	$ \begin{array}{rrrr} -86 & 41 \\ -86 & 53 \\ -87 & 00 \\ -86 & 50 \\ -86 & 29 \end{array} $	$\left.\right\}$ -86 19	
11.	-76 55188 40	2 50 A.M. 11 40 A.M. 1 00 P.M.	Direct. Direct. S.	-87 16·6 -85 55·0 -85 29·3 -85 39·4	$\left.\begin{array}{c} \text{N.w.} \\ \text{s.w.} \\ \end{array}\right\} \text{ s.s.w. } \frac{1}{2} \text{ w.}$			$\left.\right\}$ -86 07	
12.		10 15 A.M. to 11 40 A.M.	Direct. N. N.S.	-86 04·0 -86 39·8 -86 09·0		-33	-86 51	-86 23	Much motion.
	-76 16 174 14 -76 22 176 9 -76 16 175 50	3 A.M. 11 40 A.M. 2 00 P.M.	Direct. Direct. Direct. S. N. N.S.	-86 15.5 -86 20.8 -86 23.3 -86 23.6 -86 30.7 -86 30.3	S.S.W.	-79	-87 43	-87 15	
	$-76 \ 14 172 \ 35$	11 20 р.м.	Direct.	-86 34.0	s.	-90	-88 04	-87 36	
15.	-76 03 169 30	11 20 A.M.	Direct. N.	$\begin{bmatrix} -87 & 05.3 \\ -87 & 13.5 \\ 05 & 02.1 \end{bmatrix}$	} s.	-91	-88 36 -88 44		
	-76 03 167 58 -76 09 167 00 -76 10 166 50 -76 12 166 30	Noon. 4 40 p.m. 7 10 p.m. 9 00 p.m. 11 00 p.m.	N.S. Direct. Direct. Direct.	-87 03·1 -87 30·1 -87 35·3 -87 36·4 -87 42·0	S.S.E.	-81	$ \begin{array}{rrrr} -88 & 34 \\ -88 & 51 \\ -88 & 56 \\ -88 & 57 \\ -89 & 03 \end{array} $		

1841.	Position. Lat. Long.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Incli- nation. Face east.	True Inclination.	Remarks.
Feb. 16.	$-\r{7}6 20 165 32$	h m 6 00 A.M. to 8 00 A.M.	Direct. S. N. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E.		$-89 ext{ 04} \\ -89 ext{ 10} \\ -88 ext{ 59} \\ -88 ext{ 58}$		
17.	-76 46 165 2 -76 31 165 04 -76 26 164 02	3 20 A.M. 4 15 A.M. 11 45 A.M. 4 00 P.M. 5 00 P.M.	Direct. Direct. Direct. Direct. Direct.	-88 33·2 -87 51·2 -87 05·3 -87 13·3 -89 34·3	$\left.\begin{array}{c} \text{E.S.E.} \\ \text{S.S.W.} \\ \end{array}\right\} \text{S.} \\ \text{N.E. by E.} \frac{1}{2} \text{E.} \\ \end{array}$	$\begin{bmatrix} -13 \\ -81 \\ -91 \\ +58 \end{bmatrix}$	$ \begin{array}{rrrr} -88 & 46 \\ -89 & 12 \\ -88 & 36 \\ -88 & 44 \\ -88 & 36 \end{array} $	_88 19	
	-76 05 166 11 -75 49 167 32 -75 03 168 44	11 40 A.M. 8 15 P.M. 11 00 A.M. to Noon.	Direct. Direct. S. N. N.S.	-89 26.5 -88 10.1 -87 21.0 -87 35.0 -87 44.2 -87 15.9	} w. s.w.	+26 { -52	-89 00 -87 44 -88 13 -88 27 -88 36 -88 08	-87 53	-in
20. 21.		Noon. 9 00 A.M. to 10 15 A.M.	Direct. Direct. S. N.	-87 02·5 -86 01·8 -86 03·6 -86 10·7	$\left.\begin{array}{c} \text{s.w.} \\ \\ \\ \end{array}\right\} \text{s.w.by w.} \frac{1}{2} \text{w.}$	-51 -27	-87 54 -86 26 -86 28 -86 35	86. 23	Much motion.
	$\begin{vmatrix} -71 & 04 \\ -70 & 52 \\ 168 & 11 \\ -70 & 48 \\ 167 & 52 \end{vmatrix}$	10 50 A.M. 6 40 P.M. 8 15 P.M.	Direct. Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	w. w.s.w. w. by s.	$ \begin{array}{r} +24 \\ -14 \\ +5 \end{array} $	$-86 08 \\ -86 29 \\ -86 25$		ion.
22.	167 20	6 40 A.M. to 7 30 A.M.	Direct. S. N. N.S.	$ \begin{array}{c cccc} -87 & 28.0 \\ -87 & 57.8 \\ -87 & 51.4 \\ -87 & 51.3 \end{array} $	N.N.E.	+88	-86 19	—85 51	A great deal of motion.
	-70 27 166 40 -70 18 167 28 -70 14 167 34	5 00 P.M. 11 40 A.M. 10 00 A.M. to 11 50 A.M.	Direct. Direct. S. N. N.S.	-87 02.2 -87 31.9 -85 50.4 -85 45.8 -85 42.7 -85 50.0		1 + 70	-86 22	86 19	g _A
25.	-70 14 167 16	6 30 A.M. to 8 00 A.M.	Direct. S. N.	$ \begin{vmatrix} -85 & 20.7 \\ -85 & 04.7 \\ -84 & 49.2 \end{vmatrix} $		-89	-86 50 $-86 34$ $-86 18$	$-86\ 06$	Much motion.
26.	$\begin{bmatrix} -70 & 02 & 167 & 35 \\ -69 & 52 & 168 & 09 \end{bmatrix}$	5 00 р.м. 11 30 а.м.	Direct. Direct.		N.W. W.S.W.	$ +75 \\ -14$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\left \right\} - 85 41$	
27.	-69 24 167 55	10 30 A.M. to Noon.	Direct. N.S. Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.E. E.S.E. N.W.	-51 $\left\{\begin{array}{c} -51\\ -14\\ +75 \end{array}\right.$	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-85 28	
28.	-69 40 167 48 -69 56 167 36	6 00 A.M. to 8 00 A.M. Noon.	Direct. N. N.S. Direct. Direct.	-85 03·2 -85 20·6 -84 47·6 -85 14·4 -86 45·6	s. by E. s. by E. n.w. by w.	$\begin{bmatrix} -86 \\ -86 \\ +64 \end{bmatrix}$	-86 29 -86 47 -86 14 -86 40 -85 42	85 54	-

1841.	Position. Lat. Long.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
Mar. 1.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	h m 11 30 A.M. 2 00 P.M. 2 30 P.M. 3 00 P.M. 3 30 P.M.	Direct. Direct. N. N.S. Direct.	-86 51·5 -86 28·5 -87 40·5 -87 07·0 -86 49·5	N.w. by w.	$+64$ $\left\{ +74 \right\}$	-85 48 -85 25 -86 37 -86 03 -85 36	85 26	Much motion.
2.	-68 28 168 10	9 30 A.M.	Direct. S. N. N.S. Direct.	-86 12·0 -86 12·1 -86 10·2 -86 32·4 -86 24·0	w. by n.	$\begin{vmatrix} +38 \\ +64 \end{vmatrix}$	-85 34 -85 34 -85 32 -85 54 -85 20	85 07	
3.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 15 A.M. 7 45 A.M. 11 45 A.M.	Direct. S. N. N.S. Direct.	-85 01·8 -85 19·2 -85 38·5 -85 32·1 -84 55·5			-84 41 -84 58 -85 17 -85 11 -84 35	-84 28	
5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 40 A.M. 10 30 A.M. 11 10 A.M. 11 40 A.M. 7 00 A.M. 11 40 A.M. 5 10 P.M.	Direct. Direct. N. N.S. Direct. Direct. Direct.	-85 00·5 -85 05·8 -85 17·2 -85 08·8 -83 38·3 -83 28·3 -84 34·0	N.E. N. S.S.W. $\frac{1}{2}$ W. S.W. by S. W.	$\begin{vmatrix} +72 \\ +91 \\ -69 \\ -63 \\ +18 \end{vmatrix}$	-83 49 -83 35 -83 46 -83 38 -84 47 -84 31 -84 16	-83 35	A great deal of motion. Ship rolling deep.
7.	-65 53 162 14	10 00 A.M. 10 40 A.M. 11 20 A.M.	Direct. S. Direct.	-85 17·3 -85 39·2 -84 08·5	N.W. w.s.w.	$\begin{vmatrix} +72 \\ -17 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-83 51	
8.	64 41 162 34	10 10 а.м.	Direct. S. N. N.S.	-84 33·7 -84 47·7 -84 52·0 -84 32·6	N.E. by N.	+79	$\begin{bmatrix} -83 & 15 \\ -83 & 29 \\ -83 & 33 \\ -83 & 14 \end{bmatrix}$	$-82\ 55$	
10.	$\begin{array}{c} -64 & 38 & 162 & 50 \\ -64 & 22 & 164 & 32 \\ -64 & 05 & 163 & 17 \\ -64 & 13 & 163 & 18 \end{array}$	11 15 A.M. 7 30 A.M. 9 30 A.M.	Direct. Direct. Direct. Direct.	-84 26.5 -84 04.5 -85 01.7 -84 55.3	N.N.E. N.N.E. N.w. by w.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	-82 54	Much motion on the 10th.
	$63 \ 57 \ 161 \ 11$ $63 \ 28 \ 159 \ 35$	6 00 A.M. 6 30 A.M. to 7 45 A.M.	Direct. Direct. S. N. N.S. Direct.	-83 06·5 -82 44·3 -82 47·6 -82 59·7 -82 10·5 -83 07·0	s. by w.	$\begin{bmatrix} -69 \\ -82 \\ -25 \end{bmatrix}$	-84 16 -84 06 -84 10 -84 22 -83 33 -83 32		Much motion.
14.	62 41 156 59	10 30 A.M. to 11 10 A.M. 11 20 A.M.	Direct. S. N. N.S. Direct.	-83 09·0 -83 17·0 -83 28·7 -83 14·7 -81 52·5	w. w.	$+18$ $\left\{ -75 \right\}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Much
15	63 50 156 06	6 45 A.M. to 7 40 A.M.	Direct. S. N. ?	-82 38·0 -82 42·3 -83 08·3 -83 19·5	$\left.\right $ s. $\frac{1}{2}$ w.	85	_84 22	-83 54	

1841.	Position.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
	Lat. Long.	h m							
Mar. 16.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 45 A.M. 1 00 to 3 15 P.M.	Direct. Direct. S.	$ \begin{vmatrix} -83 & 28 \cdot 2 \\ -83 & 15 \cdot 0 \\ -83 & 52 \cdot 8 \end{vmatrix} $	$\begin{cases} s.w. \frac{1}{2} s. \\ s.w. by s. \end{cases}$	-57 -64	-84 25 -84 19 -84 57		
	-64 13 154 03		N. N.S. Direct.	-83 37·0 -83 28·3 -83 23·0	s.w. by s.	-64	$ \begin{array}{r rrr} -84 & 41 \\ -84 & 32 \\ -84 & 27 \end{array} $	-84 06	
17.	_64 20 153 02	10 15 A.M. to 11 15 A.M.	Direct. S. N. N.S. Direct.	-83 27.6 -83 48.1 -83 40.9 -83 47.2 -83 40.7	s.w. by s.	$\begin{vmatrix} -64 \\ -50 \end{vmatrix}$	$ \begin{array}{rrrrr} -84 & 32 \\ -84 & 52 \\ -84 & 45 \\ -84 & 51 \\ -84 & 31 \end{array} $	-84 14	ell.
18.	-63 54 151 56	5 45 A.M. to 7 00 A.M.	Direct. N. N.S.	-84 44·0 -85 14·5 -85 35·2	w. by n.	+ 37	-84 34	-84 06	A heavy head swell.
19.	-64 18 149 09	11 40 A.M. 1 40 P.M.	Direct. Direct. S.	$ \begin{vmatrix} -84 & 00.5 \\ -84 & 09.7 \\ -84 & 26.3 \end{vmatrix} $	} s.w. by s.	-64	-85 05 $-85 14$ $-85 30$	-84 48	[Ā
	$ \begin{vmatrix} -64 & 26 & 148 & 20 \\ -64 & 56 & 147 & 14 \end{vmatrix} $	3 00 p.m. 6 15 p.m.	N. N.S. Direct. Direct.	-84 26·1 -84 49·0 -84 05·0 -84 15·0	s.w. by s.	$\begin{bmatrix} -64 \\ -76 \end{bmatrix}$	$ \begin{array}{rrrr} -85 & 30 \\ -85 & 53 \\ -85 & 09 \\ -85 & 31 \end{array} $	$-85 \ 03$	1
20.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 40 A.M. 8 50 A.M. 10 00 A.M.	Direct.	-84 55·7 -85 25·8 -86 03·5	s.w. w.s.w. w.n.w.		$ \begin{array}{r rrrr} -85 & 47 \\ -85 & 41 \\ -85 & 12 \end{array} $	-85 05	
	-65 12 144 07 -65 10 143 21	10 30 A.M. 11 20 A.M. 11 40 A.M.	Direct. Direct. Direct.	-84 54·3 -85 08·0 -85 12·8	s.w. s.w. by w. w.s.w.	-51 -33 -15		$-85\ 10$	
	-65 10 143 21 -65 06 142 40	11 50 A.M. to 1 00 P.M. 4 45 P.M. 6 20 P.M.	Direct.	-85 45·0 -85 48·3 -85 56·7 -85 55·0 -85 46·5 -85 44·9	w.s.w. w. w. w. by N.	-15 $+21$ $+21$ $+38$	-86 00 -86 03 -86 12 -85 34 -85 26 -85 07		
21.	-64 20 140 40 -64 08 140 14	5 40 A.M. to 7 00 A.M.	Direct. S. N. N.S. Direct. Direct.	-85 45.8 -85 53.4 -85 59.0 -86 11.0 -85 51.7 -84 24.5*	w.n.w. N. ½ W.	+ 52	-84 54 -85 01 -85 07 -85 19 -85 00	-84 36	
22.		9 30 A.M. to 11 10 A.M.	Direct. S. N. N.S. Direct.	-85 54·5 -86 33·1 -86 57·1 -86 25·7 -86 02·0	N.w. by w.	+62	85 14	-84 46	A.

^{*} There is an obvious error here in the degree recorded; it should be probably 86°. The observation is not employed.—E. S.

1841.	Position.	Time of day.	Method employed.	Observed Inclination.	Ship's head.	Correction for ship's	Mean Inclination.	True Inclination.	Remarks.
	Lat. Long.			Face east.		attrac- tion.	Face east.		
Mar. 22.	0 / 0 /	h m	Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.w. by w.	+62	$-85 {14}$	-84 46	
22. 23.	-62 46 138 22 -62 13 136 20	4 00 P.M. 10 15 A.M. to Noon.	Direct. Direct. S. N. N.S. Direct.	-85 48.8 -85 37.9 -85 58.0 -85 51.5 -86 10.9 -85 32.5	N.w. by w.	+62	-84 48	-84 20	
24.	-61 20 134 05 -61 11 133 52	6 10 A.M. to 7 00 A.M. 11 40 A.M.	Direct. S. N. N.S. Direct.	-85 19·1 -85 17·7 -85 33·9 -85 46·2 -85 07·5	N.w. by w.	+62	-84 23	-83 55	
25.	-60 22 131 27 -60 19 131 20	11 45 A.M. 3 15 P.M. to 4 15 P.M.	Direct. Direct. S. N. N.S.	-85 05.5 -85 04.1 -85 20.6 -85 21.4 -85 32.5	N.w. by N.	+72 +79	-83 54 -83 45 -84 02 -84 02 -84 13		
26.	-59 25 130 14	10 15 A.M. to 11 40 A.M.	Direct. S. N. N.S. Direct.	-84 29.0 -84 49.0 -84 28.7 -84 56.2 -84 33.5	N.w. by N.	+79	-83 20	-82 52	
27.	-58 06 128 43	11 40 а.м.	Direct.	-84 03.0	N.N.W.	+86	$-82 \ 37$	-82 09	
28.	-57 22 127 37	10 30 A.M. 11 45 A.M.	Direct. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	W. E.N.E.	+18 +49	$-82 20 \\ -82 02$		Much motion.
29.	-56 28 129 57	11 30 а.м.	Direct.	-82 21.5	N.E.	+71	-81 11	-80 43	Ship very unsteady.
30.	-55 00 131 43 -55 11 132 10	6 15 A.M. to 7 15 A.M. 11 45 A.M.	Direct. S. N. N.S. Direct.	-81 28·5 -81 14·1 -82 29·2 -82 36·0 -81 41·0	N.E. by E. N.E. by N.	Ì	$-80^{\circ}12^{\circ}$	-80 15	Ship very Sl unsteady. u
	-54 55 132 50	5 00 p.m.	Direct. S. N. S. N. S. N. N.	-81 26·5 -81 48·5 -81 59·7 -81 54·7 -81 55·9 -82 05·5	N.E. by N. N.E. by N.	+77	-80 10 -80 32 -80 43 -80 38 -80 39 -80 48	80 07	
31.	-54 4 134 54 -54 00 135 02	11 40 A.M. 0 15 P.M. 1 00 P.M. 2 00 P.M. to 3 30 P.M.	Direct Direct. Direct. S. N. N.S. Direct.	-79 45·5 -80 25·0 -80 00·0 -81 21·3 -81 50·2 -81 46·4 -81 26·6 -81 22·7	$ \begin{array}{c} E. \frac{1}{2} N. \\ E. \frac{1}{2} N. \\ N.W. \end{array} $	+27 +19 +27 +70	-79 19 -80 06 -79 33 -80 11 -80 40 -80 36 -80 17 -80 13	-79 39	

1841.	Pos	ition.	Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
April 1.		135° 18′	h m 9 00 A.M. to 11 45 A.M.	Direct. S. N. N.S. Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.E.	+82	-79 37	-79 09	
2.	-51 16	136 50	6 00 A.M. to 7 15 A.M.	Direct. S. N. N.S.	-79 55·8 -79 49·5 -79 47·7 -79 45·0	N.N.E.	+82	-78 27	—77 59	
3.	-48 56 -48 24	138 34 138 32	11 45 A.M. 2 00 P.M. to 4 00 P.M.	Direct. Direct. N. N.S.	-78 41·6 -78 50·3 -79 09·4 -78 13·0	N.N.E.	+81	-77 22	—76 54	Much sea.
4.	-46 55	139 55	7 20 to 8 20 A.M.	Direct. N. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E.	+69	-76 10	-75 42	Heavy sea, ship rolling deep.
	-46 34	140 36	10 30 A.M. to 11 50 A.M. Noon.	Direct. N. N.S. S. N. N.S. Direct.	-77 00·5 -77 39·8 -77 37·9 -77 37·5 -77 33·2 -77 49·1 -78 11·5	N.E.				Instrument in wrong azi- muth.
		140 40	0 40 to 1 30 p.m. 4 40 p.m. to 5 50 p.m.	Direct. S. N. N.S. Direct. S. N. N.S.	-77 23·0 -76 33·5 -76 29·0 -77 18·0 -76 48·5 -76 29·7 -76 10·2 -76 50·6		+69	-75 47 -75 33	-75 12	Heavy sea. Much motion.
5.		2145 10	6 30 A.M. to 8 30 A.M. 11 40 A.M. 4 30 P.M. to 5 00 P.M.	Direct. S. N. N.S. Direct. Direct. S. N.	-76 04·0 -75 02·2 -75 11·5 -75 03·2 -75 49·5 -75 28·5 -74 57·6 -75 20·9	N.E. by E.	+60	-74 20 -74 24	}-73 54	
6		145 57 1 146 03	11 35 A.M. 1 20 P.M. to 4 30 P.M.	Direct. Direct. S. N. N.S.	-73 49·8 -73 35·5 -73 43·0 -73 41·9 -73 47·6	N.E. by E. $ \begin{array}{c} \text{N.E. } \frac{1}{2} \text{ E.} \end{array} $	+58 + 62	$\begin{bmatrix} -72 & 52 \\ -72 & 34 \\ -72 & 41 \\ -72 & 40 \\ -72 & 46 \end{bmatrix}$	-72 15	Running along the land.

Observations of the Intensity of the Magnetic Force made in Her Majesty's Ship Erebus, from September 1840 to April 1841, with Needle R. F. 4.

Observers Captain Ross and Lieutenant Smith, R.N.

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Sept. 17.	tory, H	c Observa- lobarton. 147 24	Deflector S. wt. $\frac{1}{2}$ gr. wt. 1 gr. wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. 3 grs.	50 00·8 2 41·4 5 22·7 8 14·6 10 49·6 16 15	52 52 52 52 52 52 52 52	Observed on shore*.	1.820	••••	1.820	
Oct. 17.		To obtain corrections for the ship's attraction.	s. s. s.	49 23 49 51 49 27·2 49 39	54 54 54 54	w.	1.869 1.833 1.864 1.849	035 003 043 039	1.830 1.821	
21.		trac	S. \	49 50.9	51	W.N.W.	1.833	+.008		
		at	S.	49 48.8	51	S.E.	1.835	 ∙031		
29.		ip's	S.	50 19.8	48	1	1.792	+.028	ı	
		shi	S S.	50 23.7	48	N.N.E.	1.787	+.024		
		he	S. S.	50 21·8 50 02·9	48 48	N.E. E.N.E.	1·789 1·816	+.020 + .008	-	
		r t	S.	49 53.5	48	E.	1.828	003	1.825	
		4	s.	50 09.4	48	N.N.W.	1.807	+.024		
		Su	S.	50 12.6	48	N.W.	1.803	+.020		
		eţi.	S.	49 40	48	w.s.w.	1.848	-017	1.831	
		re.	S.	49 52.2	48	w.	1.831	003		
		60	S.	49 56.2	48	1	1.826	+ .008		
		.a l	S.	49 28.8	48	1	1.862	031	i i	
		taj	S.	49 28.2	48	1	1.863	039	i	
		0	S. S.	49 27.0	48	1 1	1.864	046		
		T_{0}	S. S.	49 24.5	48 48	1	1.867	-·039	1	
			S. S.	49 39·5 49 52·7	48	1	1·849 1·830	-·031 -·017		
		9	~•	15 02 7	10	E.S.E.	1 000	01,	1 010)	
Nov.13.	-44 10	149 29	S.	49 23.8	54	[] [1.868	017	1.851	
			N.	47 05.9	54	} E.S.E. {	1.855	017	1.838	
14.	-45 13	151 57	S.	49 34.5	45	[]	1.855		$1.824 \} 1.833$	Much motion.
			\mathbf{N}_{\cdot}	46 50.5	45	} s.e. {	1.872		1.841	Observations by no means good.
15.	-45 33	152 45	S.	49 56.9	51	} E. {	1.824		1.821	Ship pitching
,,	46.70		N.	46 53.5	51	li " j	1.869		1.800	greatly.
16.	-46 18	154 30	S.	49 50.7	57		1.833	017		
,,,	47 40	157 40	N.	47 17	57	K	1.841		1.824	,
17	$-47 ext{ } 46$	157 40	S.	49 52	51		1.831	1	$\{1.811\}$	Much motion.
10	40 00	160 19	N.	47 15	51 50	$\left \begin{array}{c} \mathbf{s.e. by } \mathbf{E.} \frac{1}{2} \mathbf{E.} \end{array} \right $	1.843	020	1 020)	
18.	-49 20	100 19	S. N.	49 34 46 47·2	50 50	11 - 11	1·856 1·876	-·020	$1.836 \} 1.846$	
			TA*	40 4/2	90	h A	1.910	_ UZU	1.856 }	

^{*} The angles of deflection with 4, 5 and 6 grains, not having been observed at Hobarton, have been computed from the angles produced by the five weights which were employed at that station; they are as follows:—

gr. 4.... 22 06

^{5 28 03.5}

^{6 34 21.}

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Nov. 19.	50 ′28	16 4 ģ	S. N.	49 11 47 20	49 49	} E. {	1·884 1·838		$1.881 \ 1.835$ 1.858	
21.	Aucklan -50 33	d Island*.	$\begin{array}{c} S. \\ N. \\ wt. \frac{1}{2} gr. \end{array}$	49 44·2 47 27·6 2 33·9	42	w.n.w. {	1.842 1.830 1.830	+·008 +·008	1	
26.	At	anchor.	wt. 1 gr. wt. 2 grs. wt. 3 grs. S.	5 13 10 27·3 15 28·6 49 29·2	50 50 50 41	\rightarrow \text{N.w. by w. } \begin{cases} \text{s.s.w.} \end{cases}	1·876 1·884 1·909 1·862	+·013 +·013 +·013 -·037	1.897 >1.864 1.922 1.825	
27. 24.	On s	shore.	S. S. N. wt. ½ gr. wt. 1 gr.	49 50·6 49 29 46 50·2 2 33·5 5 18·4	42 53 53 52 52	W.S.W.	1.833 1.862 1.873	-013	1·830 J 1·859	
			wt. $1\frac{1}{2}$ gr. wt. 2 grs. wt. 3 grs. S.	8 02·2 10 36·8	52 52 52 52 46		1.867 1.856 1.851 1.778]		
26.	Ĭ	$\begin{bmatrix} \text{Island.} & \{ \\ \end{bmatrix}$	N. S.	47 38 47 50·7	46 44	Observed on shore.	1·818 1·981	}	• • • • • • • • • • • • • • • • • • • •	Excessive local attraction.
30.	Ocean	Point. Bay.	N. S. S. S. N.	45 3·6 49 49·8 49 28 49 27 47 31·7	44 51 51 58 58		1.993 1.834 1.863 1.864 1.826	}	1.847	
Dec. 2.	Aucklai	nd Island. $\left\{ \begin{array}{c} \\ \end{array} \right.$	S. N. S.	59 56 57 19·2	55 55 50	s.w.	1.854	} -∙030	1.8047	Excessive local attraction.
7.			s. s. s.	49 35 49 05·9 49 57·2	50 49	s.w. s.s.w. w. by s.	1·891 1·824	-·036 -·008	1.855	
8.			S. S. S.	49 21·9 49 19 49 29·2	52 52 50	S. S.S.E. S.E.	1.871 1.874 1.862	041 036 030	1·838 1·832	
	At and	chor.	s. s. s.	49 29·5 49 44·9 49 46·7 49 58	50 50 51 52	E.S.E. E. E.N.E. N.E.	1.862 1.841 1.838 1.823	015 003 +-008 +-018	1·838 >1·836 1·846	:
	And the second s		S. S. S.	50 06·9 49 51·4 50 01·8	52 50 50	N.N.E. N. N.N.W.	1.810 1.832 1.817	+·021 +·026 +·021	1·831 1·858 1·838	
10.		Ĺ	s. s.	50 16·3 49 27·2	50 52	N.W. S.E.	1·797 1 864	+·018 -·030	1 1	

* Mean of the results at Auckland Island, omitting those which appear to have been affected by excessive local attraction:

November 21 and 26, on board . . 1 864 November 24, on shore . . 1 859 November 30, on shore . . 1 847 December 6, 7 and 8, on board . . 1 836

1840.	Lat.	Long.	Method employed.	Angle of deflection.		Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 14. 16.	o , Campbel at anc	l Island*,∫	S. S. S.	50 01·4 49 39·2 49 04·5 49 20·5	50 50 52	N.W. W. s.s.w.	1.849 1.893	+·018 -·003 -·037	1.846 >1.846	
15.	On sh 52 42		N. wt. ½ gr. wt. 2 grs. wt. 3 grs. wt. ½ gr. wt. 1 gr. wt. 2 grs. wt. 3 grs. N.	49 20.3 46 10.8 2 35.3 10 12.1 15 30.2 2 32.9 4 59.2 10 12.6 15 30.2 49 17 46 45.7	55 55 55 55 52 52 52 52 52 52	Observed on shore.	1.873 1.917 1.930 1.906 1.963 1.929 1.906 1.877 1.878	>	1-909	
18.	-53 47	169 02	S.	49 13.6	44	S.S.E.	1.881	-·037	1.844	
10.	-54 25		Ñ.	46 18.5	44		1.908	- ⋅034		
19.	-5550		N.	45 48	48	1) - r	1.943	040		
	-57 15		N.S. N.	22 39·5 45 42·7	48 38	$\}$ s. by w. $\{$	1.949	 ∙035	J	
			N.S.	22 26		S.S.E. {				
	-57 54		N. N.S.	45 44·5 22 25·6	42	$\left. \left. \right \right\}$ s. by E. $\left\{ \left \right \right. \right.$	1.948	 ∙037	1.911	
22.	—58 57	170 57	S. N. N.S.	48 17·7 45 25·2 22 31·7	41	s. {	1·951 1·969	·040 ·040	$1.911 \atop 1.929$ 1.920	
23.	-59 41	169 38	S. N.	48 11·5 45 20·2 22 29·5	39	$\left. \left. \right \right\}$ s.s.w. $\left\{ \left \right \right. \right.$	1·959 1·975	-·031 -·031	$1.928 \\ 1.944$ 1.936	
	$-59 \ 48$	169 42		22 31.5	37	E.				
24.	-60 14			45 16·9 22 27	36 36	$\left \begin{array}{c} \end{array} \right $ s.e. $\frac{1}{2}$ s. $\left\{ \left \begin{array}{c} \end{array} \right \right $	1.978	027		
	-60 31	170 32	N.	47 59·2 45 08·1 22 27	42 41 40		1·972 1·988	029 029	$1.943 \\ 1.959$ 1.951	
	-60 46	170 44	S. N.	48 13·7 45 15·1 22 29·3	40 40 39	1 (· 027 · 027	1.953	
25.	-61 34	170 40	N.	45 08·4 22 27·6	35 35	$\left.\right $ s. $\left\{\right $	1.988	032	1.956	
26.	-62 04	172 48	N.	45 00 22 15·7	46 45	16 4.	1	+.011	_	
28.	$-62 \ 40$	174 40	S.	47 33·2 44 30·6	34 34		2·001 2·029	-·032 -·032	$1.969 \atop 1.997$ 1.983	
	-62 52	İ	N.S.	22 0·5 22 15·2	34 34	$\begin{bmatrix} s & s \end{bmatrix}$			-	
29.	-64 0		S. N.	47 53·9 44 34·2	33 33		1·978 2·026	026 026	$\left. egin{array}{c} 1.952 \\ 2.000 \end{array} \right\} 1.976$	
	-64 06	172 38	S.	22 11·7 47 45	33 34				1·960 1·986 } 1·973	
	į			44 42.3	34	} s. by w. {	2.016	030	1.986 / 1.979	1
			N.S.	22 14.7		Juli				

^{*} Mean of the results at Campbell Island :

December 14 and 15, on shore. 1.909 December 14 and 16, on board. 1.846 \} 1.877.

		。 ,			Tempera- ture.	Ship's head.	Intensity.	ship's attrac- tion.	Corrected Intensity.	Remarks.
	61 21		N.S. S.	22 17·6 47 17	33 44	s. by w.	2.018	- ∙030	1.988 } 1.988	
	-04 51	173 00	N. N.S.	44 41·1 21 26·7			2.018	030	1.988	
31	-65 58	171 47	S. N.	46 58·5 44 34	34	s. \	2·039 2·026	028 028	1.998	
-	66 17	170 57	N.S. S. N.	21 36·2 47 29·5 44 47·1	35	$\begin{cases} \\ \\ \\ \\ \\ \end{cases} $ s. by w. $\frac{1}{2}$ w. $\begin{cases} \\ \\ \\ \end{cases}$	2·005 2·012	·023 ·023		
1841. Jan. 1.	-66 30	169 13	N.S. S. N.	21 52·3 47 15·8 44 30·1	37	$\left\{\begin{array}{cccccccccccccccccccccccccccccccccccc$	2·020 2·030	•027 •027	1.993	
-	66 32	169 45	N.S. S.	21 43·5 47 13	35	$\left. \left. \right\} \right.$ N. $\left. \left\{ \right. \right. \right.$	2.023	+.006	22.008	,
2.	-66 23	170 12	N.S. S. N.	22 05·4 47 51·5 44 13·9	36		1·981 2·047	+·004 +·004	$\left\{ egin{array}{c} 1 \cdot 985 \\ 2 \cdot 051 \end{array} \right\} 2 \cdot 018$	
3.	-65 39	170 44	N.S. S. N.	21 56·1 47 01·6 44 14·5	35 34				$2.040 \ 2.052$ 2.046	Much motion.
4.	-65 22	170 40	N.S. S. N.	22 37·5 47 00·5 44 20·5	33 34	$\left\{\begin{array}{c} \\ \\ \\ \end{array}\right\} \text{E. } \frac{1}{2} \text{ s. } \left\{\begin{array}{c} \\ \\ \end{array}\right.$	2·037 2·040		$2.024 \ 2.027$ 2.025	
5.	-66 55	174 31	N.S. S.	21 54·1 47 11·7	35	IJ	1		J	Sailing among loose ice.
6.	– 68 17	175 0	N. N.S. S.	44 35·9 21 55 47 26·1	34	E.S.E.	2.009	0 15		Among ice.
7.	-68 32	175 49	S. N. S.	47 15·8 44 27·9 47 16·5	30	E. {	2.020 2.032 2.019	-·012 -·012 -·012	2.020 >2.011	Standing off and on in the pack.
8.	-68 28	176 31	N. S.	44 21·1 47 09·1	39	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2·040 2·027	-·012 -·002	2·028] 2·025]	·
			N. N.S. S.	44 04·7 21 55 47 03·3	39	E. by N. $\frac{1}{2}$ N. w. by s. $\frac{1}{2}$ s.	2·058 2·034		2.021	
	-68 28	176 32	N.S. S.	44 22·6 22 00·1 47 15·7	42	w. {	2·038 2·021	- ∙011	2·027 J 2.021 \	
	,	1,0 0%	N. N.S.	44 17·1 21 54·8		Observed	2.044		2.044	
			wt. $\frac{1}{2}$ gr. wt. 3 grs. wt. 6 grs.	2 28 14 34·3 30 38·7	41	on ice.	2·021 2·015		2·021	
9.	-68 48	176 45	S. N. N.S.	47 06 44 16 21 48·2		$\left.\right $ s.s.e. $\left\{\right.$	2·030 2·045	-·021 -·021	$2.009 \ 2.024$ 2.016	
10.	—70 23	174 50	S. N.	46 58·9 43 49·2 22 10	32 31		2·038 2·073	-·022 -·022	$2.016 \\ 2.051$ 2.033	Very unsteady.
11.	-71 15	171 15	N.S. S. N.	46 47·5 44 07·3	30 30	s. }	2·050 2·054	-·022 -·022	$2.028 \\ 2.032$ 2.030	Very unsteady.
-	—71 24	170 44	N.S. S. N. N.S.	22 03·5 46 49·9 44 08·6 21 53·6	45	$\left.\right\}$ s. by w. $\left.\right\}$	2·047 2·053	-·021 -·021	$\left[egin{matrix} 2 \cdot 026 \ 2 \cdot 032 \end{smallmatrix} ight] 2 \cdot 029$	

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
	−71 47 −72 07		S. N. S.	46 41·5 43 44·1 47 24·5	34 33 33	} w.s.w. {	2.057 2.078 2.011	- 011		Much motion. Ob- servations indif-
			N. N.S. S.	43 47·4 21 47·9 47 25·2	33 33 33	E. by N. $\frac{1}{2}$ N.	2·075 2·010	003	2.010]	servations indif- ferent.
	—71 55		N.S. N.	21 45·2 44 02			2.060	007 007	2.053	
16.	-72 12	172 13	S. N. N.S.	46 52·4 44 04 21 47·5	28	$\left \right\rangle$ s. by w. $\left\{ \right.$	2·044 2·058	-·019 -·019	2.025 2.039 2.032	
	-72 09		N. N.S.	44 26·7 21 36·5 46 30·1	30 31	E. {	2.033	007		Much motion.
	-72 57		N. N.S.	44 28·7 22 01·5		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			$2.056 \ 2.020$ 2.038	
19.	-72 35	173 34	S. N. N.S.	46 49·8 44 07·9 21 54·8	41	\right\} s.w. by w. {	1		$2.032 \ 2.039$ 2.035	
	-72 31	173 39	S. N. N.S.	46 53 43 51·8 21 50·1	34	$\int s. \text{ by } e. \frac{1}{2} e.$	2·044 2·070	018 018	$2.026 \ 2.052$ 2.039	
20.	-73 47	171 50	S. N. N.S.	46 31·9 43 56·3 21 37·7	34	s.e. {	2·067 2·066	014 014	$\left. egin{array}{c} 2 \cdot 053 \ 2 \cdot 052 \end{array} ight\} 2 \cdot 052$	
21.	-74 10	170 28	S. N.	46 50·7 43 41·8	30	s. by E.	2·046 2·080	019 019	$\left[egin{matrix} 2 \cdot 027 \ 2 \cdot 061 \end{smallmatrix} ight] 2 \cdot 044$	
	-74 0 6	171 20	N.S. S. N.	21 39 46 42 44 06	31	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2·056 2·056	004 004	$\left[egin{matrix} 2 \cdot 052 \\ 2 \cdot 052 \end{smallmatrix} \right] 2 \cdot 052$	
22.	-73 56	172 20	N.S. S. N.	22 08·6 46 57·7 44 00	32		2·041 2·062	017 017	$\left\{egin{array}{c} 2\!\cdot\!024 \ 2\!\cdot\!045 \end{array} ight\} 2\!\cdot\!035$	Very unsteady.
24.	-74 35	173 01	N.S. N. N.S.	21 52·2 44 07 21 27·8	29	S. by E.	2.055	017		
	-74 36 $-74 44$	1	S. N. N.S.	46 51·7 43 59 21 47	29		2·045 2·063	-·018 -·018	$ \begin{vmatrix} 2.027 \\ 2.045 \end{vmatrix}^{2.037} $	
zJ.	-/x 11	109 40	S. N.	46 48·6 44 05·7	30 30	E. {	2·048 2·056	-·007 -·007	$\left[egin{matrix} 2 \cdot 041 \ 2 \cdot 049 \end{smallmatrix} ight] 2 \cdot 045$	
27.	-75 22	168 48	N.S. S. N.	21 50·3 46 42 43 48·6	29 30 28	s.s.e. }	2·056 2·073	-·016 -·016	$\left[egin{array}{c} 2 \cdot 040 \\ 2 \cdot 057 \end{array} ight] 2 \cdot 048$	
	-76 06	168 11	N.S. S. N.	22 01 47 01·2 44 07·3	27 33	\	2·036 2·055	-·015 -·015	$\left\{egin{array}{c} 2 \cdot 026 \ 2 \cdot 040 \end{array} ight\} 2 \cdot 031$	
28.	_76 46	169 22	N.S. S. N.	21 44·4 46 59·9 44 03·7	37 37	E. {	2.037	008		Two points out of the meridian.
29	-77 47	7 175 43	N.S. S. N. N.S.	22 0·0 47 19·9 44 32·2 21 51·9	37 29 29 28	N. by w.		1	$\left[egin{array}{c} 2 \cdot 015 \ 2 \cdot 023 \end{array} ight] 2 \cdot 017$	

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 31.	$-\mathring{7}7$ $\acute{0}4$	188 1 8	S. N.	47 43.6 44 23.5		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1·989 2·036	001 001	2.035	
Feb. 1.	-77 04	188 30	N.S. S. N.	22 26.6 47 06.9 44 13.5			2·029 2·047	016 016	$egin{pmatrix} 2.013 \\ 2.031 \end{bmatrix} > 2.017$	
	-77 0 9	188 15	N.S. wt. 6 grs. wt. 1 gr.	22 14·8 30 45 4 42	30 31	S.E.	2.014			Ship's motion very considerable.
3.	-77 17	185 26	wt. $\frac{1}{2}$ gr. S. N.	2 27.6 46 59.9 44 02.6	$\frac{33}{34}$	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2·037 2·034	-·012 -·012	$\left. egin{array}{c} 2\!\cdot\!025 \ 2\!\cdot\!022 \end{array} ight\} 2\!\cdot\!023$	
4.	-77 00	192 18	N.S. S. N.	21 55·6 46 57·2 44 16·3			2·040 2·045	•006 •006	2.039	
5.	-77 10	192 48	N.S. S. N. S.	22 00·1 47 01·7 44 00 46 57·8	23 21 24	> E. by N. {	2·035 2·062 2·039	·006 ·006 ·007	2·056 \\ 2·030 \)	
0.	_77 14		N. N.S. S.	44 14·2 22 10 46 41·5	19 20	E. {	2.047	007	2.040 } 2.030	
			N. N.S.	44 33 22 07·8	19 18	$\left\{\right\}$ s. $\left\{\right\}$	2.027		$2.006 \int_{-\infty}^{\infty} 2.020$	
	-77 09		S. N. N.S.	47 07·7 44 06·6 21 58·9	28 24	} E.N.E. {	2.000	- 005	2·023 2·050 } 2·036	
	-76 58		S. N. N.S.	46 50·9 44 00·4 22 02·3	24		2·046 2·062	·019 ·019	$\left. egin{array}{c} 2 \cdot 027 \ 2 \cdot 043 \end{array} ight\} 2 \cdot 035$	
8.	-77 47	187 18	S. N. N.S.	47 03 44 23·2 22 03·4	34 33 32		2·034 2·038	·004 ·004	2·030 2·034	
			wt. 6 grs. wt. 3 grs. wt. 2 grs. wt. 1 gr.	30 30·9 14 14·6 9 15·6 6 15·1			2·023 2·071 2·124	·004 ·004 ·004	2.067	
10.	-77 39	187 06	wt. $\frac{1}{2}$ gr. wt. 6 grs. wt. 3 grs.	2 27·8 30 34·7 14 37	28		2.019	·019 ·019	2.000	
			wt. 2 grs. wt. 1 gr. wt. $\frac{1}{2}$ gr. S.	9 30·9 4 34·2 2 13·2 46 55·5		s. by E.	2·067 2·041	019 019		
11	-76 55	199 40	N. N.S. S.	44 13·9 21 55·9 46 47	29		1 :	019 019 002	2·028 2·022	
12.	-76 50	183 26	N.	44 13.2	25	s.e. by e. {	2.048	-·013	0.025	Much motion.
14.	—76 16	175 50	N.S. S. N.	21 47·5 46 55·1 44 33·7	24 34 33	s.s.w. {	2·042 2·026	·017 ·017	$2.025 \\ 2.009$ 2.017	
15.	-76 03	169 30	N.S. N.	22 09·9 44 08·5			2.053	 ·020	2·033 2·033	
	-76 20		N.S. S.	22 00·2 46 45·9	30	} s. {	2.051	0 12	2·039 \ _{2·041}	
			N. N.S.	44 08·4 22 09·6		s.s.e.	2.054	•012	2·042 } z·041	

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera- ture.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 19.	_7 ⁵ 03	168 44	s. N. N.s.	46 38·8 44 16·9 22 03·2	32	} s.w. {	2·059 2·044	011 011	2·048 2·033 } 2·040	
21.	-71 17	170 43	S. N.	46 55·7 44 07·7	32 30	$\left.\right\} \text{s.w.by w.} \frac{1}{2} \text{w.} \left\{\right.$	2·041 2·055	011		
1	-71 34	178 07	S. N. N.S.	47 04 44 28·2 22 12	27 26 26	\right\} w. {	2·033 2·032	-·007 -·007		
22.	-70 41	167 26	S. N.	47 01·4 43 48·5	24 24	N.N.E.	2·036 2·073		2·035 2·072	Much motion.
24.	-70 14	167 34	N.S. S. N.	22 01·3 46 43·4 44 09·6	26 25	$\left.\right\} \text{ s.s.w.} \frac{1}{2} \text{ w.} \left.\right\}$	2·055 2·052		2.037 2.034 2.036	
25.	-70 14	167 16	N.S. N. N.S.	22 12·1 44 35·3 21 41·1	22	$\left. \begin{array}{c} J \\ s. \end{array} \right. \left. \left\{ \begin{array}{c} I \\ I \end{array} \right. \right.$	2.024	020	2.004	Much motion.
27.		167 55	S. N.S.	46 46·5 21 59·9	30 29	$\left \begin{array}{c} \\ \end{array} \right $ s.e. $\left\{ \begin{array}{c} \\ \end{array} \right.$	2.050			Unsteady.
28.		167 48	N. N.S.	44 27·1 21 55·9	21	s. by E. {	2.033			
Mar. 1.		167 44 168 10	N. N.S. S.	44 31 21 56 46 50·3	24 22 27	\	2·029 2·048		2·027] 2·043 } 2·047	
			N. N.S.	44 07·8 22 20	26 28	N.w. by w. {	2.054	002	2.032	
3.	-67 5%	167 28	S. N. N.S.	46 43·4 44 17·5 22 27·9	14	} w. {	2.035	-·007 -·007	$2.048 \\ 2.037$ 2.043	
5.			N. N.S.	44 25·1 22 23·2	28 27	$\left \begin{array}{c} \\ \end{array} \right $ N. $\left\{ \begin{array}{c} \\ \end{array} \right.$		+.006		A good deal of motion.
7. 8.		162 14 162 34	S. S. N.	47 31·7 47 17·9 44 19·6	35 33	N.E. by N.	2.017	+·003 +·004 +·004	2.021 >2.024	
11.	-64 13	163 18	N.S. S. N.	22 09·6 47 29·3 44 33	31 30	N.w. by w.	2·005 2·027	+·002 +·002	$2.007 \ 2.029$ 2.018	,
12.	-63.57	161 11	N.S. S. N.	22 29·8 47 06·8 44 25·4	31 30	$\left.\right\}$ s. by w. $\left.\right\}$	2·029 2·035	-·022 -·022	$\left[egin{matrix} 2 \cdot 007 \\ 2 \cdot 013 \end{matrix} \right] 2 \cdot 010$	
14.	-62 41	156 59	N.S. S. N.	21 59 47 13 44 16·7		w . {	2·023 2·045	012 012	$2.011\ 2.033$ 2.022	
15.	-63 50	156 06	N.S. S. N.	21 49·7 47 02·7 44 22·3	33	$\left \begin{array}{c} \\ \\ \\ \end{array} \right \text{s.} \frac{1}{2} \text{ w.} \left\{ \right.$	2·034 2·039	024 024	$egin{array}{c} 2 \cdot 010 \ 2 \cdot 015 \ \end{array} \Big\} \ 2 \cdot 013$	
16.	-64 13	154 03	N.S. S. N.	21 40·8 47 04·3 44 31	1	}	2·033 2·029	-·020 -·020	$2.013 \ 2.009$ 2.011	
17.	-64 20	153 02	N.S. S. N.	22 10·1 46 50·1 44 03·6	26	s.w. by s.	1	020	$egin{array}{c} 2 \cdot 027 \ 2 \cdot 038 \ \end{array} iggr\} \ 2 \cdot 032$	
18.	-63 54	151 56	N.S. N.	22 09·2 44 32	29		2.028	005	2.023	A heavy head swell.
19.	-64 26	148 20	N.S. S. N. N.S.	22 42 46 23·5 43 29·9 22 01		s.w. by s.	2·078 2·092	020 020	$\left\{ \begin{array}{c} 2.058 \\ 2.072 \end{array} \right\} 2.065$	

· INCOMESSATION ADDRESS OF THE	SECURITIES AND ADDRESS OF THE PERSON NAMED IN COLUMN 1									
1841.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera-	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 20.	-6510	143 21	S. N.	46 45·7 43 54·1	21	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2·051 2·068	012 012	2.056	Along the edge of the pack.
21.	-64 20	140 40	N.S. S. N.	22 16·5 45 55·9 43 41	22 21	\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \	2·106 2·081	-·004 -·004		
22.	—63 09	139 28	N.S. wt. 5 grs. wt. 4 grs. wt. 3 grs. wt. 3 grs. wt. 2 grs. S. N.	21 29·5 25 11·2 19 34·1 14 18·6 14 13 9 39 46 53·9 44 21·6	34 34		2.045 2.062 2.074 2.040 2.043	002 002 002 002 002 002 002	2.043 2.060 2.072 2.040 2.041	
23.	-62 13	136 20	N.S. S. N.	22 00·2 47 16·5 44 14·5	34			-·000 -·000	2·019∫	
24.	-61 20	134 05	N.S. S. N. N.S.	21 36·6 46 47·2 43 50·1 21 56	35 35 35	1 1 1	2·050 2·072	-·000 -·000	2.050	
25.	60 19	131 20	S. N. N.S.	46 41·1 43 42·6 21 58	38 37 36		2.079	+·003 +·003	2.081 \ 2.071	
	-58 00		S. N. N.S.	46 59·2 43 58 22 01·1	35 34 34) N.N.W.	2.004	T 009	•	
	55 00		s. N. N.s.	47 34·3 44 26·7 22 20·5	40 38 38		2.033	+·003 +·007	2.040	Very unsteady.
	54 58	132 50	S. N. S. N. N.S.	47 30 44 43·5 47 31·7 44 44·4 22 33·8	40 40 39 39 39	N.E. by N.	2·016 2·002	+ ·007 + ·007 + ·007 + ·007	$2.023 \ 2.009 \ 2.027$	Deflecting needle had a fall; repeated the observations to find if any effect was produced.
31.	-54 00	132 02	S. N. N.S.	46 56·3 44 09·5 21 37·6	40 40 40	1 1		+.006		
April 1.	-53 13	135 18	S. N. N.S.	46 55·4 44 41·5 22 29·7	43 40 39		2.017	+·012 +·012 +·012	2.029	
			wt. 6 grs. wt. 5 grs. wt. 4 grs. wt. 3 grs. wt. 2 grs.	31 08·5 25 28·5 19 39·7 14 07·7 9 26·2	40 40 40 40 40 40		1.990 2.035 2.086	$ \begin{array}{c} + 012 \\ + 012 \\ + 012 \\ + 012 \\ + 012 \end{array} $	2·002 2·047 2·098	,
2.	-51 16	136 50	wt. 1 gr. S. N. N.S.	5 10·2 47 16 44 23·8 22 18·5	40 43 41 39		2·020 2·036	+·013 +·013	$2.033 \ 2.049$ 2.041	
	-48 24 $-46 55$		N. N.S. N.	45 01·5 22 56·3 46 33·4	43 44 45	N.E.	••••		•••••	Much motion and rolling deep. A heavy sea.
	-46 29		S. N. N.S.	48 37·8 45 50·1 23 03	44 44 44			+·015 +·015	1.942] 1.040	A heavy sea running.

1841.	Lat.	Long.	Method employed.	Angle of deflection.		Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
5.	-46 22 $-45 02$ $-43 41$	143 10	S. N. N.S. S. N. N.S. S. N. S. N. S. Wt. 6 grs. wt. 4 grs. wt. 2 grs. wt. 1 gr.	48 31·5 45 40·2 23 00·9 48 46·2 46 15 22 05·9 48 49·8 46 25·1 50 01·4 46 39·8 23 16·8 32 58·5 26 29·7 21 21 15 59·4 10 27·2 5 14·2	45 46 47 47 50 48 60 60 59 58 59 59 59	N.E. by E. $\left\{\begin{array}{c} \\ \\ \\ \\ \end{array}\right\}$ N.E. by E. $\left\{\begin{array}{c} \\ \\ \\ \\ \end{array}\right\}$ N.E. $\frac{1}{2}$ E. $\left\{\begin{array}{c} \\ \\ \\ \end{array}\right\}$	1.917 1.913 1.912 1.901 1.820 1.884 1.887 1.919 1.881 1.850 1.885	+·012 +·013 +·013 +·018 +·018 +·018 +·018 +·018	1.929 1.925 1.925 1.914 1.838 1.902 1.905 1.937 1.899 1.868 1.903	{ Running along the land.

Observations of Declination made on board Her Majesty's Ship Terror, between November 15, 1840, and April 5, 1841.

The Observers are distinguished by their Initials as follows:—C. Captain Crozier; P. Lieut. Phillips; Cr. Mr. Cotter, Master.

1840.	Position.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at-	Corrected Declination.	Correction for True Declinindex nation.
	Lat. Long.	g				traction.		error.
16.	. — 44 24 152 58 — 44 24 152 58 — 46 05 154 18 — 46 11 154 18 — 46 24 154 50 . — 49 06 160 10 — 49 14 160 06 — 49 14 160 52 Auckland Island	CR. CR. CR. CR. CR. CR. CR.	$ \begin{array}{r rrrr} -9 & 36 \\ -10 & 52 \\ -12 & 57 \\ -9 & 48 \\ -9 & 48 \\ -11 & 12 \\ -11 & 54 \\ -9 & 39 \end{array} $	s.e. by E. s.e. by E. s.e. s.e. s.e. s.e. by E. s.e. by E. $\frac{1}{2}$ E.	├-73 00	-4 44 -4 09 -4 09 -4 09 -4 09 -5 20 -5 20 -5 20 -5 20		Compass R. of CUMMINS, index error ascertained at Hobarton, June 1841.
Dec. 6.	-50 33 166 15 At anchor.		-21 12 -22 48 -12 11 -21 59 -21 47 -20 32 -19 32 -19 47 -20 14 -19 23 -22 09 -21 28 -20 29 -23 00 -22 05 -21 59 -22 36 -21 40 -20 54 -21 50 -24 23 -20 29 -19 39 -21 02 -21 19 -22 12 -21 49 -21 52 -23 29 -12 41 -13 20 -13 18 -13 18 -13 21 -15 34	w. by N. N.E. by N. N.N.E. E.S.E. S.E. by E. N.E.	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	+5 09 +5 09 +5 09 +5 09 +4 29 +5 07 +4 29 +5 40 +5 32 42 40 +5 35 42 29 +5 35 42 29 +3 29 +3 20 53 35 46 35 -5 36 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35 -3 55 46 35	-16 01 -16 03 -18 21 -17 18 -16 50 -17 18 -15 03 -14 25 -14 40 -15 45 -15 37 -16 34 -16 59 -15 41 -17 11 -16 46 -16 30 -16 17 -16 43 -18 48 -15 51 -16 25 -16 43 -18 48 -15 55 -16 12 -17 05 -16 14 -16 17 -17 40 -16 27 -16 17 -17 40 -16 27 -16 17 -17 40 -16 27 -17 18 54 -18 54 -18 54 -18 54 -18 54 -18 54 -19 03 -17 06	+1 23 -15 29 Compass B. of Commins, index erro

1840.	Posit	tion.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
Dec. 12.			C. C.	-1402	s.e. by e. s.e. by e.	$-\mathring{7}3 00$	$-\overset{\circ}{5} \overset{\circ}{06} \\ -5 \ 22$	-19 08 -18 45	0 /	o /	
13. 16.	-52 30 -52 34 -52 34 -52 34	169 50 169 50 169 50 169 50	C. Cr. Cr. Cr.	$ \begin{array}{r rrr} -13 & 23 \\ -12 & 57 \\ -22 & 21 \\ -21 & 49 \\ -22 & 50 \end{array} $	s.e. by e. w. by s. w.s.w.	├ ├ -73 53	$ \begin{array}{rrrr} -5 & 22 \\ +6 & 08 \\ +5 & 50 \\ +5 & 50 \end{array} $	$ \begin{vmatrix} -18 & 19 \\ -16 & 13 \\ -15 & 59 \\ -17 & 00 \end{vmatrix} $ $ -18 & 31$	+1 23	-17 08	
17.	-52 34 -52 34 -52 34	169 50	CR. CR. CR.	$ \begin{array}{r rrrr} -23 & 01 \\ -23 & 10 \\ -19 & 55 \\ -12 & 59 \end{array} $	s.w. by w. s.w. by w.	75 55	$ \begin{array}{r} +5 & 21 \\ +5 & 21 \\ +4 & 38 \\ -5 & 50 \end{array} $	$ \begin{array}{c cccc} -17 & 40 \\ -17 & 49 \\ -15 & 15 \\ -18 & 49 \end{array} $			
20. 21.	$-57 33 \\ -57 33$	168 54 170 30 170 30	CR. CR. C. C. C.	$ \begin{vmatrix} -12 & 53 \\ -14 & 11 \\ -21 & 54 \\ -21 & 06 \\ -20 & 28 \end{vmatrix} $	E.S.E. S.S.E. S.S.E. S. by E.	$\begin{array}{c} -76 \ 30 \\ -77 \ 10 \end{array}$	$ \begin{array}{r rrrr} -5 & 50 \\ -2 & 58 \\ -3 & 06 \\ -3 & 06 \\ -1 & 36 \end{array} $	$egin{pmatrix} -18 & 43 \ -17 & 09 \ -25 & 00 \ -24 & 12 \ -22 & 04 \ \end{bmatrix}$	magazatika a pazazikina poston promoto promoto poston post		
22.	-57 33 -57 33 -58 54 -58 54 -58 54	170 30 171 02 171 02	C. Cr. C. C.	$ \begin{array}{r rrrr} -23 & 45 \\ -25 & 00 \end{array} $	s. by E. s. by E. s. by E. ½ E. s.s.e.		$ \begin{array}{r rrr} -1 & 36 \\ -1 & 44 \\ -2 & 36 \\ -3 & 23 \\ \end{array} $	$ \begin{vmatrix} -22 & 04 \\ -25 & 21 \\ -26 & 44 \\ -23 & 17 \\ -24 & 04 \end{vmatrix} -23 & 21$	+1 23	-21 58	
	$ \begin{array}{rrrr} -58 & 54 \\ -59 & 04 \\ -59 & 04 \\ -59 & 09 \end{array} $	171 02 171 00 171 00	Cr. C. C.	$ \begin{array}{rrrr} -20 & 21 \\ -26 & 54 \\ -25 & 15 \\ -26 & 34 \end{array} $	S.S.E. S.S.W. S.S.W.	-78 10	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$egin{bmatrix} -23 & 44 \ -23 & 31 \ -23 & 52 \ -23 & 11 \ \end{bmatrix}$			
23.	-59 32 -59 32 -59 32	170 05 170 05 170 05	Cr. Cr. Cr.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.w. $\frac{1}{2}$ w. s.e. by e. s.e. by s.		$ \begin{array}{r} +4 & 17 \\ -6 & 23 \\ -7 & 23 \\ -5 & 03 \end{array} $	$ \begin{array}{c cccc} -19 & 48 \\ -23 & 47 \\ -24 & 01 \\ -23 & 05 \\ 24 & 22 \end{array} $			
	-59 32	170 05 170 05 170 05	CR. CR. CR. CR.	$ \begin{array}{rrrrr} -21 & 02 \\ -23 & 36 \\ -24 & 03 \\ -26 & 39 \\ -26 & 52 \end{array} $	s.s.e. s. by w. s.s.w.	├ -78 30	$ \begin{array}{c cccc} -3 & 31 \\ 0 & 0 \\ +1 & 48 \\ +3 & 31 \\ +5 & 02 \end{array} $	$ \begin{vmatrix} -24 & 33 \\ -23 & 36 \\ -22 & 15 \\ -23 & 08 \\ -21 & 49 \end{vmatrix} $ -22 19	+1 23	20 56	
	-59 32 $-59 32$ $-59 32$		CR. CR. CR. CR.	$ \begin{array}{c cccc} -20 & 52 \\ -28 & 17 \\ -29 & 01 \\ -28 & 11 \\ -28 & 10 \end{array} $	s.w. by s. s.w. s.w. by w. w. by n. w.n.w.		$\begin{vmatrix} +5 & 03 \\ +6 & 23 \\ +7 & 23 \\ +8 & 11 \\ +7 & 36 \end{vmatrix}$	$ \begin{array}{c cccc} -21 & 49 \\ -21 & 54 \\ -21 & 38 \\ -20 & 00 \\ -20 & 34 \end{array} $	-		
23.	-59 32 $-59 32$ $-59 32$	170 05	CR. CR. CR.	$ \begin{vmatrix} -27 & 50 \\ -26 & 47 \\ -25 & 49 \end{vmatrix} $	n.w. by w. n.w. n.w. by n. n. by w.	70.00	$\begin{vmatrix} +6 & 45 \\ +5 & 41 \\ +4 & 26 \\ +1 & 33 \end{vmatrix}$	$ \begin{array}{c cccc} -21 & 05 \\ -21 & 06 \\ -21 & 23 \\ 22 & 22 \end{array} $	1 1 00	20, 20	
	-59 32 $-59 32$	170 05 170 05 170 05 170 05	CR. CR. CR.	$ \begin{array}{c cccc} -21 & 34 \\ -20 & 17 \\ -18 & 32 \end{array} $	N. N. by E. N.N.E. N.E. by N.	\right\}-78 30	$ \begin{vmatrix} 0 & 0 \\ -1 & 33 \\ -3 & 02 \\ -4 & 26 \end{vmatrix} $	$\begin{bmatrix} -21 & 34 \\ -21 & 50 \\ -21 & 34 \\ -22 & 48 \end{bmatrix}$	+1 20	-20 20	
24.	$ \begin{array}{rrr} -59 & 37 \\ -59 & 37 \\ -60 & 17 \\ -60 & 17 \end{array} $	169 17 169 17 170 12 170 12	C. C. C.	$ \begin{array}{rrrr} -14 & 38 \\ -15 & 17 \\ -25 & 59 \\ -23 & 38 \end{array} $	S.S.E. $\frac{3}{4}$ E. S.S.E. $\frac{3}{4}$ E. S.		$ \begin{bmatrix} -4 & 53 \\ -4 & 53 \\ 0 & 0 \\ -3 & 41 \end{bmatrix} $	$ \begin{array}{c cccc} -19 & 31 \\ -20 & 10 \\ -25 & 59 \\ -27 & 19 \end{array} $			
THE PROPERTY OF THE PROPERTY O		170 12 170 12 170 12 170 34 170 34	C. C. Cr.		s.e. by s. s.s.e. s.e. ½ s. s.e.	├ -79 00	$ \begin{array}{r rrrr} -5 & 17 \\ -3 & 41 \\ -6 & 00 \\ -6 & 41 \\ -6 & 41 \end{array} $	$ \begin{vmatrix} -27 & 42 \\ -27 & 32 \\ -28 & 00 \\ -25 & 00 \\ 24 & 39 \end{vmatrix} -25 & 11$	+1 23	-23 48	
	$\begin{bmatrix} -60 & 35 \\ -60 & 35 \end{bmatrix}$	170 34 170 34 170 34 170 34	CR.	$ \begin{array}{r rrrr} -17 & 57 \\ -21 & 50 \\ -21 & 14 \\ -20 & 40 \end{array} $	s.e. s.s.e. s.s.e. s.e. by s.		$ \begin{vmatrix} -6 & 41 \\ -3 & 41 \\ -3 & 41 \\ -5 & 17 \end{vmatrix} $	$\begin{bmatrix} -24 & 38 \\ -25 & 31 \\ -24 & 55 \\ -25 & 57 \end{bmatrix}$			

1840.	Posi	l	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's at-	Corrected Declination.	index	True De	Remarks.
	Lat.	Long.	0				traction.		error.		<u> </u>
Dec. 29.	-64 11		Cr.	$\begin{vmatrix} -\mathring{27} & 44 \\ -24 & 39 \end{vmatrix}$	s. ½ E. s. by E.		- 1 08 - 2 16	$ \begin{array}{cccc} -28 & 52 \\ -26 & 55 \end{array} $	0 /	۰	•
30.	-64 11 $-64 26$		CR.	$ \begin{array}{r rrr} -25 & 09 \\ -34 & 58 \end{array} $	s. by E.		$\begin{bmatrix} - & 2 & 16 \\ + & 8 & 23 \end{bmatrix}$	$ \begin{array}{c cccc} -27 & 25 \\ -26 & 35 \end{array} $,	
1	-64 26 $-64 26$		C. C.	$\begin{vmatrix} -34 & 22 \\ -35 & 07 \end{vmatrix}$	S.W. S.W. ½ S.	├ —81 15	$\begin{vmatrix} + & 8 & 23 \\ + & 7 & 30 \end{vmatrix}$	-25 59 > -27 15 -27 37 > -27 15	+1 23	-25 5	2
	$-64 26 \\ -64 48$	173 15	C. Cr.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.w. s. by E.		$\begin{vmatrix} + & 4 & 34 \\ - & 2 & 16 \end{vmatrix}$	$ \begin{array}{c c} -28 & 20 \\ -27 & 31 \end{array} $			
9.1	$-64 \ 48$	172 56	Cr.	-34 20	s.w.	J	+ 8 23	$-25\ 57$			
31.	$ \begin{array}{rrr} -65 & 42 \\ -65 & 42 \end{array} $	172 13	C.		s. ½ E. s. by E.		$\begin{bmatrix} - & 1 & 10 \\ - & 2 & 24 \end{bmatrix}$	$ \begin{array}{c c} -27 & 19 \\ -28 & 37 \end{array} $			
	-65 42 -65 42		C. Cr.	$\begin{vmatrix} -25 & 23 \\ -26 & 26 \end{vmatrix}$	s. by E. s. by E.	}−82 00	$\begin{vmatrix} - & 2 & 24 \\ - & 2 & 24 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	26 1	7
	-6542	172 13	CR.	-26 18	s. by E.		- 2 24	-28 42	1 20		
	-65 42 -65 42		CR.		s. by E. s. by E.		$\begin{vmatrix} - & 2 & 24 \\ - & 2 & 24 \end{vmatrix}$	$ \begin{array}{c c} -25 & 58 \\ -26 & 35 \end{array} $	-	AND ADDRESS OF THE PROPERTY OF	
1841. Jan. 2.	-66 24		c.		E. by s. ½ s.	<u> </u>	-11 57	-29 11)			
	-65 15	172 40	Cr.	-19 54	S.E.		- 9 09	-29 03			
	$-65 \ 15$ $-65 \ 27$		Cr.	$\begin{vmatrix} -20 & 48 \\ -21 & 14 \end{vmatrix}$	s.e. e. by s. ½ s.		$\begin{bmatrix} -9 & 09 \\ -11 & 57 \end{bmatrix}$	$ \begin{array}{c c} -29 & 57 \\ -33 & 11 \end{array} $			
	-65 27	173 20	C.	-21 00	E. by s. $\frac{1}{2}$ s.		-11 57	$-32\ 57$			
	-65 27 $-65 27$		C.	$\begin{vmatrix} -17 & 49 \\ -19 & 17 \end{vmatrix}$	E. $\frac{1}{2}$ S. E. by S. $\frac{1}{2}$ S.	>-82~00	$\begin{bmatrix} -12 & 13 \\ -11 & 57 \end{bmatrix}$	$\begin{array}{c c} -30 & 02 \\ -31 & 14 \end{array} -30 \ 40$	+1 23	-29 1	7
-	$-65 \ 30$	173 30	C.		E. by s. $\frac{1}{2}$ s.		-11 57 $-11 44$	$ \begin{array}{c cccc} -32 & 01 \\ -32 & 55 \end{array} $			
*	$ \begin{array}{c c} -65 & 30 \\ -65 & 31 \end{array} $		C.	$\begin{bmatrix} -21 & 11 \\ -22 & 19 \end{bmatrix}$	E.S.E. S.E. by E.		$\begin{bmatrix} -11 & 44 \\ -10 & 38 \end{bmatrix}$	$-32\ 57$			1
	$ \begin{array}{rrr} -65 & 32 \\ -65 & 32 \end{array} $		C. C.	$\begin{vmatrix} -21 & 48 \\ -25 & 56 \end{vmatrix}$	S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.		$\begin{bmatrix} -9 & 53 \\ -6 & 07 \end{bmatrix}$	$\begin{bmatrix} -31 & 41 \\ -32 & 03 \end{bmatrix}$			io Index error ascertained at Hobarton, June 1841.
,	-65 32	173 50	C.	$-22 \ 38$	s.e. by E. ½ E.	1	-10 34	$-33 \ 12$			2, Jur
	-65 35 $-65 35$		C.	$ \begin{array}{r rrr} -26 & 59 \\ -26 & 54 \end{array} $	s.s.e. s. by e.		$\begin{vmatrix} - & 4 & 41 \\ - & 2 & 18 \end{vmatrix}$	$ \begin{array}{c cccc} -31 & 40 \\ -29 & 12 \end{array} $			barto
	$-65 \ 35$	173 52	C.	-25 22	S.S.E. ½ E.	·	- 5 45	-31 07			at Ho
	$-65 ext{ } 35 \ -65 ext{ } 27$	173 52 173 20	C. P.	$ \begin{array}{r rrr} -25 & 54 \\ -23 & 56 \end{array} $	s.s.e. e. by s. ½ s.	$-81 \ 30$	$\begin{vmatrix} -4 & 40 \\ -11 & 16 \end{vmatrix}$	$\begin{bmatrix} -30 & 34 \\ -35 & 12 \end{bmatrix}$. 1 09	<i>a</i> n 4	ined
	$-65 \ 35 \\ -65 \ 28$	173 52	P. Cr.	$ \begin{array}{r rrrr} -22 & 34 \\ -18 & 25 \end{array} $	s.e. by e. e. by s.	Z-81 30	$\begin{vmatrix} -10 & 02 \\ -11 & 25 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	-29 4	scerta
	-6528	173 20	Cr.	-17 29	E.S.E.		-11 04	-28 33			rror a
	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		CR.	$\begin{vmatrix} -18 & 27 \\ -20 & 09 \end{vmatrix}$	E.S.E.		$\begin{vmatrix} -11 & 04 \\ -11 & 04 \end{vmatrix}$	$ \begin{array}{c cccc} -29 & 31 \\ -31 & 13 \end{array} $			dex e
5.	-66 15	173 32	Cr.	$-25 \ 37$	S.S.E.	J	_ 4 41	$-30 \ 18$			11.
6.	$-68 07 \\ -68 07$		CR.	$\begin{bmatrix} -30 & 21 \\ -30 & 28 \end{bmatrix}$	S.S.E. S.S.E.		$\begin{bmatrix} -5 & 57 \\ -5 & 57 \end{bmatrix}$	$\begin{bmatrix} -36 & 18 \\ -36 & 25 \end{bmatrix}$			v used
7.	$-68 \ 30$	175 30	Cr.	$\begin{bmatrix} -24 & 25 \\ 22 & 26 \end{bmatrix}$	s.e. by e.		-12 58	-37 43			won si
	-68 30 $-68 30$		Cr.	$\begin{vmatrix} -23 & 36 \\ -23 & 42 \end{vmatrix}$	s.e. by e.	02 20	-1258 -1100	$\begin{bmatrix} -36 & 34 \\ -34 & 42 \end{bmatrix}$	1 09	24 2	P, wa
	$-68 \ 30$ $-68 \ 30$	175 30	Cr.	$\begin{vmatrix} -23 & 12 \\ -47 & 46 \end{vmatrix}$	E.S.E. s.w. by w.	$-83 \ 30$	$\begin{vmatrix} -14 & 09 \\ +12 & 58 \end{vmatrix}$	$-37 \ 21 \ -34 \ 48$	+1 23	04 0	urked
8.	-68 26	176 32	C.	-22 19	s.e. by e.		-12 58	-35 17			s, ma
	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	176 32 176 32	C. C.	$\begin{bmatrix} -20 & 36 \\ -20 & 59 \end{bmatrix}$	s. 73° e. s. 85° e.		$\begin{bmatrix} -14 & 30 \\ -14 & 56 \end{bmatrix}$	$\begin{bmatrix} -35 & 06 \\ -35 & 55 \end{bmatrix}$			MMIN
11.	-70 53	173 00	C.	$-45 \ 31$	S. $\frac{1}{4}$ E.	ĺ	- 1 10	$-46\ 41$			of Cun
	-70 53 $-70 53$		C.	$\begin{bmatrix} -48 & 51 \\ -43 & 10 \end{bmatrix}$	s. by w.		$\begin{bmatrix} + & 4 & 43 \\ 0 & 0 \end{bmatrix}$	$\begin{bmatrix} -44 & 08 \\ -43 & 10 \end{bmatrix}$			card c
	-70 53 $-70 53$	173 00	Cr.	$\begin{vmatrix} -43 & 22 \\ -44 & 57 \end{vmatrix}$	s.	>-85 50	0 0	-43 22	+1 03	45_4	Gr & & & & & & & & & & & & & & & & & & &
	-70 55	1/9 00	CR.	-11 0/	s.	00 00 –	0 0	-TT 0/ >-40 TO	LI OO	- TU 1	1

1841.	Position. Lat. Long.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Decli- nation.	Remarks.
Jan. 11.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. C. C.	- 49 10 - 51 03 - 53 04 - 54 21 - 54 32 - 53 11	s. ½ w. s. by w. s. by w. s. by w. s. by w.	$\rightarrow -8550$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} -51 & 03 \\ -48 & 21 \\ -49 & 38 \end{vmatrix} $	+ 1 03	_ 45 45	A light card of CUMMINS, marked
		C. C. CR. CR. CR.	- 51 22 - 51 33 - 50 08 - 52 01 - 53 19 - 53 18 - 53 00 - 50 53	s. by w.	-86 00	$\begin{array}{c} 0 & 0 \\ + & 4 & 56 \\ + & 4 & 56 \\ + & 4 & 56 \\ + & 4 & 56 \\ + & 4 & 56 \\ + & 4 & 56 \end{array}$	$\begin{vmatrix} -51 & 22 \\ -46 & 37 \\ -45 & 12 \\ -47 & 05 \\ -48 & 23 \\ -48 & 22 \\ -48 & 04 \end{vmatrix} -47 & 55$	+1 03	— 46 52	ns, marked P, was now used.
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. C	- 57 58 - 53 25 - 27 35 - 52 46 - 54 17	s.w. by s. s. by w. ½ w. E. by s. ½ s. s.s.w. s. by w. s. by w. s. by s. E. by s. s.s.w. s. s.y. s. s.y.	\right	$ \begin{array}{r} +14 & 14 \\ + & 7 & 22 \\ -24 & 22 \\ + & 9 & 48 \\ + & 9 & 48 \end{array} $	- 43 44 - 48 03 - 51 57 - 42 58 - 44 29 - 48 10 - 48 15 - 50 10 - 51 54 - 48 23	+1 03	— 46 40	Index error
	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C. C	- 35 06 - 35 46 - 35 00 - 35 00 - 34 37 - 34 19 - 64 55 - 64 17 - 65 46 - 62 42 - 64 56	s.e. by e. s.e. $\frac{1}{2}$ e. s.e. by e. s.e. by e. s.e. by e. s.e. by s. s.w. by s. s.w. by s. s.w. by s.	\{\}-86 00	-21 21 -19 44 -21 21 -21 21 -21 21 -21 21 +14 14 +14 14 +14 14 +12 00 +14 14	$ \begin{vmatrix} -56 & 27 \\ -55 & 30 \\ -56 & 21 \\ -56 & 21 \\ -55 & 58 \\ -55 & 40 \\ -50 & 41 \\ -50 & 03 \\ -51 & 32 \\ -50 & 42 \end{vmatrix} $	+1 03	— 52 35	
19.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C. C. C. Cr. Cr. Cr.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	s.w. ½ s. s.w. s.w. ½ s. s.w. ½ s. s.w. ½ s. s.w. 5.w. ½ s.	-86 10	$\begin{vmatrix} +16 & 53 \\ +18 & 55 \\ -18 & 55 \\ +16 & 50 \\ +18 & 55 \\ +16 & 53 \\ +18 & 55 \\ +16 & 53 \end{vmatrix}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	– 48 49	
22.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. Cr. Cr. Cr. Cr. Cr. Cr.	- 44 51 - 44 23 - 43 53 - 45 36 - 49 19 - 54 17 - 53 18 - 48 34 - 34 19	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. S.S.E. S. by E. S. S. S. S.E. S. S.E.	_86 10	$ \begin{array}{c cccc} -10 & 12 \\ -10 & 12 \\ -5 & 08 \\ 0 & 0 \\ 0 & 0 \\ -10 & 12 \\ -32 & 26 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	— 54 34	
	$ \begin{array}{c ccccc} -73 & 51 & 171 & 50 \\ -73 & 52 & 170 & 40 \\ -73 & 44 & 171 & 03 \end{array} $	C. P. Cr.	44 12	E. by s. $\frac{1}{4}$ s. N.E. $\frac{1}{2}$ E. N.E. by N.	\ -86 50	-24 30	$ \begin{array}{c cccc} - & 67 & 44 \\ - & 68 & 42 \\ - & 58 & 04 \end{array} $ $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	- 65 41	

1841.	Position.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's at-	Corrected Declination.	Correction for index	True Declination.	Remarks.
·	Lat. Long.	sqo	observed.	sinp s nead.		traction.		error.	nation.	Ren
Jan. 22.	$ \begin{vmatrix} -\mathring{7}3 & 46 & 1\mathring{7}1 & 25 \\ -73 & 46 & 171 & 25 \\ -73 & 46 & 171 & 25 \\ -73 & 46 & 171 & 25 \\ -73 & 46 & 171 & 25 \end{vmatrix} $	Cr. Cr.	- 36 51 - 36 16	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N. E.N.E. E.N.E. E. by N.	>-86 50	$ \begin{vmatrix} -24 & 30 \\ -29 & 58 \\ -29 & 58 \\ -32 & 03 \end{vmatrix} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	-6541	
	$ \begin{bmatrix} -73 & 46 & 171 & 25 \\ -73 & 46 & 171 & 35 \\ -73 & 46 & 171 & 35 \\ -73 & 46 & 171 & 35 \\ -73 & 46 & 171 & 35 \\ -73 & 59 & 171 & 40 \\ -73 & 59 & 171 & 40 \\ -74 & 03 & 171 & 40 \end{bmatrix} $	CR. CR. CR. CR. C.	- 36 14 - 36 12 - 36 50	E. by N. E. E. E. S. S.	-86 40	$\begin{vmatrix} -31 & 04 \\ -31 & 04 \\ -31 & 04 \end{vmatrix}$	$\begin{vmatrix} -67 & 16 \\ -67 & 54 \\ -66 & 23 \\ -62 & 48 \\ -63 & 52 \end{vmatrix} -65 = 15$	+1 03	3— 64 ₋ 12	
		C. C. C. Cr. Cr.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. E. by s. E. by s. S. E. by s.		-27 31	$ \begin{vmatrix} -63 & 47 \\ -68 & 04 \\ -68 & 18 \\ -66 & 18 \\ -62 & 02 \\ -65 & 33 \end{vmatrix} $	+1 03	65 04	
25.	$egin{array}{cccccccccccccccccccccccccccccccccccc$	Cr. Cr. Cr. Cr. Cr.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.W. S.S.W. E.S.E. E.S.E.		+13 46 $-34 13$ $-34 13$ $-34 13$	$ullet - 67 \ 27 \ - 66 \ 38 \ - 73 \ 41 \ - 69 \ 48$	+1 08	8 - 68 40	
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. CR C. C. C. C. CR C. CR	$ \begin{array}{rrrrr} -102 & 27 \\ -33 & 53 \\ -53 & 33 \\ -56 & 14 \\ -60 & 19 \\ -55 & 50 \end{array} $	s. by w. E. ½ S. E.S.E. E.S.E. E.S.E.		$ \begin{array}{rrrr} -47 & 08 \\ -36 & 33 \\ -36 & 33 \\ -36 & 33 \end{array} $	-9652	7 +1 08	3 — 9 0 44	
28.	-75 40 168 28 -75 58 168 56 -75 58 168 56 -76 47 169 26 -76 47 169 26 -77 17 171 38 -77 22 172 00	CR C. C. C. C. C. C. C.		E.S.E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. E. $\frac{3}{4}$ S. E. by S. E. $\frac{1}{2}$ S.		-36 38 -28 16 -28 16 -36 36 -36 38 -34 48	$egin{array}{cccc} 8 & -95 & 12 \ -100 & 22 \ -101 & 27 \ \end{array} egin{array}{cccc} -100 & 44 \ -108 & 53 \ -107 & 23 \ \end{array} egin{array}{cccc} -108 & 08 \ -116 & 13 \ \end{array} egin{array}{cccc} -108 & 08 \ \end{array} \end{array}$	+1 05	3 - 9941 $3 - 10705$	
29.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. C. C. P. P. C.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{3}{4}$ W. N. $\frac{1}{4}$ W. N. by E. N. by E.	87 00	$ \begin{array}{c cccc} + & 4 & 46 \\ + & 1 & 35 \\ - & 6 & 21 \\ - & 6 & 21 \\ 0 & 0 \end{array} $	$\begin{bmatrix} -115 & 12 \\ -115 & 11 \end{bmatrix}$ $\begin{bmatrix} -105 & 00 \\ -100 & 25 \\ -100 & 48 \end{bmatrix}$ $\begin{bmatrix} -103 & 19 \\ -103 & 19 \end{bmatrix}$		B - 114 21 B - 102 09	
	$egin{array}{cccccccccccccccccccccccccccccccccccc$	C. CR C. C. B C. C.	$egin{array}{c} -123 & 50 \\ -110 & 43 \\ -65 & 19 \\ -64 & 40 \\ -76 & 06 \\ -74 & 36 \\ -77 & 11 \\ \end{array}$	N. by w. N.E. N.E. S.E. by S. S.E. by S.	-86 00	$ \begin{array}{r} + 6 & 21 \\ -17 & 26 \\ -17 & 26 \\ -14 & 14 \\ -14 & 14 \end{array} $	$ \begin{vmatrix} -105 & 27 \\ -104 & 22 \end{vmatrix} $ $ \begin{vmatrix} 6 & 82 & 45 \\ 6 & 82 & 06 \end{vmatrix} $ $ \begin{vmatrix} 4 & 90 & 20 \\ 4 & 88 & 50 \\ 8 & 86 & 59 \end{vmatrix} $ $ \begin{vmatrix} -86 & 19 \\ 8 & 86 & 59 \end{vmatrix} $	2 +- 1 0:	3 — 85 09	
2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 C. 3 C. 3 C.	- 74 47 - 75 23 - 76 56 - 77 48	s. 62° E. s.e. by E. s.e. by E.	\rightarrow -85 50	$ \begin{vmatrix} -21 & 00 \\ -20 & 29 \\ -20 & 29 \end{vmatrix} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4 +1 0	3 - 95 21	

1841.	Position. Lat. Long.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
Feb. 2.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	P. C.	-7456 -7457	s.e. by e.	>-85 50	$ \begin{array}{r rrr} -23 & 22 \\ -18 & 56 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	_ 9s 21	
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C. C. C. C.	-115 08 -118 10 - 77 37 - 76 48 - 75 16 - 74 39	N. 74° W. N. 80° W. N. 56° E. S. 56° E. E.S.E.	-85 50	$\begin{vmatrix} +23 & 07 \\ +24 & 00 \\ -19 & 50 \\ -20 & 29 \\ -22 & 41 \\ -22 & 41 \end{vmatrix}$	$ \begin{vmatrix} & 92 & 01 \\ & 94 & 10 \\ & 97 & 27 \\ & 97 & 17 \\ & 97 & 57 \end{vmatrix} $ $ - 96 & 02$	+1 03	— 94 59	
ļ	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	CR. C. C. C.	$\begin{array}{rrrrr} -&77&31\\ -&76&06\\ -&73&42\\ -119&49\\ -&117&43\\ -&77&32 \end{array}$	s. 75° E. E. by s. s. 74° w. s. 67° w. s. 10° E.	-86 00	$\begin{array}{rrrrr} -21 & 30 \\ -25 & 04 \\ +21 & 49 \\ +23 & 39 \\ -4 & 31 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	— 97 11	
5.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CR. C. CR. C. C. C. C. C. C.	- 62 37 - 62 30 - 63 34 - 61 20 - 96 17 - 88 25 - 83 24 - 65 46	s.s.w. $\frac{1}{2}$ w. s. by w. s. $\frac{1}{4}$ E. N.E. by E. $\frac{1}{2}$ E.	-85 40	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	- 83 55 - 85 18 - 85 14 - 82 38 - 85 05 - 83 54 - 84 29 - 85 56	+1 03	– 8 3 03	
6.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CR. C. C. C. C. C. C. C. C.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	s.s.w. s. $\frac{3}{4}$ w. s. $\frac{1}{2}$ w. E.N.E. E. by N. $\frac{1}{2}$ N. s. $\frac{3}{4}$ E. s. by w. $\frac{3}{4}$ w.	>-86.00	+ 9 03 + 3 42 + 2 28 -23 10 -24 00 - 3 42 + 8 35 + 2 28 0 0	- 83 51 - 84 54 - 86 49 - 86 06 - 84 44 - 84 48 - 84 11	+1 03	— 83 24	
•	-76 56 186 21 -76 56 186 21 -76 56 186 21 -76 56 186 21 -77 10 187 10 -77 07 186 50 -77 07 186 50 -77 07 186 50 -77 07 186 50 -77 07 186 50	C. C	- 95 43 - 61 53 - 63 01 - 63 08 - 92 37 - 72 58 - 70 33 - 77 19 - 75 44 - 76 11	s. by w. $\frac{1}{2}$ w. E. E. $\frac{1}{4}$ N. s. by w. $\frac{3}{4}$ w. s.e. by e. $\frac{1}{2}$ E. E.S.E. s.E. $\frac{3}{4}$ s. s.E.		$\begin{array}{c} + 7 & 22 \\ -25 & 25 \\ -25 & 25 \\ -25 & 06 \\ + 8 & 35 \\ -22 & 30 \\ -23 & 39 \\ -15 & 12 \\ -18 & 07 \\ -18 & 07 \end{array}$	- 88 21 - 87 18 - 88 26 - 88 14 - 84 02 - 95 28 - 94 12 - 92 31 - 93 51 - 94 18	+1 03	— 89 37	
8.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. C. C. Cr.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E. $\frac{1}{2}$ S. E. $\frac{1}{4}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. by N. $\frac{3}{4}$ N. S.E. by E. $\frac{3}{4}$ E. E.N.E.	86 00	$\begin{array}{rrrr} -25 & 16 \\ -25 & 07 \\ -25 & 07 \\ -23 & 35 \\ -23 & 04 \\ -25 & 25 \\ -23 & 10 \\ \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 03	- 93 24	

184I.	Position		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at-	Corrected Declination.	index	True Decli- nation.	Remarks.
	Lat.	Long.	<u> </u>				traction.		error.		R
	$-\mathring{7}7 \overset{6}{5}4$ $-\overset{7}{7} \overset{5}{5}4$	190 50	C.	-106 37	s.w. by s.		+14 14	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	o /	0 /	
	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	190 50 189 25	Cr. P.	-10742 -11045 -11056 -11410		$-86\ 00$	+14 14 + 12 01	$ \begin{vmatrix} -95 & 41 \\ -96 & 31 \\ -98 & 55 \\ -98 & 58 \end{vmatrix} $ $ -95 & 45$	+1 03	94 42	
	$ \begin{array}{ccccc} -77 & 43 \\ -76 & 26 \\ -76 & 25 \end{array} $	187 07 177 19	P. C. Cr.	$ \begin{array}{c cccc} -111 & 30 \\ -101 & 52 \\ -104 & 06 \end{array} $	s.w. s.s.w. s.s.w.		$\begin{vmatrix} +18 & 07 \\ +13 & 01 \\ +13 & 01 \end{vmatrix}$	$egin{bmatrix} -& 93 & 23 \ -& 88 & 51 \ -& 91 & 05 \ \end{pmatrix} -& 89 & 58 \ \end{bmatrix}$	+1 03	— 88 5 5	
	$ \begin{array}{c cccc} -76 & 31 \\ -76 & 30 \\ -76 & 30 \\ -76 & 30 \end{array} $	166 15 166 15	C. C.	- 82 26 - 67 30 - 65 14 - 70 38	S.S.E. $\frac{3}{4}$ E. S.E. E. by S. E. by S.		$\begin{bmatrix} -32 & 02 \\ -46 & 49 \end{bmatrix}$	$egin{array}{cccc} -105 & 13 \\ -99 & 32 \\ -112 & 03 \\ -117 & 27 \\ \end{array}$			
	$ \begin{array}{c cccc} -76 & 30 \\ -76 & 30 \\ -76 & 30 \end{array} $	166 15 166 15	C.	$\begin{bmatrix} -74 & 30 \\ -82 & 25 \end{bmatrix}$	E. by S. E. $\frac{1}{2}$ N. N.E. by E. E. $\frac{1}{2}$ N. E. by S. $\frac{3}{4}$ S.	-87 40	$ \begin{vmatrix} -46 & 47 \\ -37 & 36 \\ -46 & 47 \end{vmatrix} $	$ \begin{vmatrix} -111 & 17 \\ -120 & 01 \\ -120 & 09 \end{vmatrix} $	+1 03	-111 44	
	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c c} 166 & 20 \\ 166 & 30 \end{array} $	C. C.	$\begin{bmatrix} -72 & 58 \\ -144 & 55 \end{bmatrix}$	E. by s. $\frac{1}{2}$ s. w. by N. $\frac{1}{2}$ N.	}	$\begin{bmatrix} -45 & 14 \\ +45 & 20 \end{bmatrix}$	$egin{bmatrix} -111 & 11 \ -118 & 12 \ - & 99 & 35 \ -100 & 30 \ \end{bmatrix}$			
	$ \begin{array}{ccccc} -76 & 05 \\ -76 & 00 \\ -76 & 05 \\ -76 & 05 \end{array} $	167 00 165 49	С.	- 51 37	N.W. N.W. by W. E. 1/4 S.	$\left \begin{array}{c} -87 & 40 \end{array} \right $	$\begin{vmatrix} +37 & 36 \\ -47 & 27 \end{vmatrix}$	$ \begin{vmatrix} -100 & 30 \\ -103 & 14 \\ -99 & 04 \\ -104 & 03 \end{vmatrix} $ $ -101 & 17$	+1 03	-100 14	
19.	$-76 00 \\ -75 12$	167 00	C. C. C.	$\begin{array}{r rrrr} -129 & 44 \\ -100 & 16 \\ -110 & 40 \end{array}$	W.N.W. S. $\frac{3}{4}$ W. S.W.	$\left.\right\} - 87 40$	$\begin{vmatrix} +42 & 44 \\ + & 6 & 05 \\ +38 & 02 \end{vmatrix}$	$\begin{bmatrix} -87 & 00 \\ -94 & 11 \\ -72 & 38 \end{bmatrix}$ - 90 35		- 89 32	
	$-74 51 \\ -74 51$	168 10 168 10 168 10	C. Cr.	$ \begin{array}{c cccc} -109 & 33 \\ -110 & 11 \\ -109 & 24 \\ \hline 72 & 00 \end{array} $	s.w. s.w.	-88 00	+38 02	$\begin{vmatrix} -71 & 31 \\ -72 & 09 \\ -71 & 22 \end{vmatrix} - 71 & 55$	+1 03	— 70 52	
22.	$ \begin{array}{rrrr} -72 & 22 \\ -70 & 22 \\ -70 & 20 \\ -70 & 22 \end{array} $	170 00 166 50	C. Cr.	$ \begin{array}{c cccc} - & 72 & 08 \\ - & 19 & 00 \\ - & 21 & 22 \\ - & 45 & 30 \end{array} $	E.N.E. E. by N.	$\begin{bmatrix} -86 & 20 \\ \end{bmatrix}$	$\begin{bmatrix} -21 & 18 \\ -22 & 48 \end{bmatrix}$	$ \begin{array}{c cccc} - & 44 & 55 \\ - & 40 & 18 \\ - & 44 & 10 \\ - & 46 & 37 \end{array} $	·		
	$ \begin{array}{cccc} -70 & 32 \\ -70 & 32 \\ -70 & 32 \\ -70 & 09 \end{array} $	167 34 167 34	Cr.	$\begin{bmatrix} -57 & 07 \\ -48 & 07 \end{bmatrix}$	S. $\frac{1}{4}$ E. w. by N. $\frac{3}{4}$ N. N.W. $\frac{1}{4}$ W. N.W. $\frac{3}{4}$ N.	$-85 \ 40$	$\begin{vmatrix} +21 & 40 \\ +16 & 48 \\ +13 & 34 \end{vmatrix}$	$\begin{vmatrix} -38 & 12 \\ -40 & 19 \\ -34 & 33 \end{vmatrix} - 38 & 44$	+1 03	- 37 41	
	$ \begin{array}{c cccc} -70 & 03 \\ -70 & 03 \end{array} $	167 30	C. C.	$\begin{bmatrix} - & 46 & 51 \\ - & 51 & 55 \\ - & 50 & 19 \end{bmatrix}$	N.W. N.W. $\frac{1}{2}$ W. N.W. by W.		$\begin{vmatrix} +16 & 03 \\ +17 & 32 \\ +19 & 01 \end{vmatrix}$	$ \begin{array}{c ccccc} - & 30 & 48 \\ - & 34 & 23 \\ - & 31 & 18 \end{array} $			
26.	$ \begin{array}{cccc} -70 & 03 \\ -69 & 51 \\ -69 & 51 \end{array} $	167 50 167 50	C.	$\begin{bmatrix} -53 & 54 \\ -53 & 23 \end{bmatrix}$	w. by s. ½ s.	11	$\begin{vmatrix} +22 & 06 \\ +21 & 30 \end{vmatrix}$	$ \begin{vmatrix} -40 & 36 \\ -31 & 48 \\ -31 & 53 \\ -32 & 59 \end{vmatrix} $			
27. 28.	$ \begin{array}{c cccc} -68 & 48 \\ -68 & 48 \\ -69 & 26 \\ -69 & 55 \end{array} $	167 42 167 40	Cr.	- 47 25	w. by s. $\frac{1}{2}$ s.	85 30	$\begin{vmatrix} +21 & 48 \\ + & 4 & 20 \end{vmatrix}$	$ \begin{vmatrix} -32 & 39 \\ -29 & 43 \\ -43 & 05 \\ -45 & 41 \end{vmatrix} $ - 37 09	+1 03	— 36 06	
Mar. 1.	1	168 00 167 37	Св. С.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.s.e. w. by n. ½ n. n.w.byw.½w.		$\begin{bmatrix} -8 & 43 \\ +15 & 28 \\ +14 & 15 \end{bmatrix}$	$ \begin{array}{c cccc} - & 44 & 51 \\ - & 30 & 24 \\ - & 31 & 02 \end{array} $		·	
5.	$ \begin{array}{c cccc} -68 & 10 \\ -68 & 19 \\ -65 & 32 \\ 65 & 30 \end{array} $	$ \begin{array}{c c} 167 & 50 \\ 167 & 20 \end{array} $	C. Cr. C.	$ \begin{array}{c cccc} - & 46 & 45 \\ - & 46 & 49 \\ - & 28 & 22 \end{array} $	w.n.w. w. by n. s. by w. ½ w.	84 00	$\begin{vmatrix} +16 & 01 \\ + & 4 & 53 \end{vmatrix}$	- zo ze	+1 03	— 27 06	
	$ \begin{array}{rrrr} -65 & 32 \\ -65 & 32 \\ -65 & 32 \end{array} $	167 40	C. C.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s. by w. s. by w. ½ w. s.s.w.		+ 4 53	$\begin{bmatrix} -23 & 41 \\ -27 & 50 \\ -26 & 19 \end{bmatrix}$		-	

1841.	Position. Lat. Long.	Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Decli- nation.	Remarks.
Mar. 6.	-65 50 164 40 -65 47 164 30	C. C	$ \begin{vmatrix} -38 & 53 \\ -39 & 02 \\ -38 & 29 \\ -40 & 08 \end{vmatrix} $	s.w. by s. s.w. $\frac{1}{2}$ s. s.w. w. $\frac{3}{4}$ N.	-83 45	+ °7 36 + 6 12 + 6 12 + 4 40 + 8 59 +10 13 +11 27 +15 23	$ \begin{array}{c cccc} -29 & 36 \\ -28 & 50 \\ -28 & 10 \\ -28 & 43 \\ -29 & 54 \\ -29 & 08 \\ -27 & 02 \\ -24 & 35 \end{array} $	+1 03	-26 56	
7. 8.	$ \begin{vmatrix} -65 & 34 & 162 & 08 \\ -65 & 34 & 162 & 08 \\ -65 & 34 & 162 & 08 \\ -65 & 34 & 162 & 08 \\ -65 & 34 & 162 & 08 \\ -64 & 44 & 162 & 20 \end{vmatrix} $	C.	$\begin{array}{r} -29 & 08 \\ -27 & 42 \\ -29 & 19 \\ -36 & 28 \\ -16 & 26 \\ -25 & 28 \end{array}$	N.N.W. N.W. s.E. by E.		$\begin{vmatrix} +15 & 35 \\ +4 & 08 \\ +4 & 08 \\ +5 & 31 \\ +10 & 19 \\ -12 & 58 \\ +4 & 08 \\ -3 & 49 \end{vmatrix}$	$ \begin{array}{c cccc} -26 & 45 \\ -25 & 00 \\ -23 & 34 \\ -23 & 48 \\ -26 & 09 \\ -29 & 26 \\ -26 & 08 \\ -29 & 13 \end{array} $	+1 03	-23 47	
9.	$ \begin{vmatrix} -64 & 20 & 164 & 34 \\ -64 & 23 & 164 & 15 \\ -64 & 23 & 164 & 15 \end{vmatrix} $	C. C. C. C. C. C. C.	$\begin{array}{r} -23 & 05 \\ -20 & 49 \\ -19 & 40 \\ -18 & 01 \\ -30 & 53 \\ -31 & 16 \\ -33 & 23 \\ -32 & 17 \end{array}$	N.N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ E. s. by W. s. by W. $\frac{1}{4}$ W. s.s.W. $\frac{1}{2}$ W. s.s.W. $\frac{1}{4}$ W.	-83 00	$\begin{array}{c} -5 & 07 \\ -6 & 18 \\ -8 & 31 \\ -10 & 32 \\ +2 & 43 \\ +3 & 25 \\ +6 & 48 \\ +6 & 10 \end{array}$	-28 12 -27 07 -28 11 -28 33 -28 10 -27 51 -26 35 -26 07	+1 03	-26 58	
11.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	CR. C. CR. CR. C. C. C. C. C. C.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. N.w. ½ w. N.w. ½ w. N.w. by w. N.w. ½ w. N.w. ½ w. S.w. ¾ s. S.w. ¾ s. S.w. ¼ v.	-83 00	+ 2 43 +10 32 +10 32 +11 30 + 9 34 + 6 17 + 9 06 + 9 06 +12 00	$ \begin{array}{c cccc} -29 & 08 \\ -23 & 52 \\ -22 & 02 \\ -21 & 44 \\ -23 & 08 \\ -27 & 27 \\ -26 & 49 \\ -24 & 17 \\ -24 & 53 \end{array} $	+1 23	-22 48	Card R substituted.
12.	$\begin{vmatrix} -64 & 04 & 162 & 40 \\ -64 & 04 & 162 & 40 \end{vmatrix}$	C. C. C. C. C.	$ \begin{array}{rrrrr} -30 & 53 \\ -37 & 54 \\ -38 & 41 \\ -34 & 41 \\ -34 & 28 \\ -29 & 30 \\ -37 & 55 \end{array} $	s.w. by w. s.w.byw.½w. w.s.w. w.½ s. w. by s. s.s.w.½ w. s.w. by w.	83 00	+12 00 +12 34 +13 09 +13 51 +13 48 + 6 48 +12 00	$ \begin{array}{c cccc} -24 & 53 \\ -25 & 20 \\ -25 & 32 \\ -20 & 50 \\ -20 & 40 \\ -22 & 42 \\ -25 & 55 \end{array} $	+1 23	-22 19	
14.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	C. C. C. Cr. Cr. Cr.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.e. s. by e. ½ e. s. by e. ¾ e. s.s.e. s.s.e. s.s.e.	$-82\ 45$	- 5 24 - 5 24 - 4 00 - 4 42 - 5 24 - 5 24 - 5 24	-25 53	+1 23	—26 49	
18.	$\begin{array}{c} -63 & 50 \\ -63 $	C. C. C. C. C. C. C. C. C.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S. by W. S. $\frac{1}{2}$ E. S. by E. $\frac{1}{2}$ E. S. S. E. S. by E. $\frac{1}{4}$ E. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ E. S. S. E.	-83 45	+ 3 06 - 1 30 - 4 30 - 6 12 - 3 50 + 1 30 + 11 27 + 1 30 - 1 30 - 6 12	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	-18 31	,

1841.	Positi		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's at-	Corrected Declination.	Correc- tion for index	True Decli- nation.	Remarks.
	Lat.	Long.	ő				traction.		error.	Mation:	Ren
	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	149 00 149 00 149 00 149 00 149 00 148 12	C.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.w. $\frac{1}{2}$ s. s.s.w. $\frac{3}{4}$ w. s.s.w. $\frac{1}{2}$ w. s.s.w. $\frac{1}{2}$ w. s.w. by s. s.w. by s. s.w. by s. w. $\frac{1}{2}$ N.	-84 15	+11 11 + 9 05 + 6 45 + 8 19 + 9 50 + 9 50 + 16 13	$ \begin{array}{c cccc} -\mathring{1}3 & \mathring{1}7 \\ -14 & 58 \\ -10 & 52 \\ -15 & 12 \\ -18 & 10 \\ -16 & 01 \\ -19 & 01 \\ -5 & 36 \end{array} $	+1 23	-13 59	
22.	$ \begin{array}{r} -63 & 10 \\ -63 & 10 \\ -63 & 06 \\ -63 & 06 \end{array} $	140 00 139 30 139 30 139 30 139 40 139 40	C. C. C. C. C. C.	$\begin{array}{rrrrr} -21 & 13 \\ -17 & 14 \\ -15 & 50 \\ -18 & 22 \\ -16 & 01 \\ -17 & 47 \end{array}$	w. by N. N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{4}$ W. N.W. by W. N.W. $\frac{1}{2}$ W.	-84 00	$ \begin{array}{r} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	_ 3 29	
23. 25.	$ \begin{array}{rrrr} -62 & 25 \\ -62 & 05 \\ -62 & 05 \\ -62 & 05 \\ -60 & 23 \end{array} $	136 30 136 30 136 00 136 00 136 00 131 38	C. C. C. C. C.	$ \begin{array}{ c c c c c } -14 & 54 \\ -11 & 20 \\ - & 2 & 53 \end{array} $	N.W. $\frac{1}{2}$ W. N.W. by N. N.W. $\frac{1}{4}$ W. W. by N. $\frac{1}{4}$ N. W. by N. W.N.W. N.W. $\frac{1}{2}$ N.	$-83 \ 45$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	+1 23	+ 1 35	
	$\begin{array}{ccccc} -60 & 23 \\ -60 & 23 \\ -60 & 23 \\ -60 & 23 \\ -60 & 23 \\ -60 & 23 \\ -60 & 33 \\ -60 & 33 \\ -60 & 33 \\ \end{array}$	131 38 131 38 131 38 131 38 131 38 131 38	C. C		N.W. \frac{1}{2} N. N.W. \frac{1}{2} N. N.W. \frac{1}{2} W. N.W. \frac{1}{2} N. N.W.	>-83 10	+ 8 43 + 8 43 + 10 48 + 9 48 + 8 43 + 8 43 + 9 15 + 9 48 + 9 48	+ 8 08 + 5 28 + 5 55 + 5 36 + 6 26 + 6 19 + 6 41 + 9 07 + 7 50	+1 23	+ 8 15	
	-60 23 -60 20 -60 20	131 38 131 30 131 30 131 30 131 30 131 30 131 30 131 30 131 30	CR. C.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. w. by N. ½ N. N. ½ W. N.W.byW.½W. N. ¾ W. N. ¾ W. N.W.byW.¼W. N.N.E. N.E. by N. N.N.E. N.W.byW.½W.	-83 00	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	+ 8 14	+1 23	+10 23	
27.		129 40 129 40 129 40 129 40 129 40 129 45		$ \begin{vmatrix} - & 0 & 17 \\ + & 7 & 47 \\ + & 4 & 29 \\ + & 2 & 34 \\ + & 1 & 08 \\ + & 5 & 05 \\ + 10 & 02 \end{vmatrix} $	N.W. ½ N. N. ¾ W. N. by W. ¼ W. N.N.W. ¼ W. N.N.W. ¾ W. N.N.W. N.N.W.	$\left. \begin{array}{c} -82 & 45 \end{array} \right.$	$\begin{array}{c} + & 8 & 15 \\ + & 1 & 49 \\ + & 3 & 03 \\ + & 5 & 32 \\ + & 6 & 41 \\ + & 4 & 58 \\ & 0 & 0 \\ + 11 & 30 \end{array}$	+ 7 58 + 9 36 + 7 32 + 8 06 + 7 49 +10 03 +10 02	+1 23	+10 07	
28.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	127 40 127 40 127 40 127 40 127 40 127 40	C. C. C. Cr. Cr. C.	$\begin{vmatrix} - & 3 & 41 \\ - & 2 & 00 \end{vmatrix}$	w. by s. $\frac{3}{4}$ s. w. by s. w. $\frac{1}{2}$ s. E. by N. $\frac{3}{4}$ N. w. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	-81 45	+11 48 $+11 49 $ $-11 04 $ $+11 47 $ $-8 58 $ $-8 58$	+ 6 35 + 8 07 + 9 49 + 3 20 + 9 28 +11 03 + 3 29 + 5 58	+1 23	+ 8 37	

1841.	Position	n. Long.	Declination observed.		Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
Mar. 29.				8 N.E. by E. ½ E.	- · ·	- °9 41	+ °6 17) ° ′	0 /	· /	
mar. 29.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	29 50 C 29 50 C 29 37 C	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. $\frac{1}{2}$ E. N.E. E. by N.	-81 15	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	+5 21	
30.		29 30 C 30 10 C 32 00 C	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. by N. N.E. E. $\frac{3}{4}$ E. N.E. by E. $\frac{1}{2}$ E.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{cccc} + & 5 & 35 \\ + & 3 & 11 \\ + & 3 & 25 \\ - & 1 & 00 \end{array} $			
		$egin{array}{c cccc} 32 & 00 & 0 \ 32 & 00 & 0 \ 32 & 00 & 0 \ \end{array}$. + 8 28	$N.E. \frac{1}{2} N.$ $N.E. \frac{1}{2} N.$ $N.E.$	80 20	$ \begin{array}{c cccc} - & 6 & 50 \\ - & 6 & 05 \\ - & 6 & 50 \\ - & 5 & 20 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	+0 45	
	-55 12 13 -55 04 13 -55 04 13 -55 04 13	32 00 C 32 10 C 32 10 C 32 10 C 32 10 C	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by E. $\frac{3}{4}$ E. N. $\frac{1}{2}$ E. N.E. by E. N.N.E. $\frac{1}{2}$ E. N. $\frac{3}{4}$ E.	-80 20	- 3 13 - 0 50 - 8 24 - 4 40 - 1 26	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	+1 23	+0 16	
	-55 04 13 -54 56 13 -54 56 13 -54 56 13 -54 56 13 -55 06 13	$egin{array}{c cccc} 32 & 15 & 0 \ 32 & 15 & 0 \ 32 & 15 & 0 \ 32 & 15 & 0 \ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. by N. N.N.E. $\frac{3}{4}$ E. N. by E. $\frac{3}{4}$ E. N. $\frac{3}{4}$ E. N.N.E.	$\left.\right = -80 \ 20$	$ \begin{vmatrix} -7 & 18 \\ -5 & 32 \\ -5 & 01 \\ -3 & 13 \\ -1 & 26 \\ -3 & 48 \end{vmatrix} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	-0 06	
	$ \begin{array}{c cccc} -55 & 01 & 13 \\ -54 & 05 & 13 \\ -54 & 05 & 13 \\ -54 & 05 & 13 \\ -54 & 05 & 13 \end{array} $	34 50 C 34 50 C 34 50 C 34 50 C	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by N. $\frac{1}{2}$ N. E. by N. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.		- 6 05 - 8 33 - 8 15 - 8 24 - 9 01 - 8 56	_ 3 19			
•	-54 05 13 -54 06 13 -54 06 13 -54 06 13 -54 06 13	34 50 C 34 31 C 34 31 C 34 31 C		E. $\frac{1}{2}$ N. E. by N. E. by N. E. by N.	-79 15	- 9 01 - 8 52 - 8 52 - 8 52 - 9 10	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	-3 44	
April 1.	-54 06 13	34 48 C 34 50 C 34 50 C	+338	E. N.N.E. $\frac{3}{4}$ E. N.E. $\frac{1}{2}$ E.		- 9 10 - 4 18 - 6 33 - 4 18	$ \begin{array}{cccc} & 5 & 32 \\ & 4 & 48 \\ & 7 & 19 \\ & 5 & 02 \end{array} $			
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c cccccccccccccccccccccccccccccccc$	$egin{array}{c cccc} -1 & 52 \\ -1 & 18 \\ -2 & 56 \\ \hline \end{array}$	N. by E. $\frac{1}{4}$ E. N. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E.	79 00	$ \begin{array}{c cccc} & 2 & 01 \\ & 2 & 25 \\ & 2 & 25 \\ & 3 & 12 \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1 23	—3 55	
2.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	35 10 C 36 49 C 36 49 C 36 50 C		N.N.E. N. by E. $\frac{3}{4}$ E. N. by E. $\frac{1}{4}$ E.		$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{c c} -7 & 20 \\ -7 & 58 \\ -5 & 56 \\ -7 & 09 \end{array} $	+1 23	-5 38	***************************************
5.	-44 53 14 -44 53 14 -44 56 14 -44 40 14 -44 56 14	$egin{array}{c ccc} 43 & 00 & 0 & 0 \\ 43 & 16 & 0 & 0 \\ 43 & 50 & 0 & 0 \\ \hline \end{array}$	$\begin{bmatrix} -8 & 16 \\ -7 & 21 \end{bmatrix}$	N.E. by E. N.E. N.E. 3 E.	72.00	- 3 43 - 3 43 - 4 26 - 3 43 - 4 00	-11 27 -11 05 -11 38 -11 59 -11 21	, 1 oo	S 3V	
	$ \begin{vmatrix} -44 & 56 \\ -44 & 50 \\ -44 & 50 \\ -44 & 05 \\ -44 & 05 \\ -44 & 05 \end{vmatrix} $	43 20 C 43 20 C 45 30 C	R. — 2 22	S.E. S.S.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	>-73 00	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	+1 23	o sy	
	-44 05 14		-557		J	-353				

General Table of the Declinations observed on board Her Majesty's Ships Erebus and Terror, between November 1840 and April 1841.

Lat.	Long.	Ship.	No. of observa-	Declina- tion.	Lat.	Long.	Ship.	No. of observations.	Declina- tion.
. ,	. ,			. ,	0 /	0 /			0 /
+ 15° to + 5°.						166 12		6	$-1^{\circ}7$ 44
CO 201				. 10 00	-52 33	169 09	Erebus.	2	-1752
$ \begin{array}{rrr} -60 & 20 \\ -59 & 03 \end{array} $	$\begin{array}{ccc} 131 & 30 \\ 129 & 33 \end{array}$	Terror. Terror.	10 7	+10 23 $+10 07$		151 35 169 06	Terror. Erebus.	10 5	-18 31 $-18 44$
	129 33	Erebus.	10	+ 8 47		151 48	Erebus.	6	-18 44 -18 59
	127 40	Terror.	8	+ 8 37		151 51	Erebus.	6	$-20 \ 15$
	129 38	Erebus.	11	+ 8 32	l .	170 05	Terror.	8	-20 20
9	131 21	Erebus.	8	+ 8 18	1 -	170 05	Terror.	13	-20 56
-60 25	131 38	Terror.	11	+ 8 15	-59 32	169 59	Erebus.	8	-21 28
	131 37	Erebus.	10	+ 8 09	-57 10	170 06	Erebus.	7	-21 58
$-60^{\circ} 20$			7	+ 7 38	1	170 39	Terror.	12	-21 58
-56 14			8	+ 5 46		170 26	Erebus.	7	-21 59
-56 39	129 45	Terror.	7	+ 5 21		161 47	Terror.	7	-22 19
1	4	5° to -	5°.			170 55	Erebus.	11	-22 32
$-62 \ 13$				+ 1 35	1	163 04 170 25	Terror. Erebus.	7	$-22 ext{ } 48$ $-22 ext{ } 49$
	130 12	Erebus.	5 7	$+ 1 35 \\ + 1 34$		170 25 162 08	Terror.	10 6	$-22 ext{ } 49 $
	132 44	Erebus.	9	+ 109	$-60 \ 18$	170 12	Terror.	12	$-23 \ 48$
1	132 00	Terror.	7	+ 0.45	-64 05	161 13		9	-24 06
8	131 15	Erebus.	7	+ 0 31	-63 10		Erebus.	9	-24 07
-55 04	132 10		5	+ 0 16				,	
	132 13	Terror.	6	- 0 06			25° to — 3	35~.	
	136 07	Erebus.	6	— 0 27	-65 06		Erebus.	8	-25 06
	135 26	Erebus.	7	— 1 03		163 14	Erebus.	11	-25 18
	136 23	Erebus.	7	- 1 13		172 31	Erebus.	9	-25 33
-54 04		Erebus.	7	- 1 44		173 00	Terror.	9	-25 52
$-54 04 \\ -63 22$		Erebus.	6	-150 -329		162 42 172 44		9	-25 54 $-25 57$
	$139 41 \\ 134 44$	Terror. Terror.	8 11	-329 -344	11	172 44	Erebus. Terror.	8 7	-25 57 -26 17
9	$135 \ 05$	Terror.	8	-355		157 01	Terror.	7	-26 17
$-62 \ 37$			6	- 4 05		164 39	Terror.	9	-26 56
-51 11			5	- 4 39	-64 33	163 23	Terror.	10	-26 58
	'		, -0	-	-6652	167 35	Terror.	8	-27 06
		5° to -1	5~.			171 45	Erebus.	7	-27 11
-51 15			3	- 5 38		169 44		8	-27 21
$-63 \ 13$		1	12	- 5 58		172 29	Erebus.	11	-27 34
	140 40	1	6	-657		172 34	Erebus.	10	-28 08
3	143 56 $145 04$		11	$\begin{bmatrix} -8 & 39 \\ -8 & 46 \end{bmatrix}$		169 51 165 10	Erebus.	9	-28 21 $-28 23$
-44 18 $-42 52$			9 6	-840 -1024		173 05	Erebus. Terror.	13 12	-28 23 $-29 17$
-44 24			2	-10^{21}	$-65 \ 35$		Terror.	12	-29 42
		Erebus.	2	$-12 \ 37$	-67 16		Erebus.	16	-31 29
-45 36			8	-13 09	-67 56	167 31	Erebus.	8	$-32 \ 35$
-46 08	154 15	Erebus.	8	-13 38	-68 31	176 05	Erebus.	12	-3352
-46 13			4	-1347	-68 00	175 05	Erebus.	13	_34 04
$-46 \ 30$			7	-1358	-68 24			10	-34 38
-64 17			7	-13 59	-68 28			1	-34 39
-49 18			. 4	-14 44	-68 55	176 20	Erebus.	5	—34 58
1	15° to — 2			- ;	35° to — 4	45°.			
-50 33	166 15	Terror.	42	-15 29	-69 23			7	-36 06
-50 54	166 35	Erebus.	7	-16 03	-68 59	167 46	Erebus.	12	-36 12
-52 22	169 38	Terror.	11	-1708	-70 27	167 57	Terror.	11	$-37 \ 41$
-49 47			8	-17 16	-69 33	167 31	Erebus.	11	-38 21
-64 17	149 03	Erebus.	5	-17 19	-70 03	167 30	Erebus.	10	-39 21

General Table of Declination. (Continued.)

Lat.	Long.	Ship.	No. of observa- tions.	Declina- tion.	Lat.	Long.	Ship.	No. of observa-	Declina- tion.
	. ,			· /	. ,	. ,			. ,
	35° to —			8	85° to — 9)5°.			
-70 23 -71 00 -71 22 -71 51 -71 08 -71 52 -71 25 -72 33 -72 36 -72 16 -72 36 -72 40	167 23 172 25 170 56 171 53	Erebus. Erebus. Erebus. 45° to — Terror. Terror. Erebus. Terror. Erebus. Erebus. Erebus. Erebus. Erebus.	7 9 10 9	-39 34 -39 44 -43 56 -44 0: -44 24 -46 46 -46 59 -48 19 -50 3: -51 4: -52 3: -52 4:	$\begin{array}{c cccc} -76 & 23 \\ -77 & 12 \\ -76 & 25 \\ -77 & 22 \\ -75 & 36 \\ -77 & 03 \\ -77 & 28 \\ -77 & 28 \\ -77 & 36 \\ -77 & 36 \\ -77 & 36 \\ -77 & 44 \\ -77 & 51 \\ -77 & 46 \\ \end{array}$	177 25 187 02 177 35 186 21 167 45 186 40 186 33 168 12 188 22 186 40 186 41 188 00	Erebus. Terror. Erebus. Terror. Terror.	5 2 10 2 6 2 10 6 9 9 9 9 9 8 8 8 8	
-72 34		55° to —		-54 34	-77 45				
-73 53	171 37 171 42	Erebus.	•		$ -77 \ 43$	-	Terror.	8 6 6	$\begin{bmatrix} -95 & 21 \\ -95 & 52 \\ -96 & 00 \end{bmatrix}$
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	172 35 171 23 168 37 169 00 168 10 168 42 167 53	Terror. Terror. Erebus. Terror.	5 10 6 7 4 10 2	$ \begin{vmatrix} -65 & 04 \\ -65 & 4 \\ -68 & 40 \\ -69 & 40 \\ -70 & 50 \\ -71 & 00 \\ -74 & 40 \end{vmatrix} $	-77 51 -77 47 -77 44 -76 07 -75 58 -76 10 -76 04 -77 47	186 38 180 34 186 06 168 45 168 50 166 02 166 19 176 19 175 57	Erebus. Erebus. Terror. Erebus. Terror. Erebus. Terror. Terror. Erebus.	10 1 5 4 2 4 5 5 7	- 96 14 - 96 17 - 97 11 - 98 45 - 99 41 - 99 41 - 100 14 - 102 09 - 104 25
$\begin{array}{c cccc} -76 & 57 \\ -77 & 18 \\ -77 & 08 \\ -77 & 11 \\ -77 & 22 \\ -77 & 07 \\ -76 & 57 \\ -77 & 17 \end{array}$	186 38 192 38 189 02 192 58 188 43 192 22 188 30 191 35	Erebus. Erebus. Erebus. Terror. Terror.	5 9 13 6 6 12 13 9 6 9	-77 5 -81 3 -81 5 -82 0 -82 2 -82 2 -83 0 -83 5 -83 5 -84 5	$\begin{bmatrix} -77 & 50 \\ -76 & 22 \\ -76 & 47 \\ -76 & 32 \\ -76 & 36 \\ -76 & 33 \\ -77 & 22 \\ \end{bmatrix}$	178 00 165 44 169 26 166 30 166 18 164 45	Terror. Terror. Erebus.	115°. 4 6 2 9 13 8 4	-105 21 -106 13 -107 05 -111 44 -113 23 -113 41 -114 21

Total number of observations 1368. No observation has been omitted or its result rejected. The scale of the declination chart has not permitted the insertion of all the results comprised in this table, and a few of those of the Terror have consequently been omitted in the very high latitudes where the figures are most crowded. The next number of these contributions, embracing the observations of the succeeding voyage, will contain a declination chart of the high latitudes on a more extended scale, in which all the results of both voyages will be inserted.

General Table of the Inclinations observed in Her Majesty's Ship Erebus, from June 1840 to April 1841.

Lat.	Long.	No. of observations.	Inclination.	Lat.	Long.	No. of observa-	Inclination.
-48 41 -48 29 -48 17 -47 55 -47 46 -47 12 -47 03 -47 39 -47 35 -47 45 -47 41 -47 41 -47 41 -46 13 -45 59 -45 17 -44 24 -46 13 -45 52 -44 16 -45 13 -45 33 -46 18 -47 46 -49 20 -50 28 -50 33 -52 34 -54 06 -55 50 -57 15 -57 54 -58 57 -59 43 -60 19 -60 46 -61 34 -62 06 -62 40 -62 44 -64 00 -64 06 -63 31 -65 58 -66 17 -66 30 -66 32 -66 32 -66 32 -66 32 -65 39 -65 22	68 54 76 55 80 15 83 00 86 18 89 45 93 00 102 42 106 26 110 39 114 15 121 30 135 38 139 19 141 39 142 38 147 24 149 29 151 57 152 45 154 30 157 40 166 19 169 10 169 09 170 40 170 25 170 40 170 57 169 39 170 44 172 57 173 40 174 36 172 47 173 40 174 36 175 170 12 170 12 1	tions. 9 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} -\mathring{7}0 & 00 & a \\ -70 & 55 \\ -71 & 50 \\ -72 & 34 \\ -73 & 33 \\ -73 & 35 \\ -74 & 37 \\ -74 & 28 \\ -74 & 31 \\ -75 & 26 \\ -76 & 04 \\ -76 & 41 \\ -75 & 17 \\ -73 & 48 \\ -73 & 23 \\ -73 & 33 \\ -70 & 41 \\ -71 & 49 \\ -71 & 37 \\ -72 & 04 \\ -71 & 37 \\ -72 & 04 \\ -73 & 14 \\ -74 & 23 \\ -73 & 10 & c \\ -74 & 46 \\ -76 & 16 \\ -77 & 43 \\ -74 & 46 \\ -76 & 16 \\ -77 & 43 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -78 & 34 \\ -79 & 58 \\ -79 & 30 \\ -79 & 41 \\ -79 & 58 \\ -80 & 09 \\ -81 & 03 \\ -81 & 11 \\ -82 & 20 \\ -82 & 25 \\ -82 & 40 \\ -82 & 53 \\ -81 & 51 \\ -81 & 43 \\ \end{array}$	-68 17 -68 28 -68 28 -68 28 -68 28 -68 23 -70 23 -71 15 -71 24 -71 52 -72 17 -72 17 -72 17 -72 35 -72 35 -72 35 -72 35 -72 35 -74 43 -74 45 -75 22 -76 06 -77 07 -77 47 -77 06 -77 07 -77 10 -77 09 -77 17 -77 09 -77 17 -77 09 -77 17 -77 09 -77 17 -77 09 -77 17 -77 09 -77 17 -77 00 -77 17 -77 00 -77 55 -76 59 -77 38 -76 22 -76 50 -76 10 -77 55 -77 38 -76 22 -76 50 -76 17 -77 55 -77 38 -76 22 -76 59 -77 55 -77 38 -76 22 -76 50 -77 55 -77 38 -76 22 -76 50 -77 55 -77 38 -76 22 -76 50 -77 55 -77 38 -76 22 -76 50 -77 55 -77 55	175 00 175 49 176 31 176 32 176 23 174 50 171 15 170 44 170 52 172 08 171 51 173 35 176 06 173 34 173 39 171 47 170 40 171 35 173 23 169 48 168 23 169 01 168 48 188 36 189 08 181 54 189 08 181 36 182 18 185 26 192 18 185 26 192 48 188 43 189 04 187 00 188 05 183 26 175 37 172 35 169 48 188 36 189 04 187 00 188 05 183 26 175 37 172 35 168 07 172 35 168 07 172 35 168 07 173 36 175 37 176 36 175 37 176 36 177 37 178 378 378 378 378 378 378 378 378 378 3	tions. 5 6 5 5 5 4 4 4 3 3 5 4 4 7 8 8 7 5 4 3 4 4 2 2 5 5 4 4 5 6 5 5 2 5 4 3 6 1 7 4 5 6 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6	-83 12 -83 28 -83 17 -83 35 e -83 40 -85 50 -85 53 -86 13 -85 53 -86 13 -85 55 -86 36 -86 51 -87 04 -87 12 -87 12 -87 25 -88 21 -88 27 -88 21 -86 23 -86 12 -86 23 -86 12 -86 23 -86 12 -86 23 -86 23 -87 25 -88 21 -86 23 -86 23 -87 26 -88 21 -88 25 -88 21 -88 25 -88 26 -88
$ \begin{array}{r rrr} -66 & 55 \\ -67 & 27 \end{array} $	$174 \ 31$ $174 \ 51$	3 4	$-82 \ 13$ $-82 \ 58$	$\begin{vmatrix} -72 & 13 \\ -70 & 55 \end{vmatrix}$	171 04 168 43	$\begin{vmatrix} 4 \\ 3 \end{vmatrix}$	-86 23 $-85 53$

 $[\]alpha$ On shore at Kerguelen Island. b On shore at Van Diemen Island. c On shore at Auckland Island. d. On shore at Campbell Island. e On Ice.

General Table of Inclination. (Continued.)

Lat.	Long.	No. of observations.	Inclination.	Lat.	Long.	No. of observa- tions.	Inclination.
-70 41 -70 17 -70 14 -69 57 -69 24 -69 46 -69 06 -68 28 -67 47 -65 49 -65 53 -64 41 -64 20 -63 54 -64 18 -64 33	167 20 167 24 167 16 167 52 167 55 167 43 168 10 167 22 168 12 162 14 162 34 163 29 160 55 156 59 156 06 154 47 154 03 153 02 151 56 149 09 148 03	463255557344554335334	-85 51 -86 19 -86 06 -85 41 -85 28 -85 54 -85 26 -85 07 -84 28 -83 35 -83 51 -82 55 -82 54 -83 32 -83 33 -83 34 -84 06 -84 14 -84 06 -84 48 -85 03	-65 14 -65 11 -65 09 -64 20 -63 09 -62 18 -61 18 -60 20 -59 25 -58 06 -57 22 -56 28 -55 02 -54 02 -53 13 -51 16 -48 48 -46 55 -46 25 -44 57 -43 50	144 37 143 52 143 07 140 40 139 28 136 40 134 02 131 21 130 14 128 43 127 37 129 57 131 48 132 50 134 59 135 18 136 50 138 34 139 55 140 55 144 18 146 00	336576551215685443785	-85 05 -85 10 -85 16 -84 36 -84 46 -84 20 -83 55 -83 31 -82 52 -82 09 -81 43 -80 43 -80 15 -80 07 -79 39 -79 39 -77 59 -76 54 -75 42 -75 12 -73 54 -72 15

General Table of the Intensity of the Magnetic Force from the observations made on board Her Majesty's Ship Erebus, between July 1840 and April 1841.

Latitude.	Longitude.	Intensity.	Latitude.	Longitude.	Intensity.	Latitude.	Longitude.	Intensity.
		London = 1.372.	<u></u>	S .	London = 1.372.			London = 1.372.
-4841	$\overset{\circ}{68}$ $\overset{\prime}{54}$	1.465	$-60^{\circ} 31^{\circ}$	170 32	1.951	$\begin{vmatrix} -\mathring{7}7 & \acute{0}0 \end{vmatrix}$	192 18	2·0 39
-48 29	76 55	1.539	$-60 \ 31$	170 32	1.960	$-77 \ 00$	192 18	2·036
$-48 \ 17$	80 15	1.574	$-62 \ 40$	174 40	1.983	-77 14	192 02	2.020
-47 55	83 51	1.601	-64 00	172 44	1.976	-77 09	188 50	2.036
-47 46	86 18	1.575	-64 06	172 38	1.973	-7658	188 40	2.035
-47 12	89 45	1.565	$-64 \ 31$	172 55	1.988	-77 43	187 11	2.035
-47 03	93 00	1.712	$-65 \ 46$	171 40	1.996	-7655	188 49	2.048
-47 26	99 54	1.783	$-66 \ 31$	169 20	2· 008	-7650	183 26	2.035
-47 35	106 26	1.863	-6623	170 12	2.018	-76 16	175 50	2.017
-47 40	112 27	1.898	-65 39	170 44	2.046	-7603	169 30	2.033
-47 41	121 30	1.992	-65 22	170 40	2.025	-76 20	165 32	2.041
-47 34	124 43	1.996	-6655	174 31	2.009	-75 03	168 44	2.040
-4628	130 13	2.007	-68 30	175 40	2.011	-71 17	170 43	2.037
-45 59	135 38	1.989	-68 28	176 31	2.032	-71 04	170 07	2.026
-45 17	139 19	2.005	-68 28	176 32	2.025	-70 25	167 27	2.036
-44 24	141 39	1.976	$-68 \ 48$	176 45	2.016	-6924	167 49	2.025
-44 16	142 38	1.934	-70 23	174 50	2.033	-68 28	168 10	2.047
-45 02	143 10	1.923	-71 15	171 15	2.030	-67 52	167 28	2.043
-46 22	141 06	1.954	-71 24	170 44	2.029	$-65 \ 31$	167 42	2.041
-4629	140 40	1.949	-7147	170 52	2.056	-64 58	162 27	2.024
$-43 \ 41$	146 03	1.892	-72 07	172 19	2.038	-64 13	163 18	2.018
-4252	147 24	1.820	-71 55	171 51	2·028	-63 57	161 11	2.010
-44 10	149 29	1.844	-72 12	172 13	2·032 2·026	$-62 \ 41$	156 59	2.022
-45 13	151 57	1.833	-72 09	173 35		-63 50	156 06	2.013
-45 33	152 45	1.843	-7257	176 06	2·038 2·035	-64 13	154 03	2.011
-46 18	154 30	1.820	-72 35	173 34	2·035 2·039	-64 20	153 02	2.032
-47 46	157 40	1.817	$-72 \ 31$	173 39	2·059 2·052	-63 54	151 56	2.023
-49 20	160 13	1.846	-73 47	171 50	2·032 2·044	-64 26	148 20	2.065
-50 28	164 09	1.858	-74 10	170 28	2·052	$-64 \ 45$	142 00	2.068
-50 33	166 19	1.851	-74 06	171 20	2·035	-63 09	139 28	2.043
-5242	169 10	1.877	-7356	172 20	2·037	-61 46	135 12	2.051
-5347	169 02	1·844 1·874	$\begin{bmatrix} -74 & 36 \\ -74 & 44 \end{bmatrix}$	173 01 169 43	2·045	$-60 19 \\ -58 00$	131 20 128 40	2·071 2·056
-54 25	169 16	1.874	4 *	169 43	2·048			2·056 2·027
-55 50	170 06	1.903	$\begin{bmatrix} -75 & 22 \\ -76 & 06 \end{bmatrix}$	168 48	2.031	$\begin{bmatrix} -54 & 44 \\ -53 & 13 \end{bmatrix}$	132 21 135 18	2·027 2·047
$-57 15 \\ -57 54$	$170 \ 40$ $170 \ 25$	1.914	-76 06 $-76 46$	169 22	2.040	-53 13 -51 16	136 50	2·047 2·041
$-57 54 \\ -58 57$	170 25	1.911	$-70 \ 40$ $-77 \ 47$	175 43	2.017	-51 10	190 90	% U 11
$-58 \ 57$ $-59 \ 41$	169 38	1.920	$\begin{bmatrix} -77 & 47 \\ -77 & 04 \end{bmatrix}$	188 24	2.017	0		
$-60 \ 14$	170 15	1.951	-77 17	185 26	2.023			
-00 14	1/0 10	1 201	1 11	100 20	l	5		